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INGENIERIA COMPUTACIONAL

Adaptive T-spline Refinement for Isogeometric Analysis in Planar Geometries

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**Isogeometric Analysis: Integrating Design and Analysis (IGA 2014),
January 8-10, 2014, Austin, Texas, USA**

MINECO y FEDER Project: CGL2011-29396-C03-00

CONACYT-SENER Project, Fondo Sectorial, contract: 163723

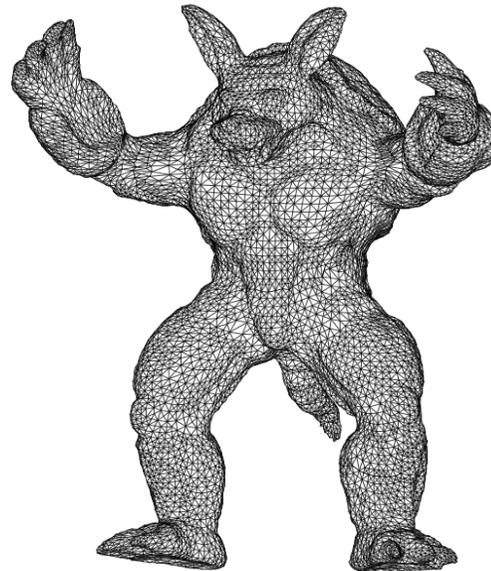
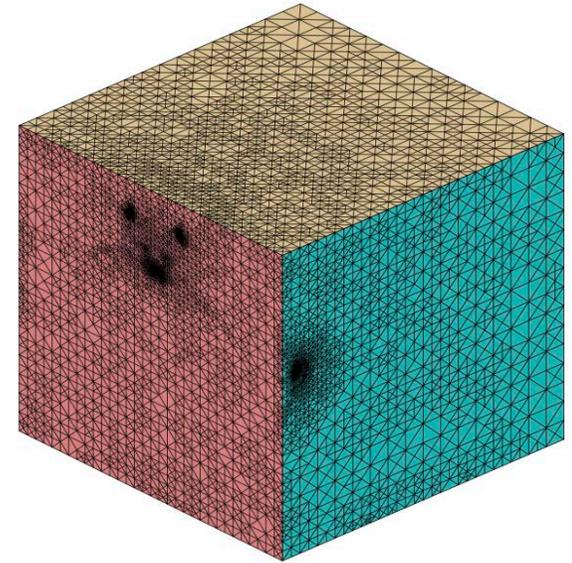
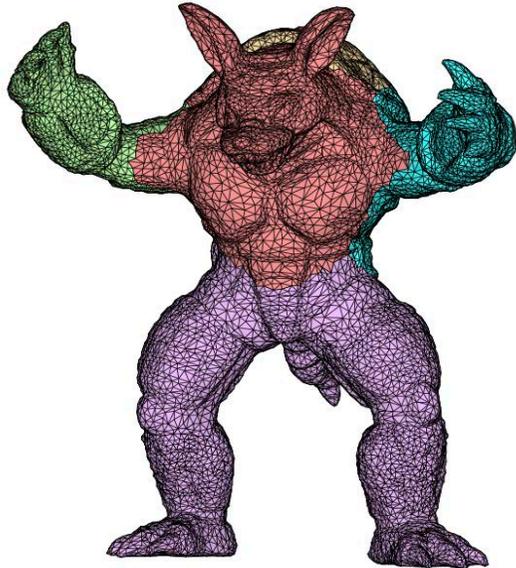
- ❑ **The Meccano Method (based on tetrahedral mesh optimization)**
 - **The initial algorithm for tetrahedral mesh generation**
 - **Volumetric parameterization of tetrahedral meshes**
 - **Application to isogeometric solid modeling and analysis**

- ❑ **The Meccano Method (based on a new 2D T-mesh optimization)**
 - **The new algorithm for two-dimensional T-mesh generation**
 - **T-spline parameterization of 2D geometries**
 - **Geometries with several materials or holes**
 - **Application to isogeometric modeling and analysis**

- ❑ **Comments and Future Research**

Meccano Method for Complex Solids

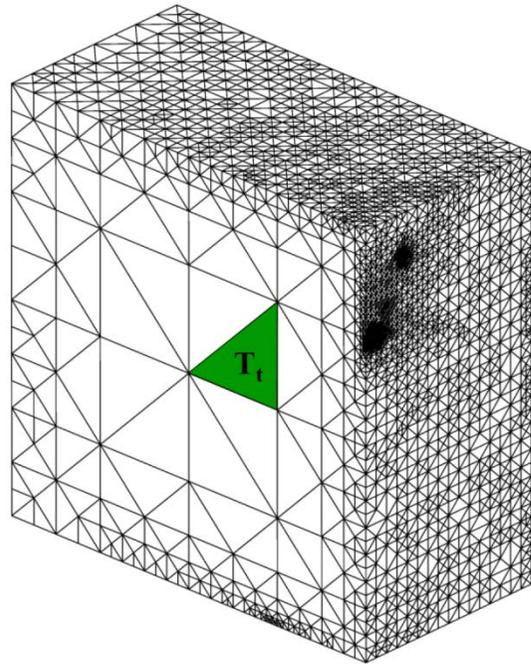
Volume parameterization based on SUS of tetrahedral meshes



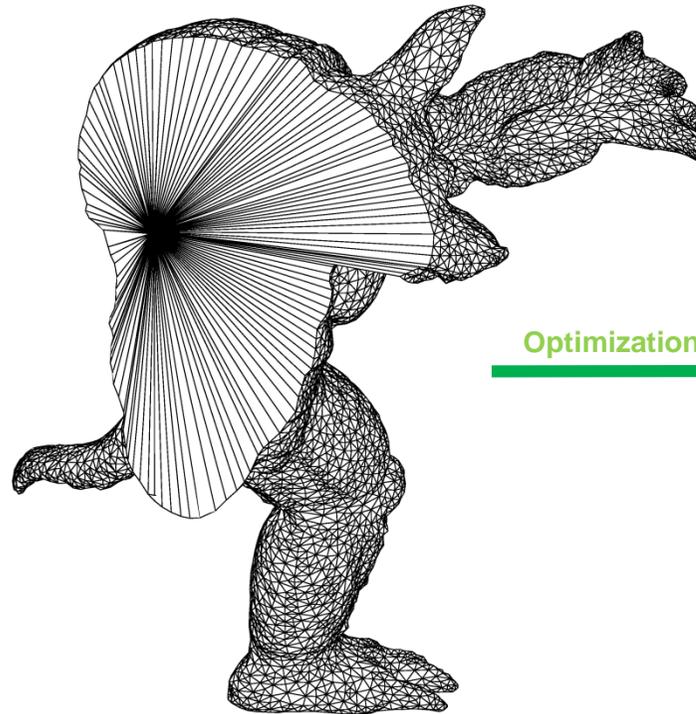
- Parameterization
- Refinement
- Untangling/Smoothing

Meccano Method for Complex Solids

Volume parameterization based on SUS of tetrahedral meshes

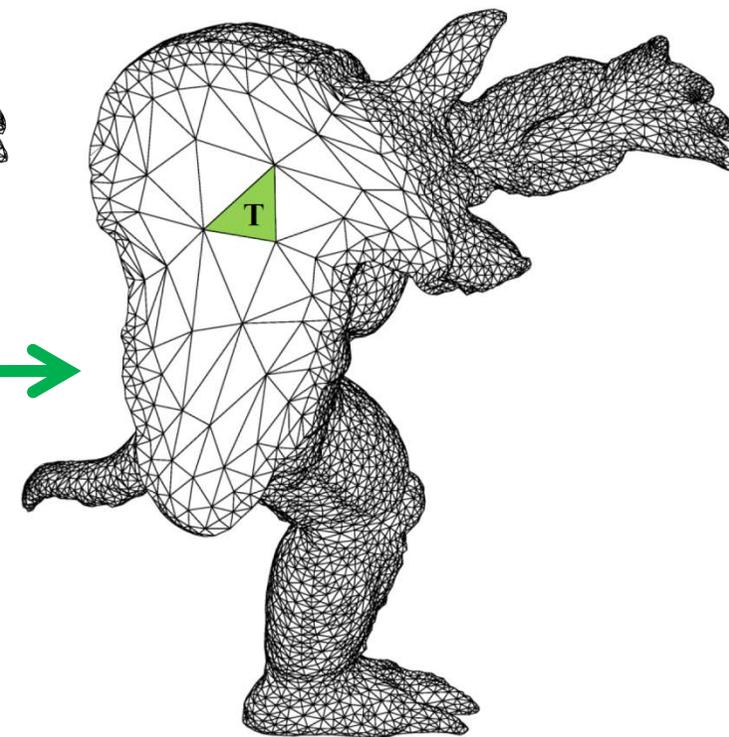


Parameter space
(meccano mesh)



Physical space
(tangled mesh)

Optimization →



Physical space
(optimized mesh)

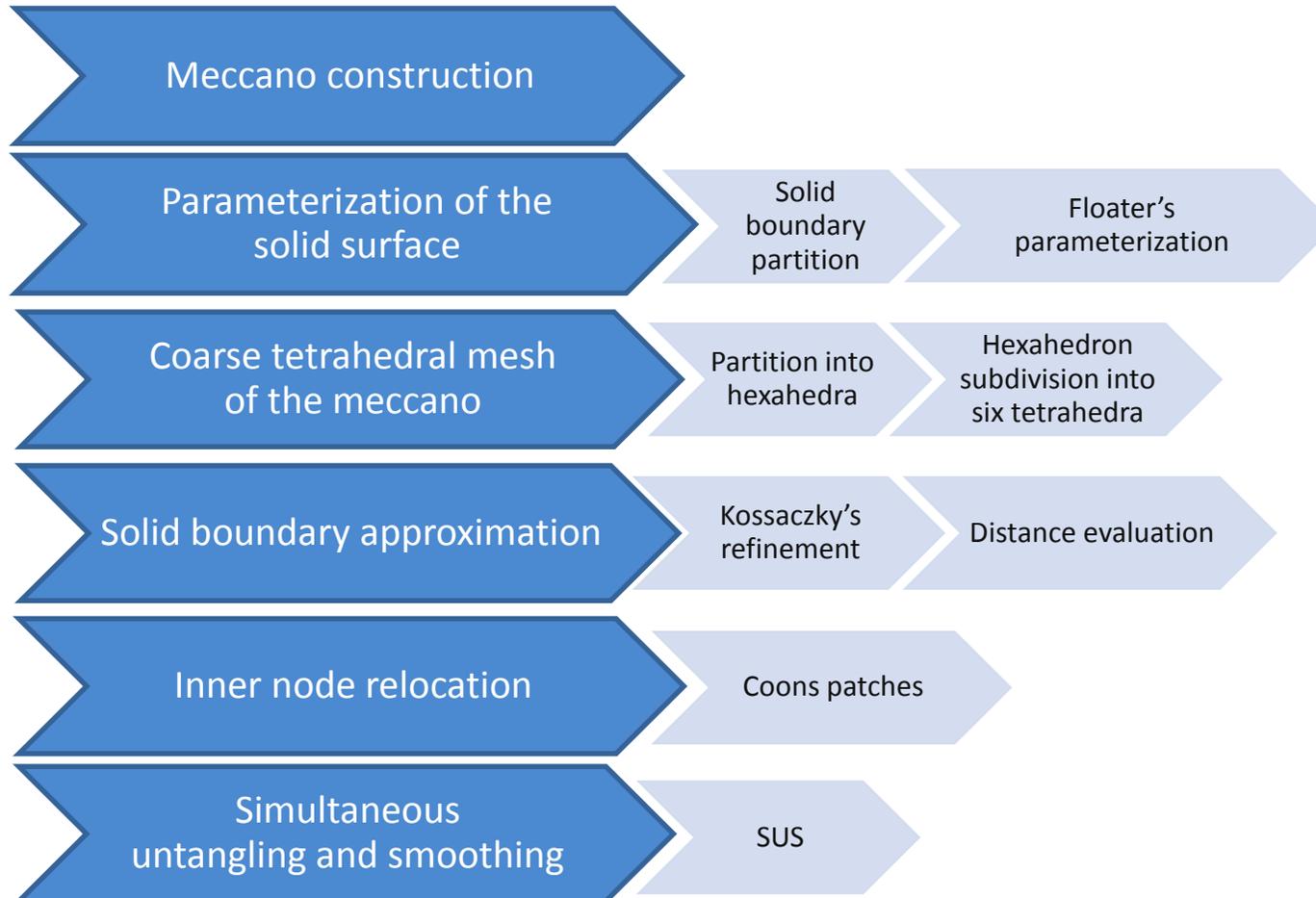
Target Element T_t ← Optimization

Physical Element T

(to get less distortion in the parameterization)

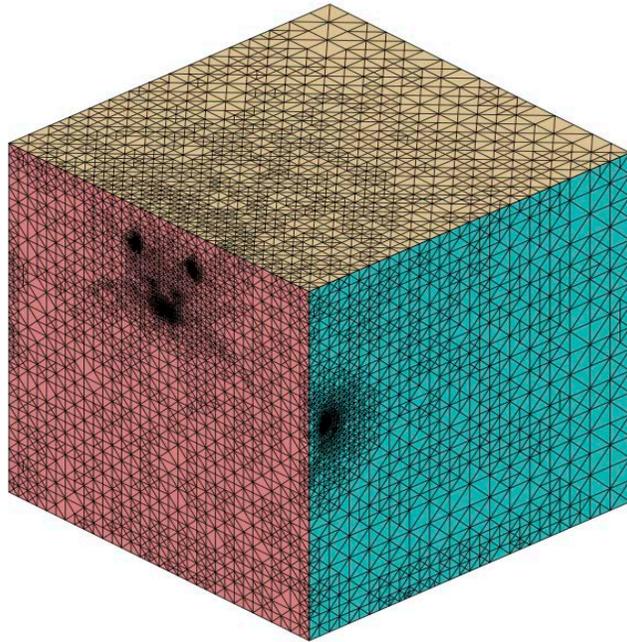
Meccano Method for Complex Solids

Algorithm steps

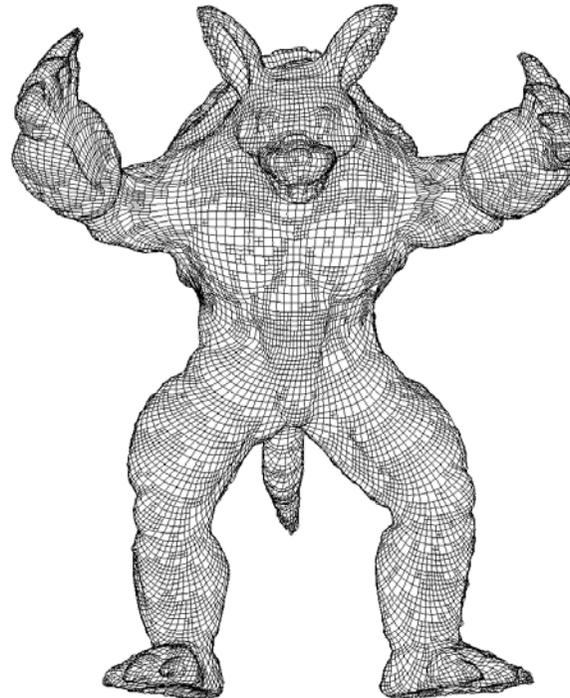
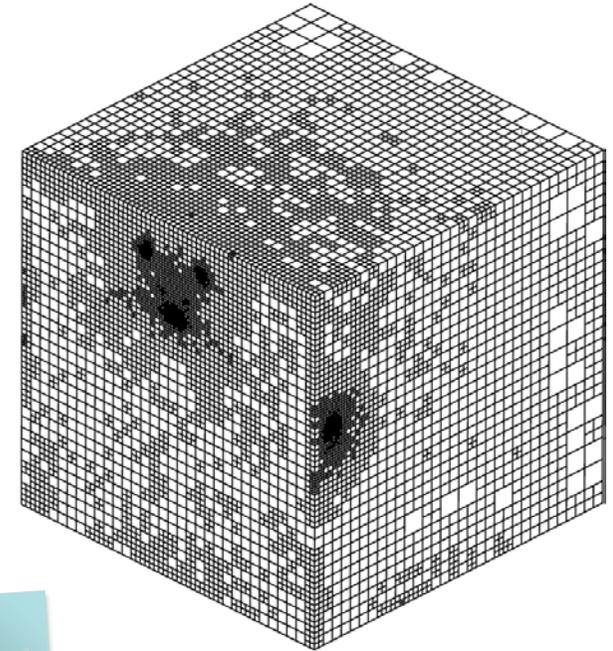


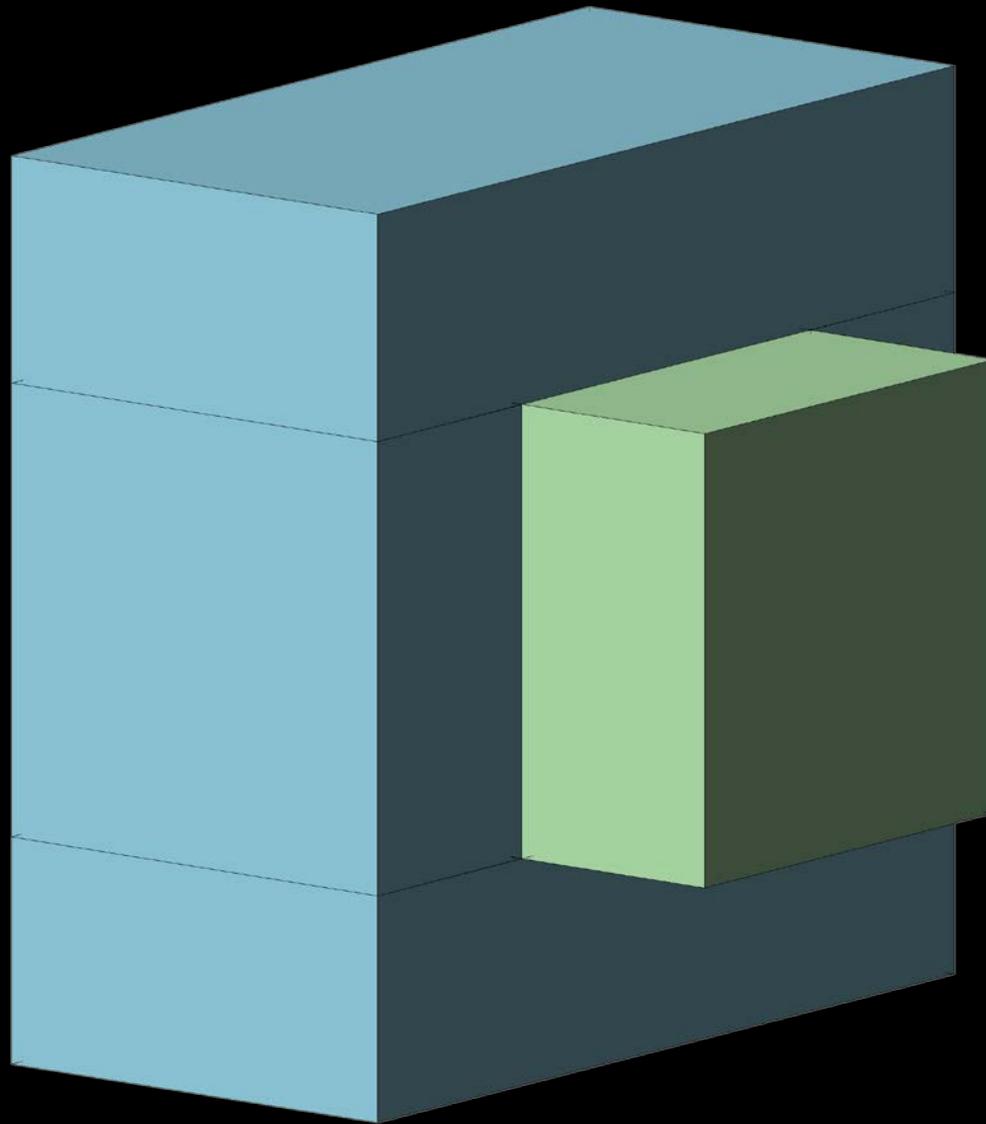
Meccano Method for Complex Solids

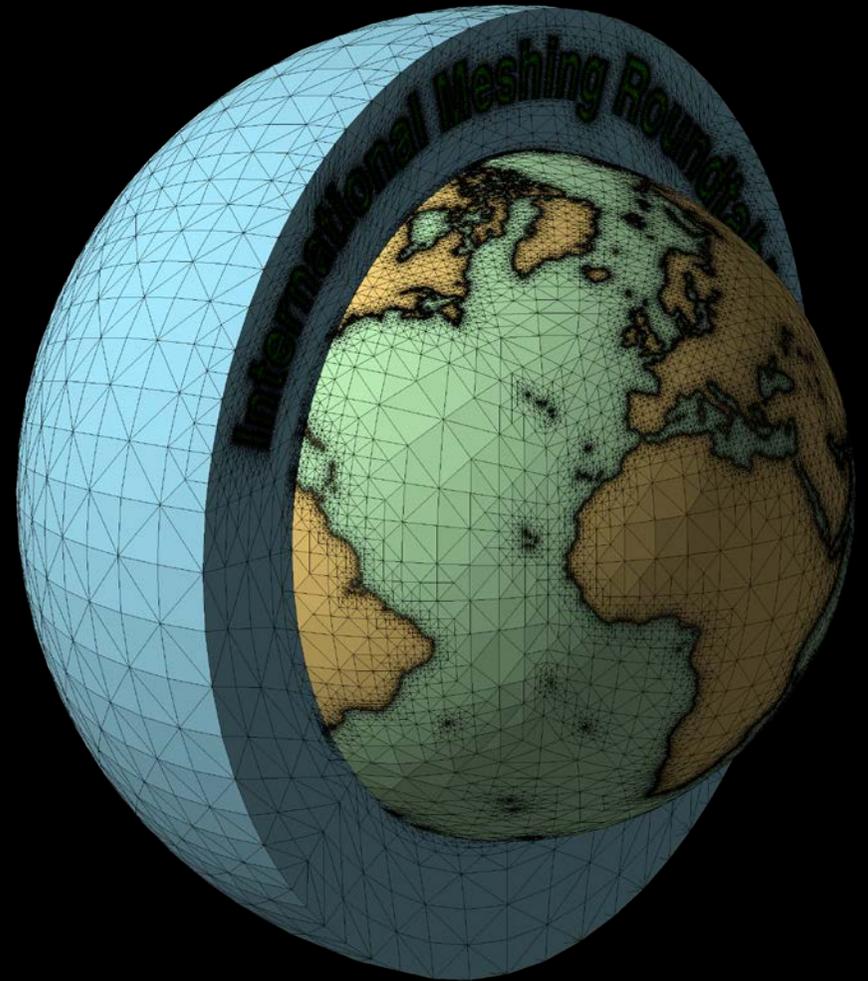
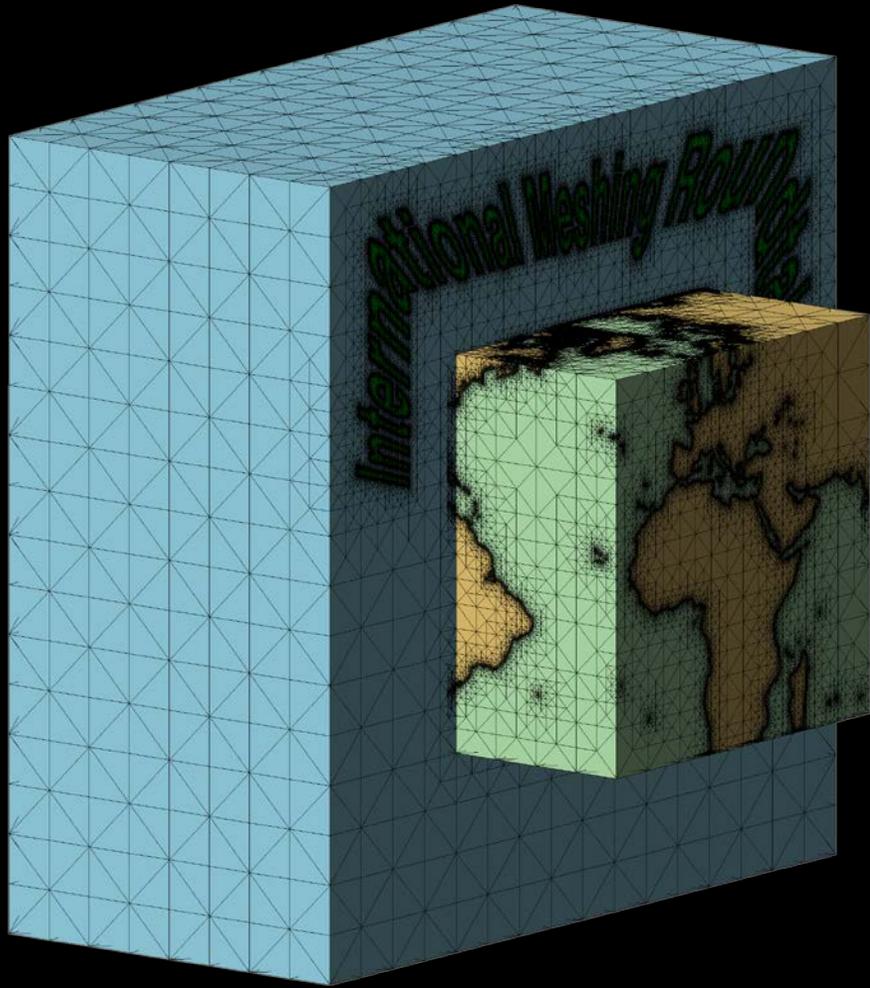
Volume parameterization based on SUS of tetrahedral meshes

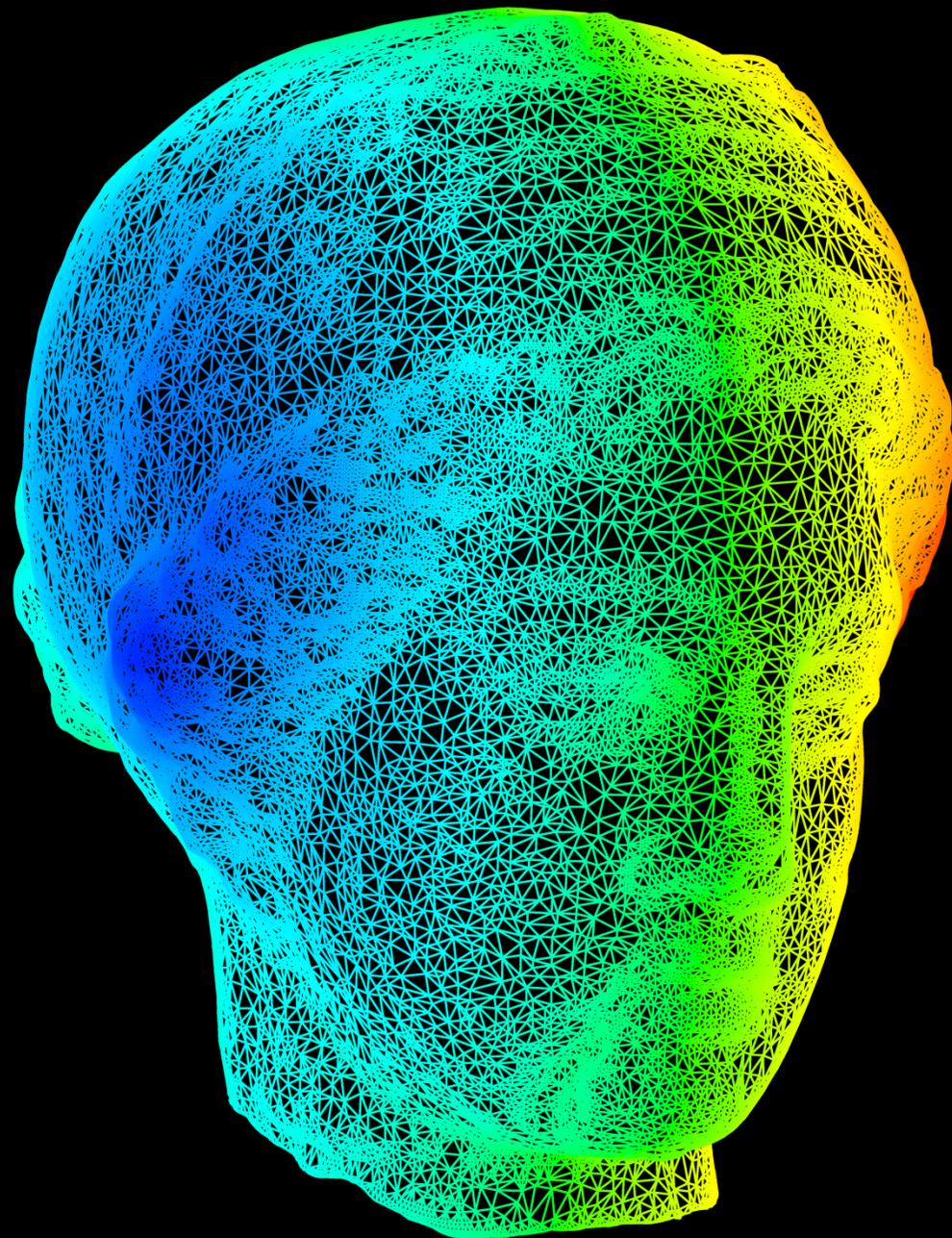


- Octree subdivision



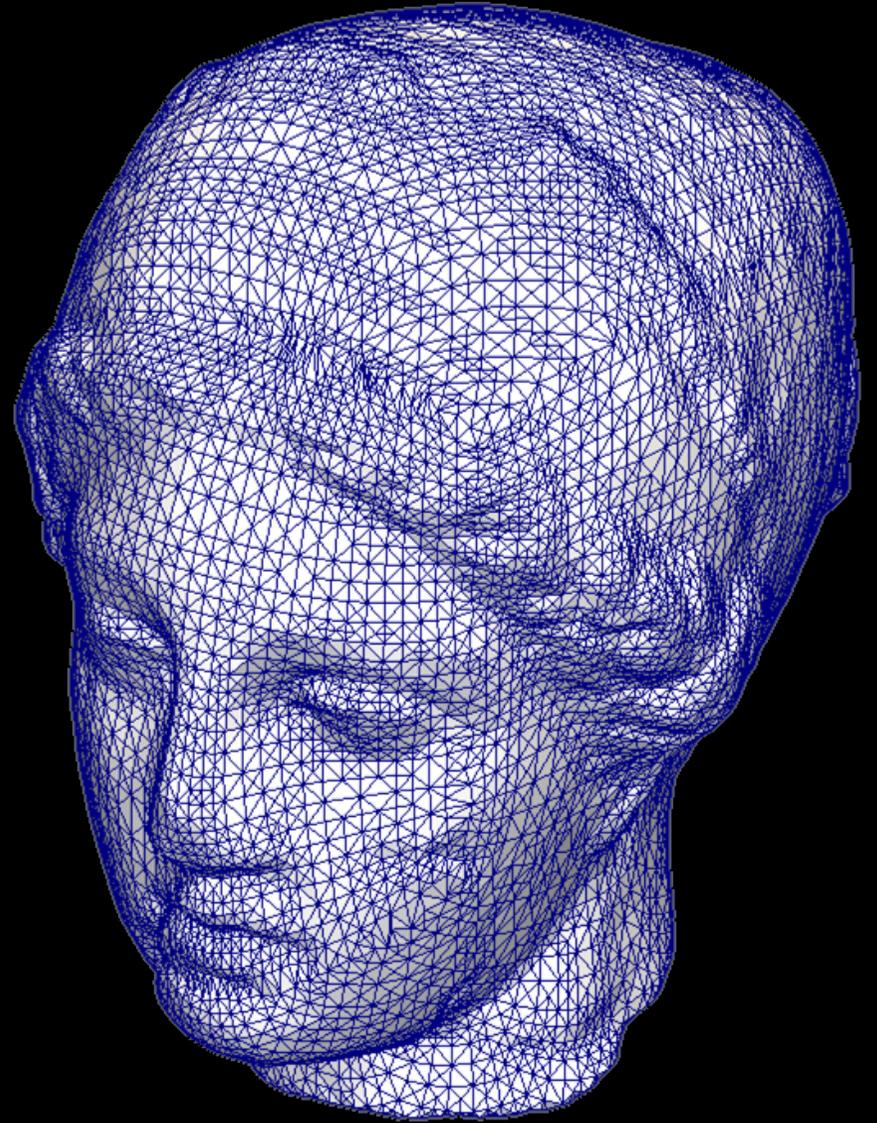
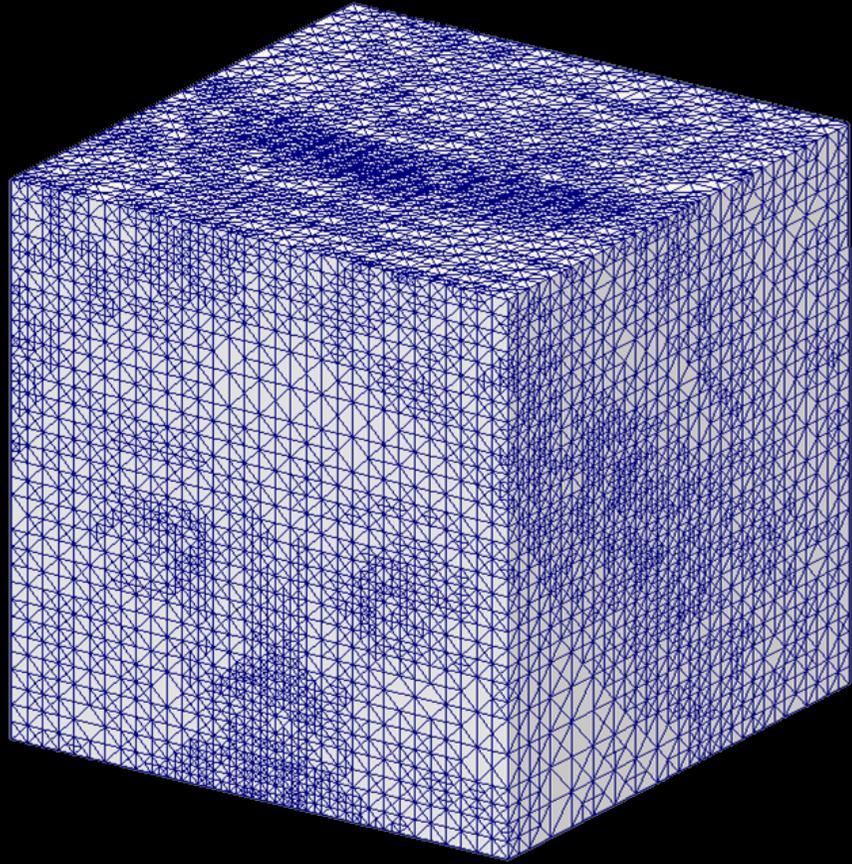






INPUT DATA: Surface Triangulation

<http://www.cyberware.com/>



Adaptive Isogeometric Refinement (EWC 2012)

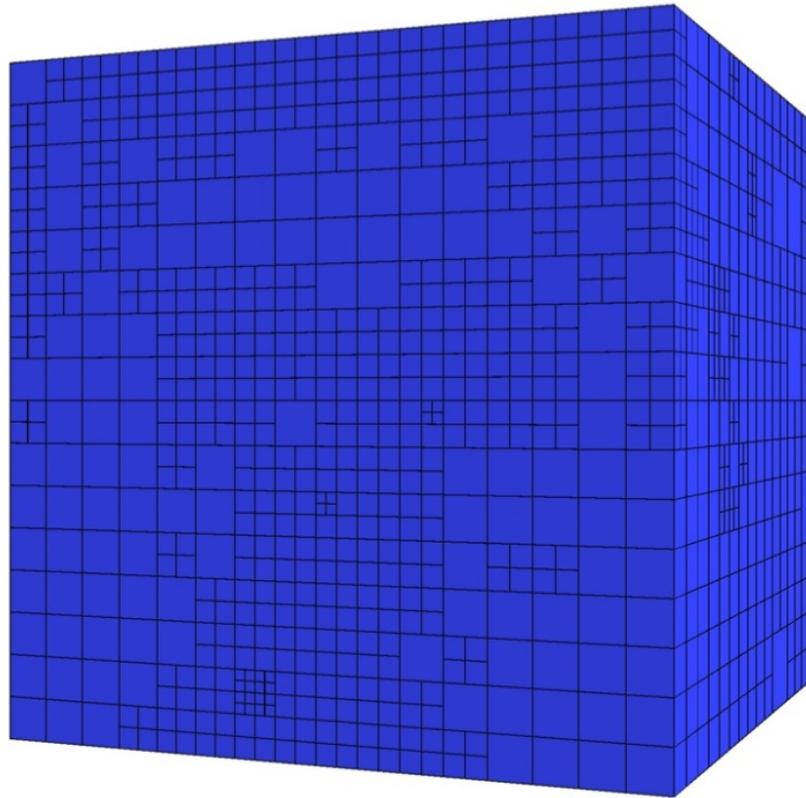
Application in Igea: Poisson problem with a central source

$$\Delta u = \frac{1}{25} e^{-\frac{(x^2+y^2+z^2)}{10}} (-15 + x^2 + y^2 + z^2) \quad \text{in } \Omega$$

$$u|_{\partial\Omega} = 0$$

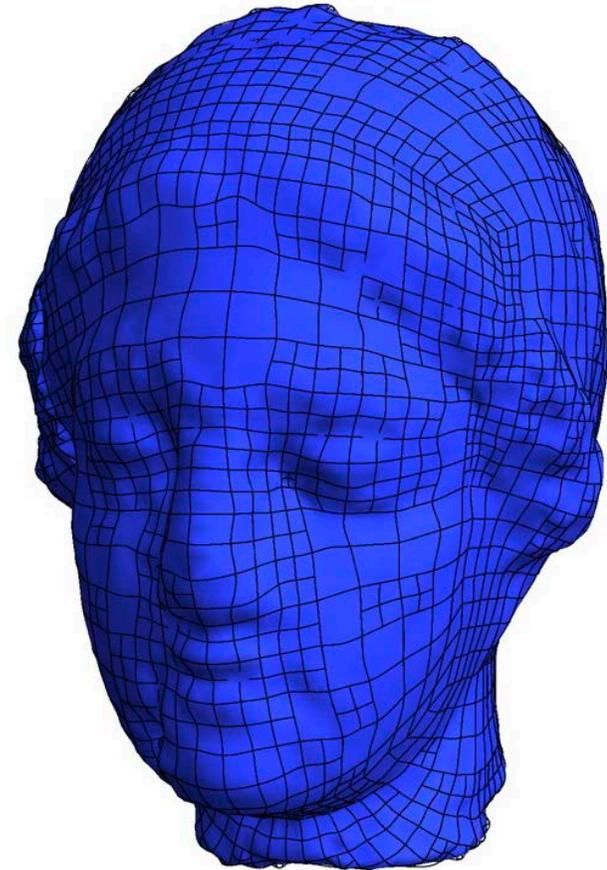
Exact solution:

$$u \approx e^{-\frac{(x^2+y^2+z^2)}{10}}$$



T-mesh

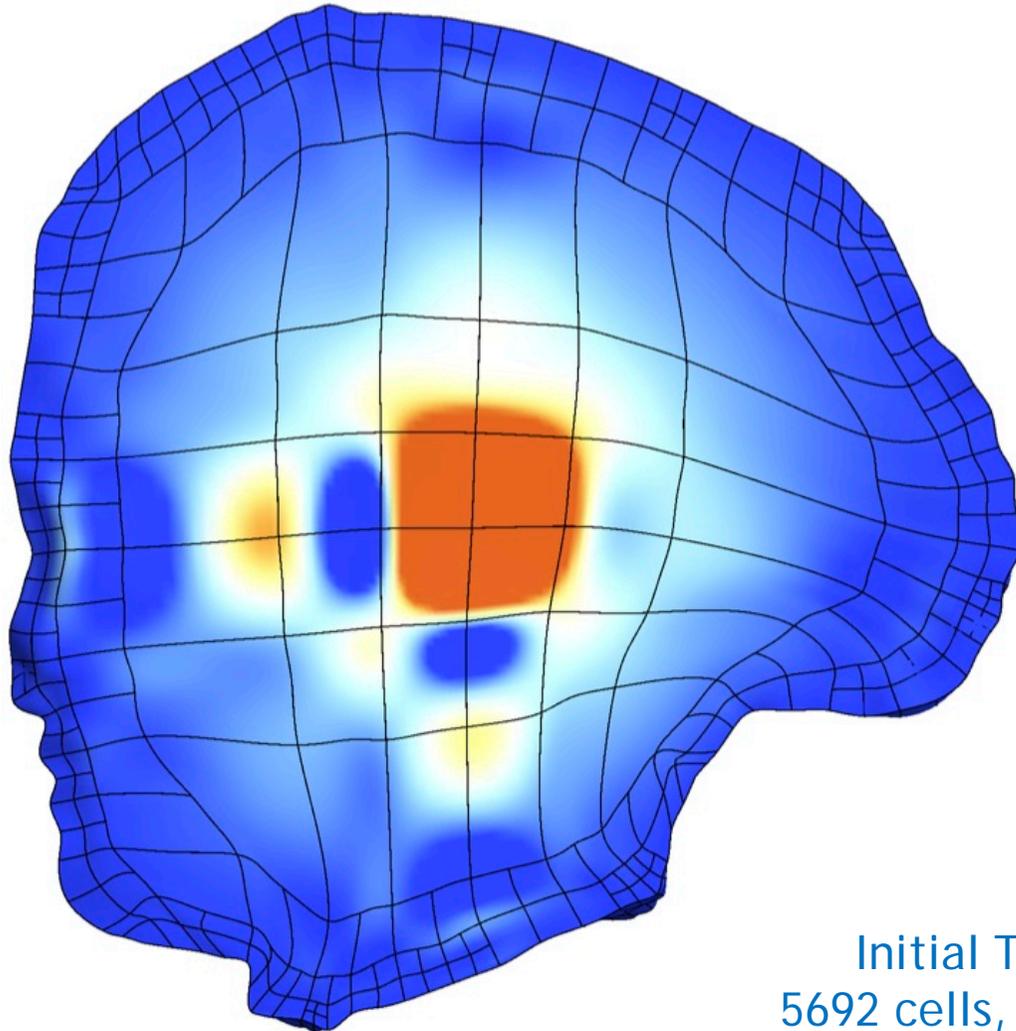
$S(\xi)$



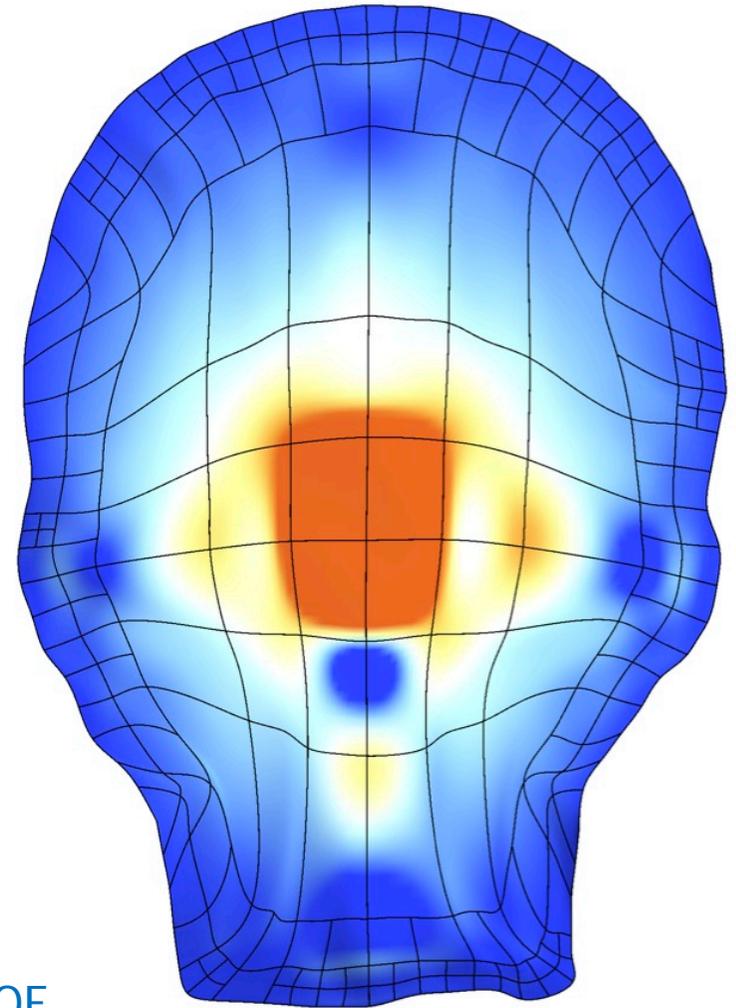
T-spline

Adaptive Isogeometric Refinement (EWC 2012)

Igea: T-spline of Numerical Solution



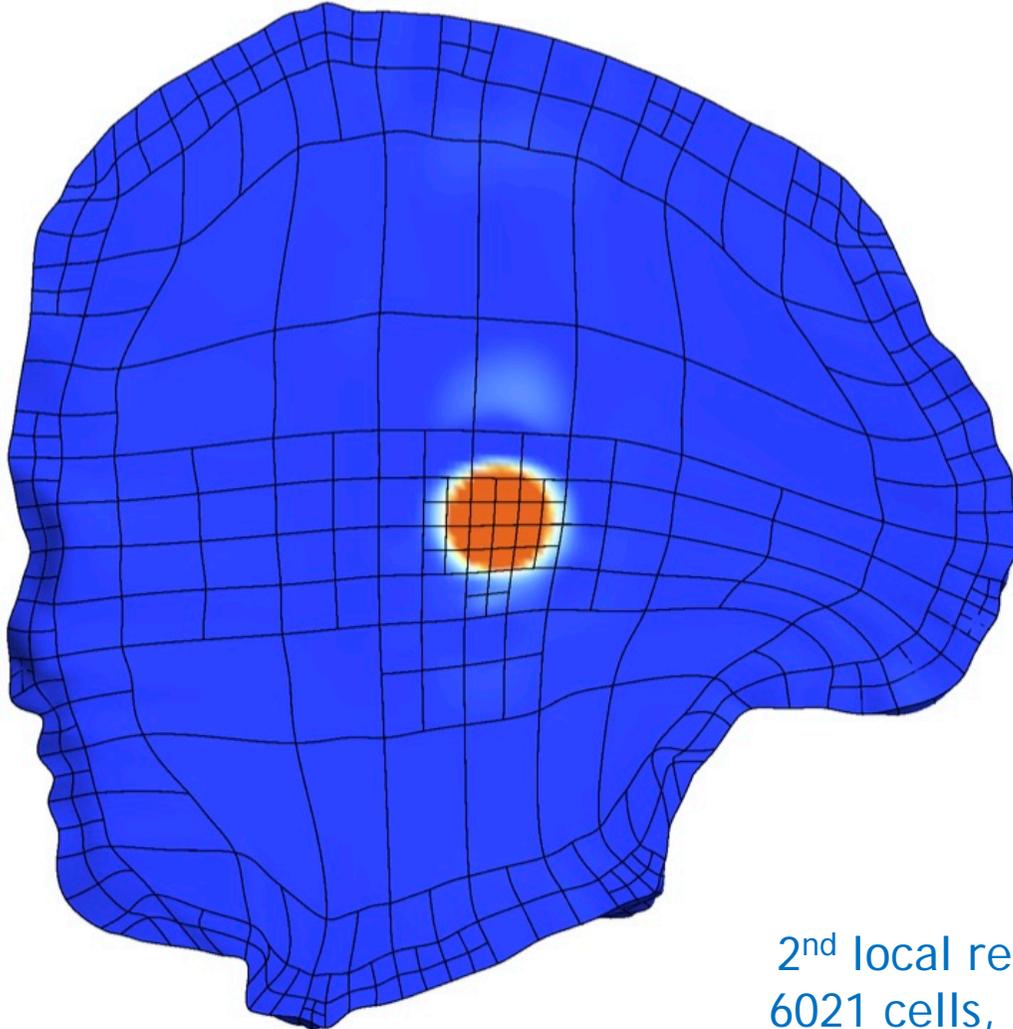
Initial T-mesh
5692 cells, 9304 DOF



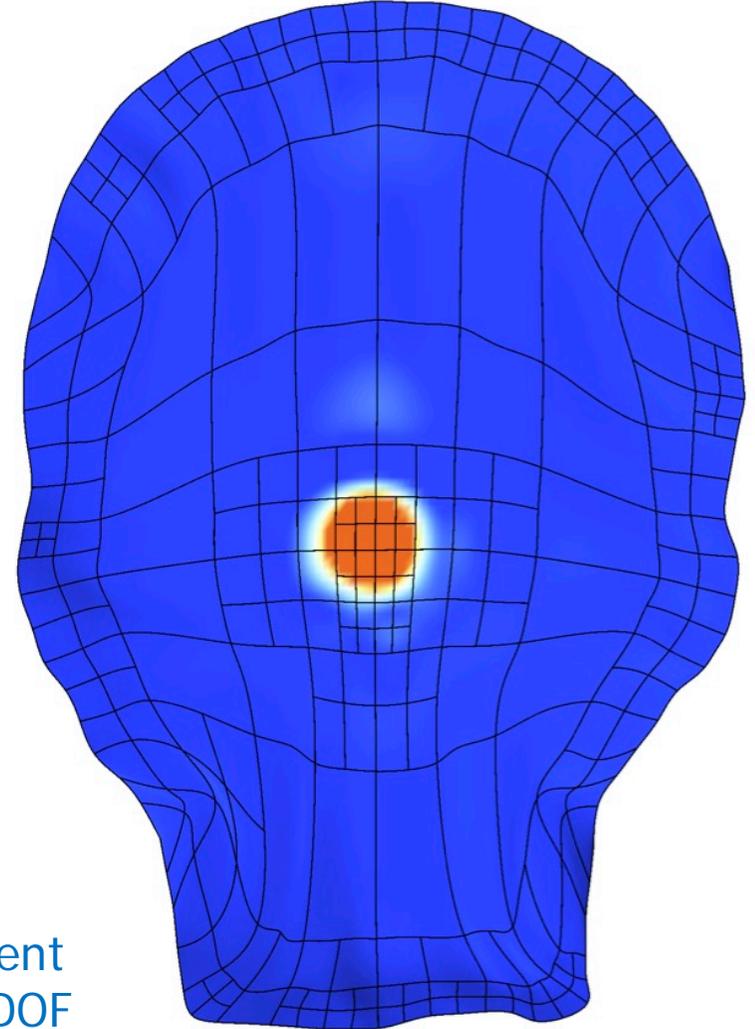
Adaptive Isogeometric Refinement (EWC 2012)

Igea: T-spline of Numerical Solution

$$\text{Error indicator : } \eta(\Omega_e)^2 = \int_{\Omega_e} h^2 (f + \Delta u_h)^2 d\Omega$$



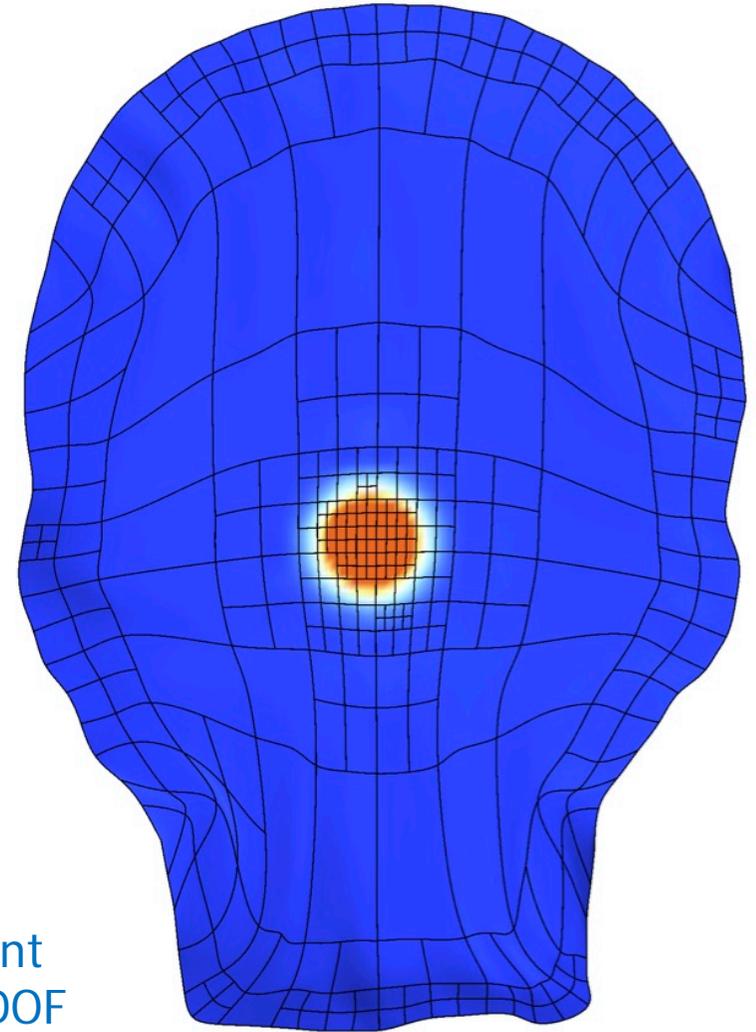
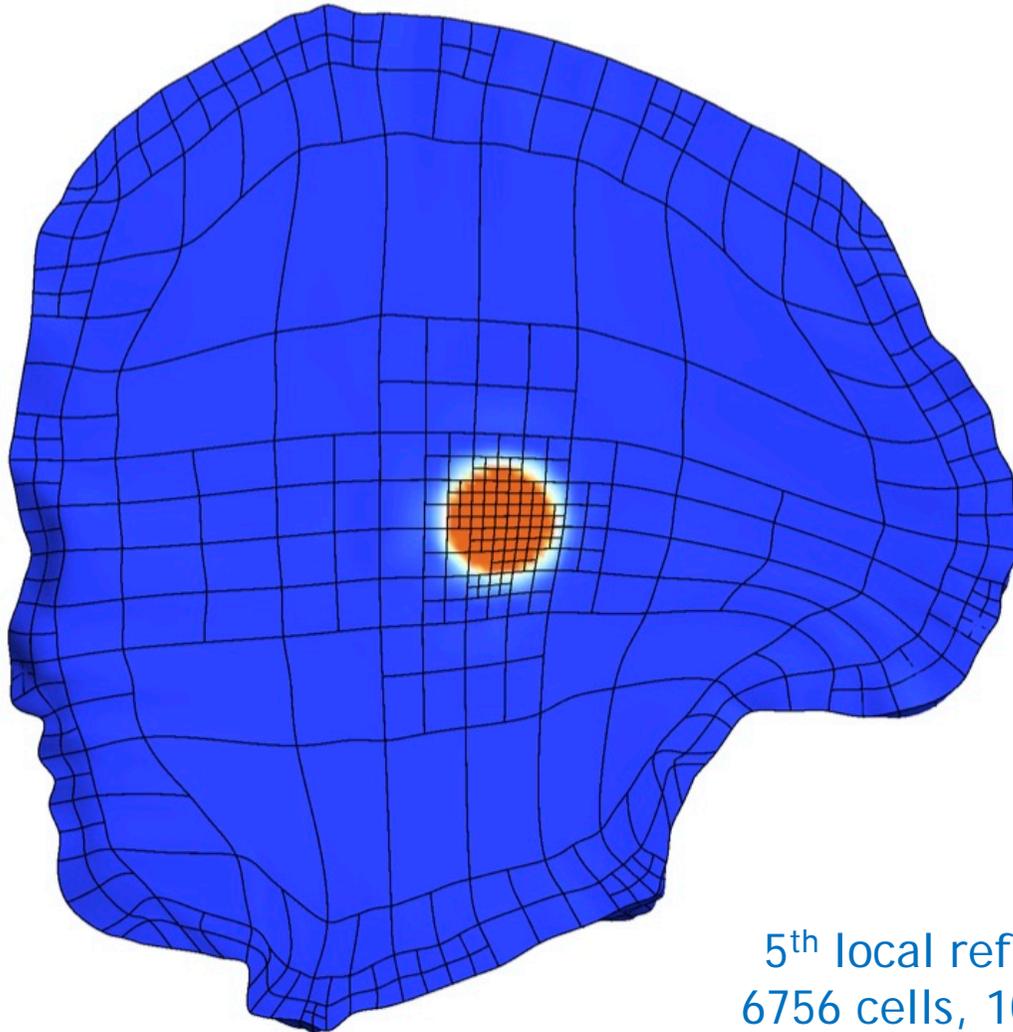
2nd local refinement
6021 cells, 9807 DOF



Adaptive Isogeometric Refinement (EWC 2012)

Igea: T-spline of Numerical Solution

$$\text{Error indicator : } \eta(\Omega_e)^2 = \int_{\Omega_e} h^2 (f + \Delta u_h)^2 d\Omega$$



5th local refinement
6756 cells, 10838 DOF

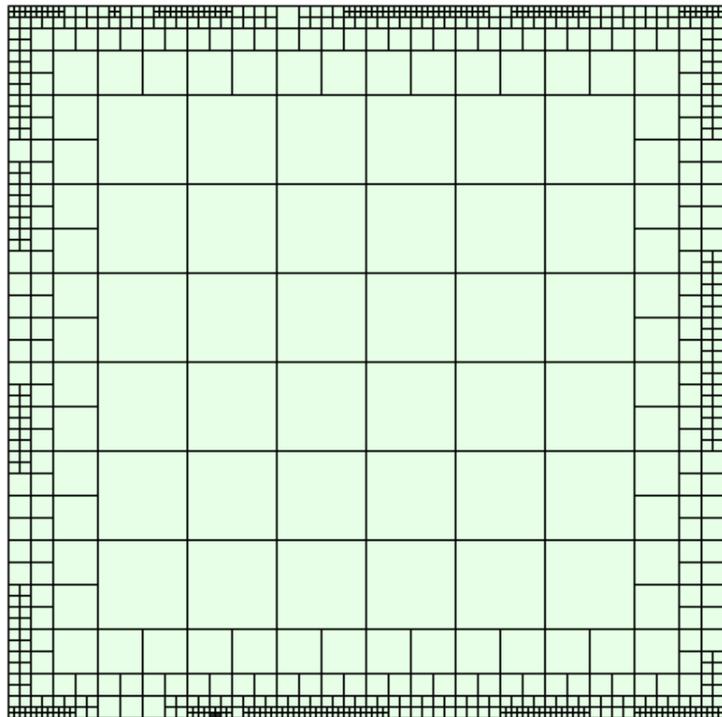
1. The key of the meccano method is the simultaneous untangling and smoothing (SUS) procedure.
2. The quality of the T-spline mapping (i.e., positive Jacobian, good uniformity and orthogonality of the isoparametric curves) depends on the quality of the T-mesh in the physical space. We have to fix a quality metric for this mapping.
3. In order to simplify the procedure and to get less distortion in the volume parameterization, it should be interesting to **directly apply the meccano method on T-meshes instead of tetrahedral meshes.**
4. We have started analysing the problem in 2-D.

The Meccano Method on T-meshes in 2-D

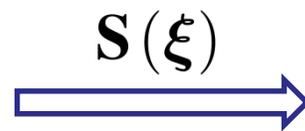
Input data: Boundary representation of the object

Objective: Construction of a high quality T-spline parameterization

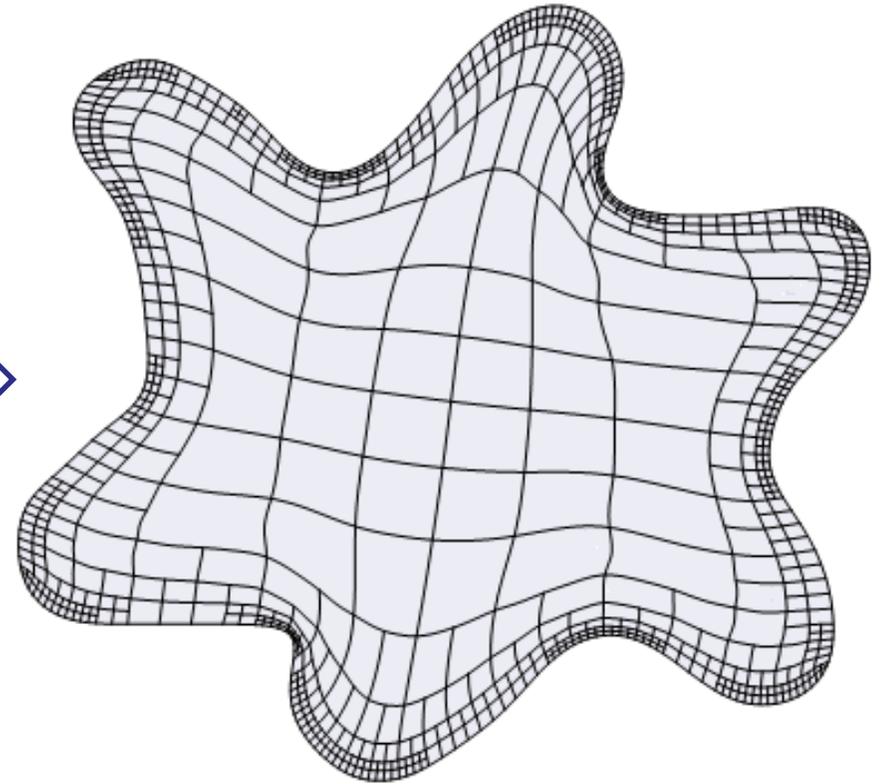
T-mesh



Parameter space



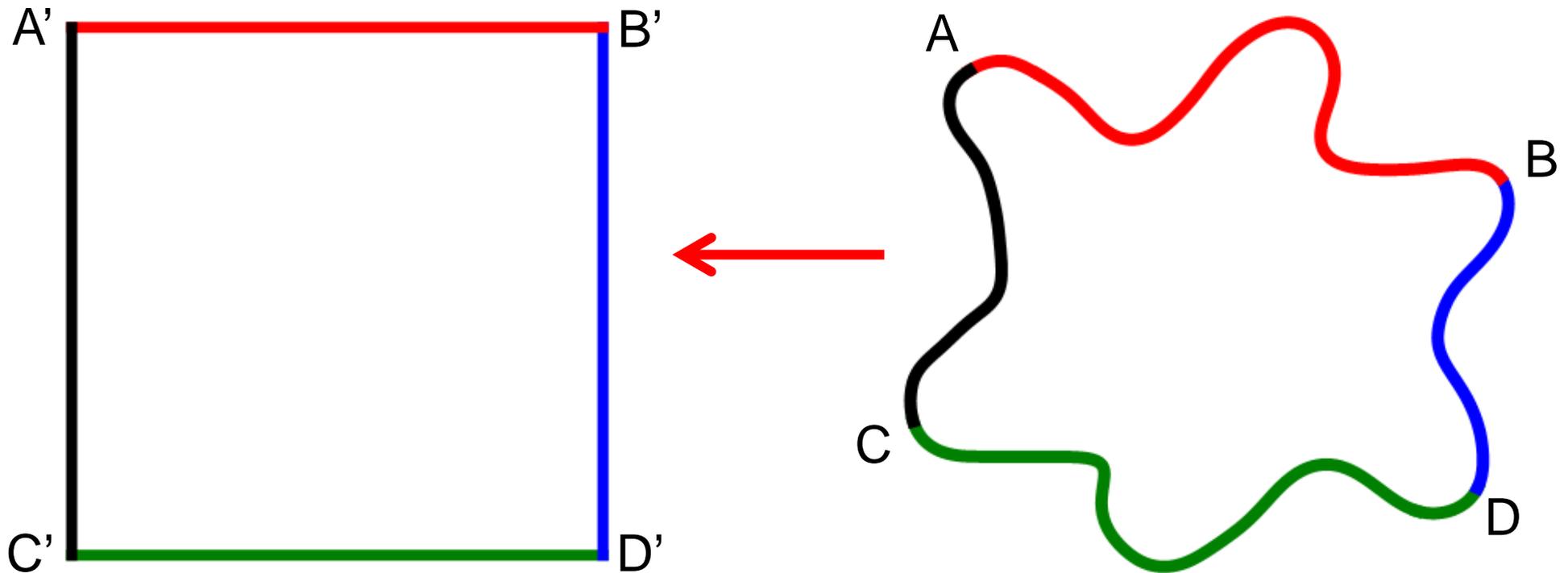
T-spline mesh



Physical space

The Meccano Method on T-meshes in 2-D

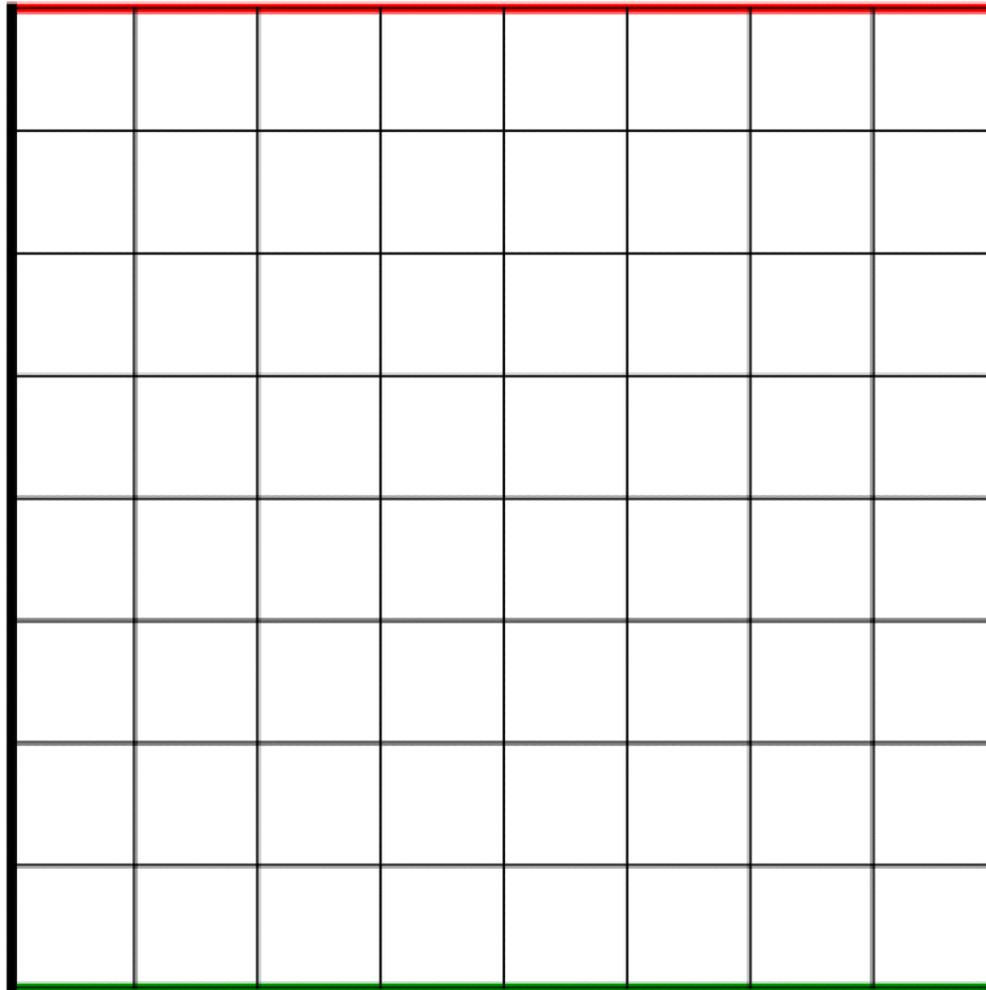
Step 1: Input boundary (image, polyline, curve, etc.) and boundary mapping



- Select four points (A, B, C, D) of the input boundary
- Boundary parameterization via chord-length

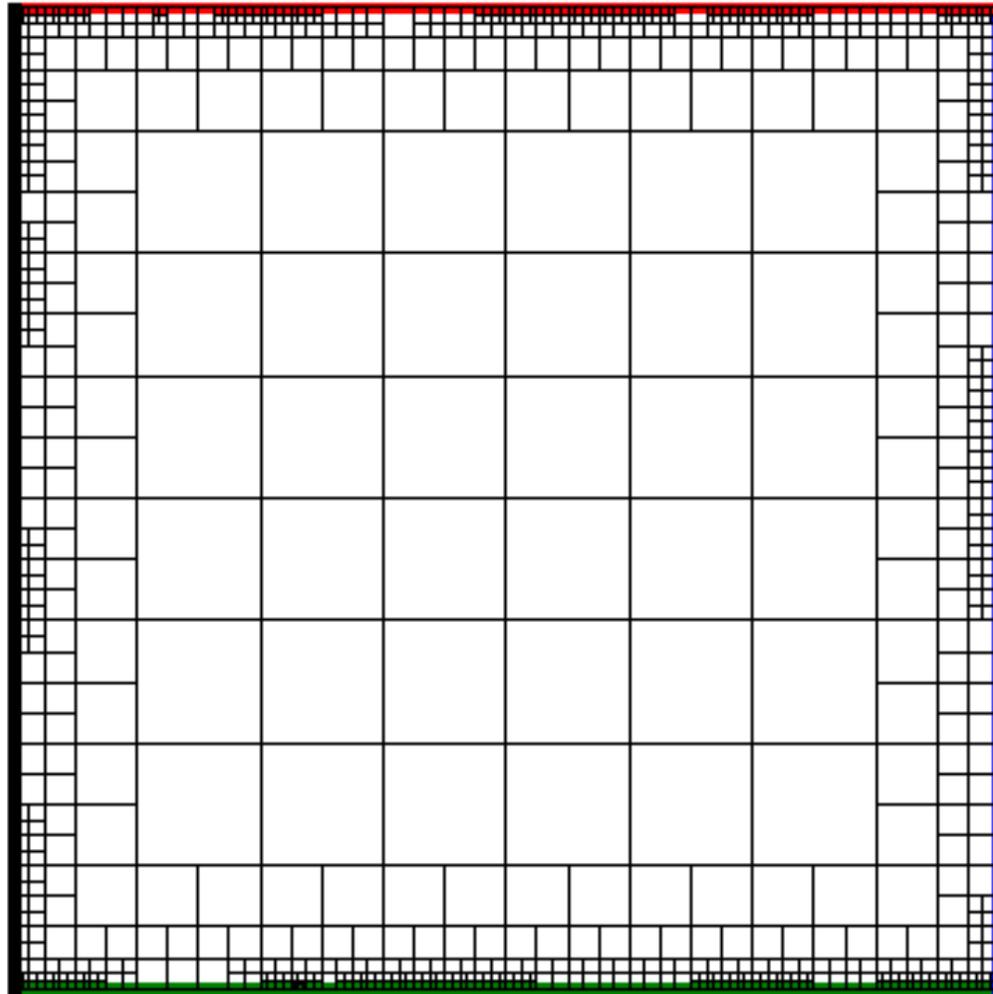
The Meccano Method on T-meshes in 2-D

Step 2: Coarse quadrilateral mesh of the meccano (parameter space)



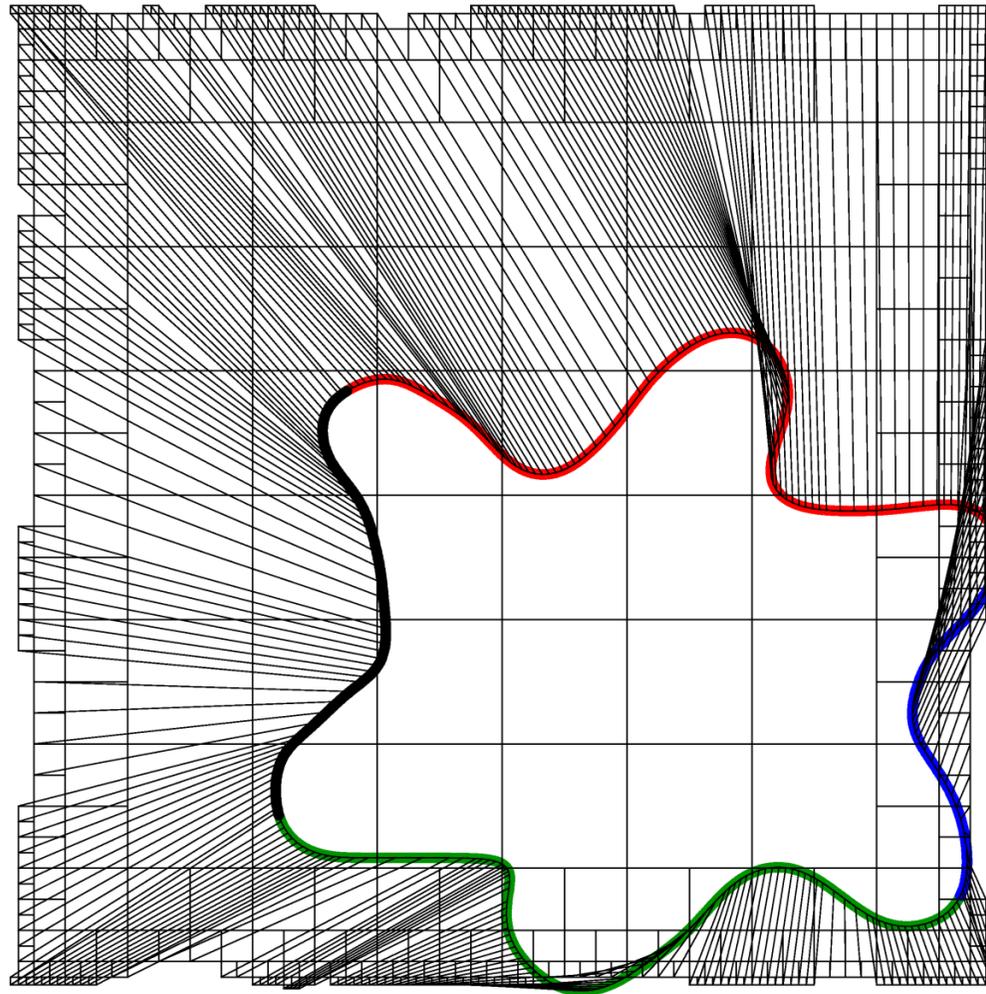
The Meccano Method on T-meshes in 2-D

Step 3: Refine mesh with quadtree subdivisions to approach the boundary



The Meccano Method on T-meshes in 2-D

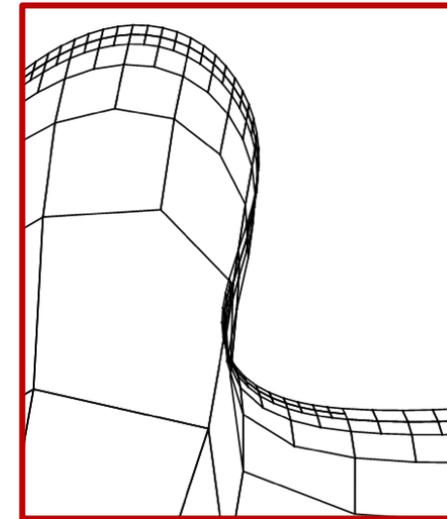
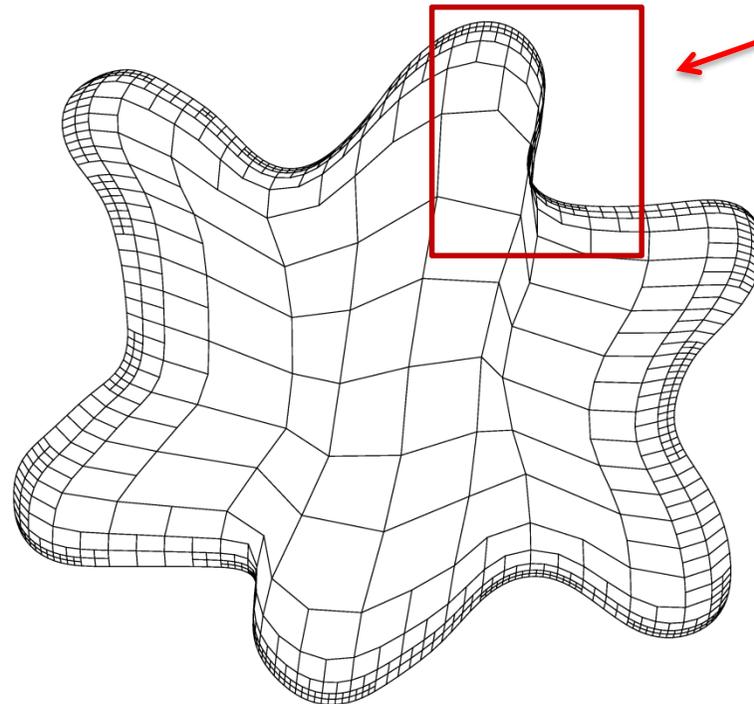
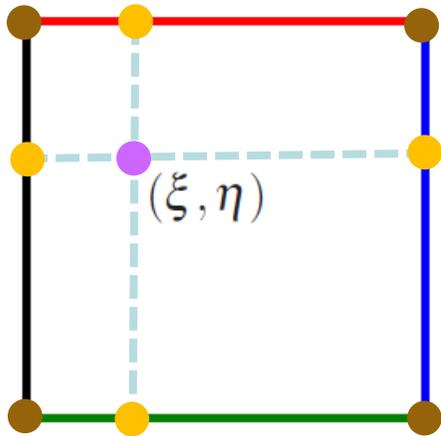
Step 4: Move the meccano boundary nodes to the object boundary



The Meccano Method on T-meshes in 2-D

Step 5: Inner node relocation with Coons patch to facilitate the optimization

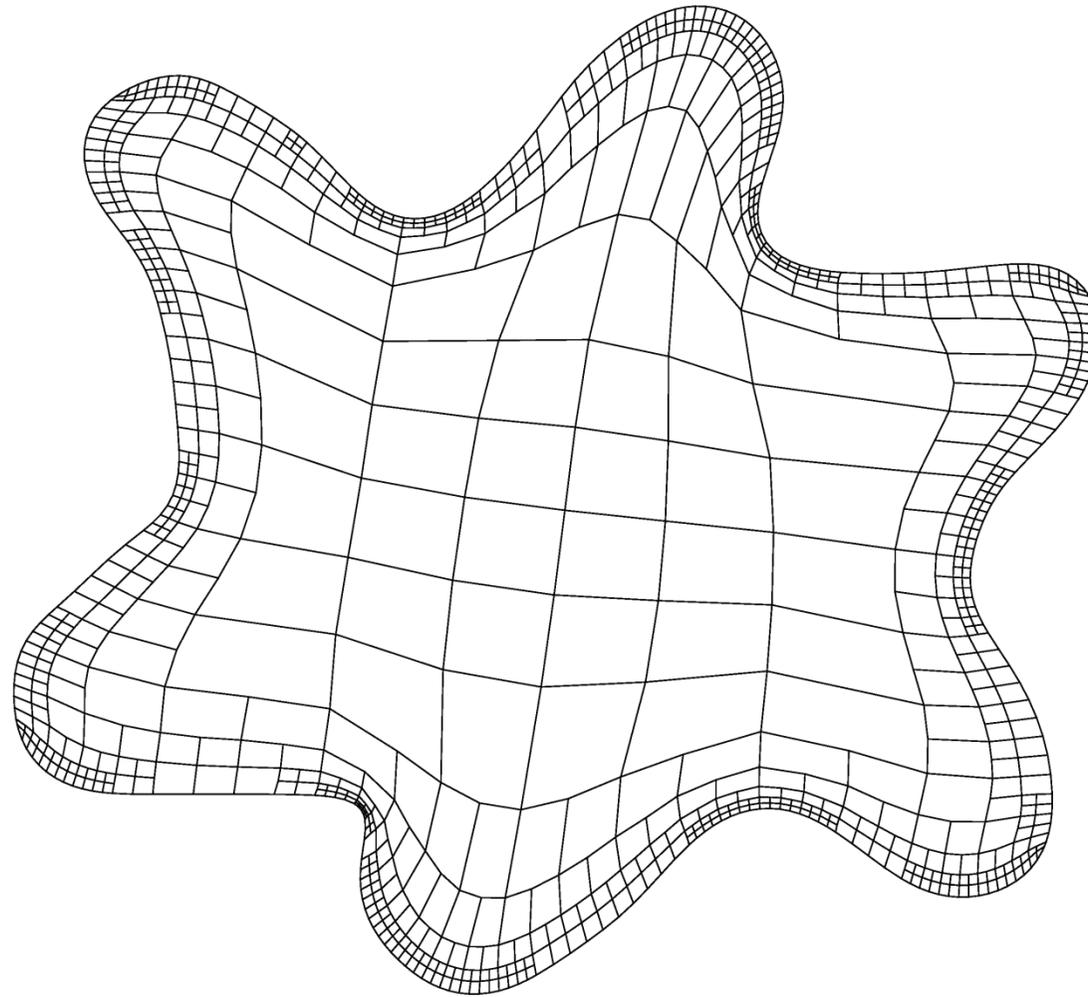
$$\begin{aligned} \mathbf{x}(\xi, \eta) &= (1 - \xi)\mathbf{x}(0, \eta) + \xi\mathbf{x}(1, \eta) \\ &+ (1 - \eta)\mathbf{x}(\xi, 0) + \eta\mathbf{x}(\xi, 1) \\ &- [1 - \xi \ \xi] \begin{bmatrix} \mathbf{x}(0, 0) & \mathbf{x}(0, 1) \\ \mathbf{x}(1, 0) & \mathbf{x}(1, 1) \end{bmatrix} \begin{bmatrix} 1 - \eta \\ \eta \end{bmatrix} \end{aligned}$$



Mesh folder

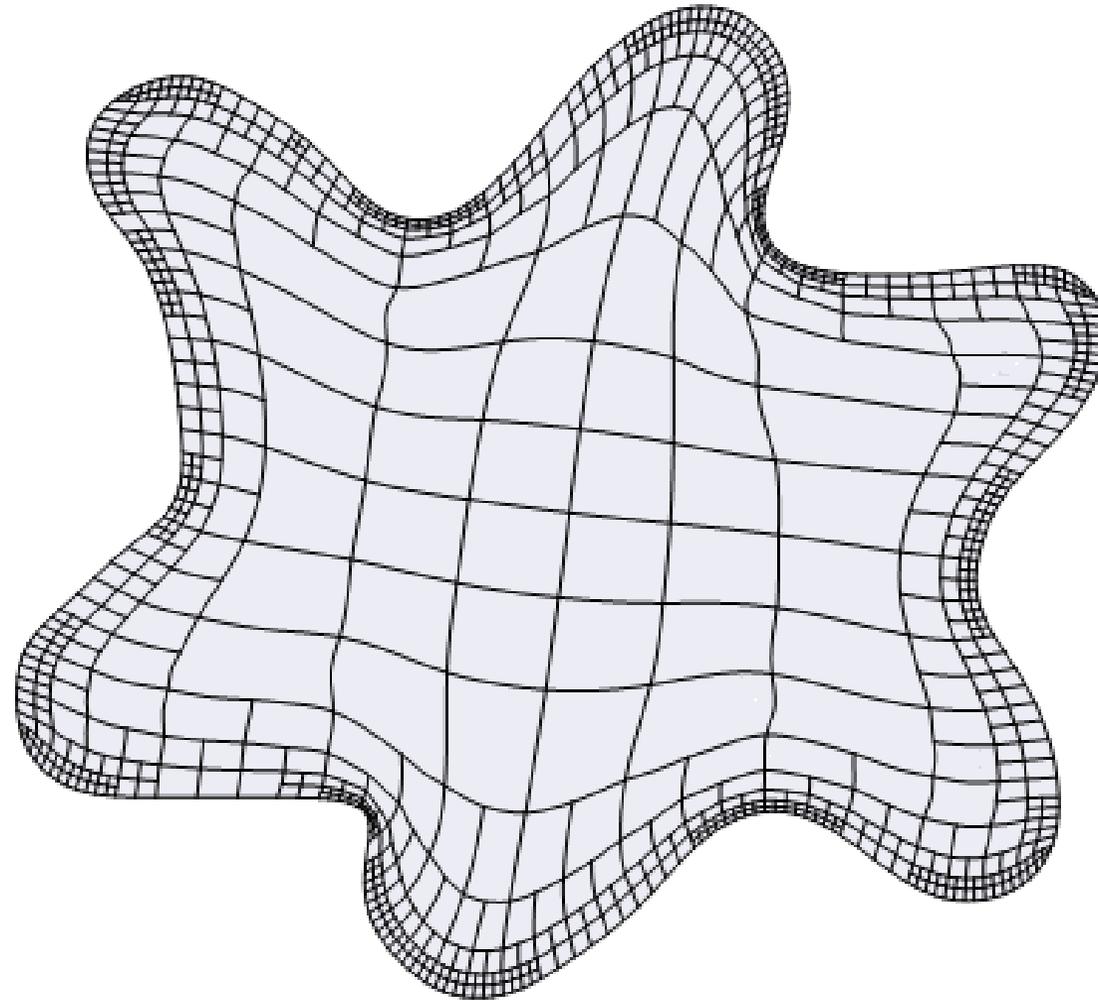
The Meccano Method on T-meshes in 2-D

Step 6: Simultaneous Untangling and Smoothing (SUS) of the T-mesh



The Meccano Method on T-meshes in 2-D

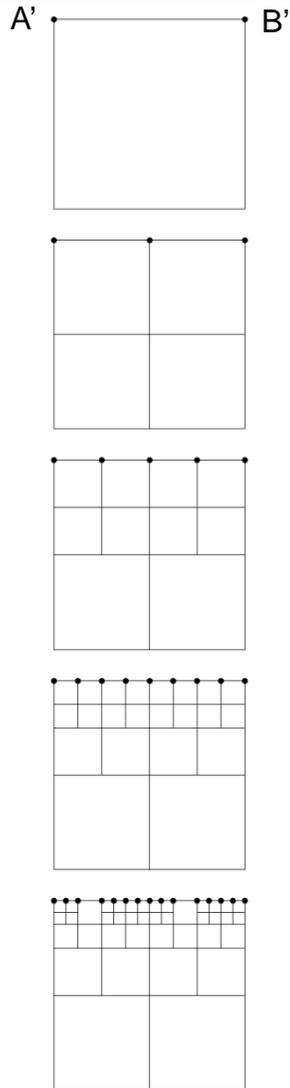
Step 7: T-spline representation of the spot



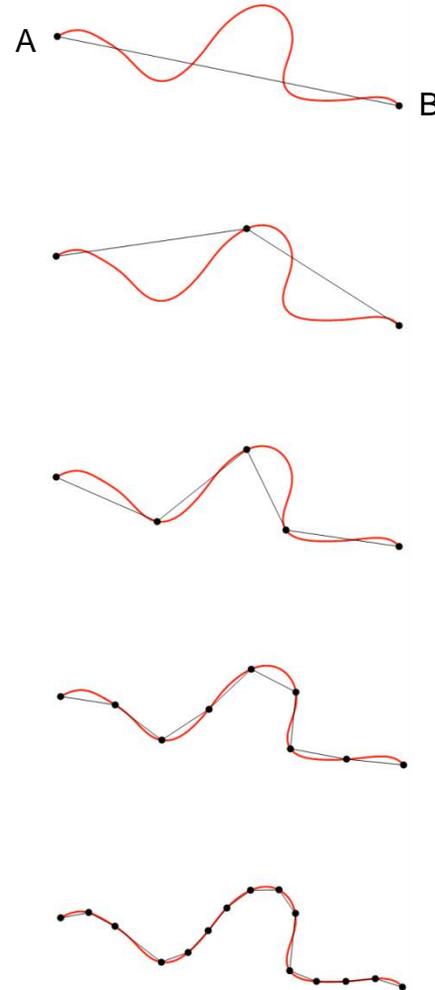
Boundary Approach in 2-D

Input data: Boundary polyline approximation (red color line)

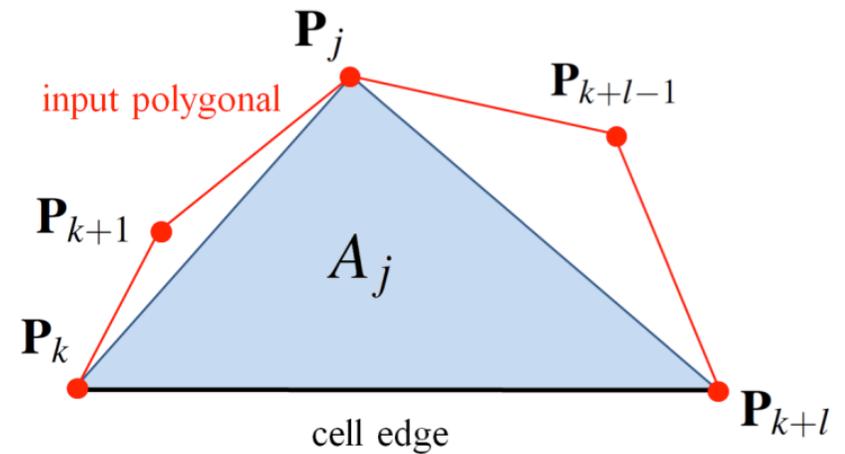
T-mesh adaptation in parameter space



Boundary approximation in physical space



Boundary edge refinement criterion:



$$\exists j : A_j > \varepsilon \Rightarrow \text{refine}$$

$$A_j = \text{Area}(\mathbf{P}_k, \mathbf{P}_j, \mathbf{P}_{k+l})$$

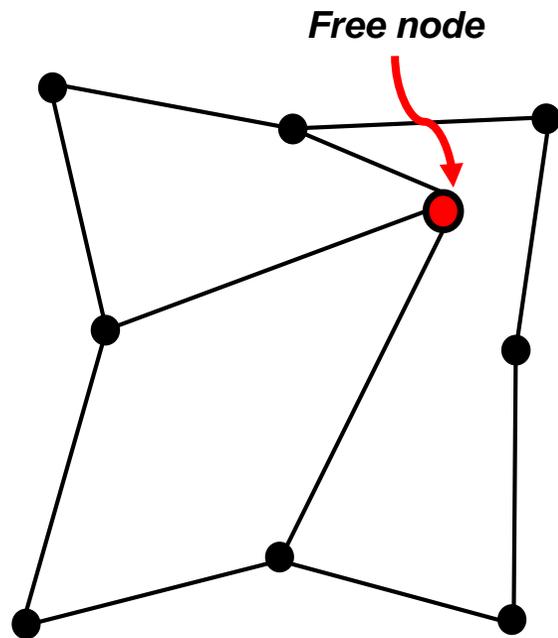
$$k+1 \leq j \leq k+l-1$$

Simultaneous Untangling and Smoothing

Case of plane T-meshes (EWC 2013)

Local optimization

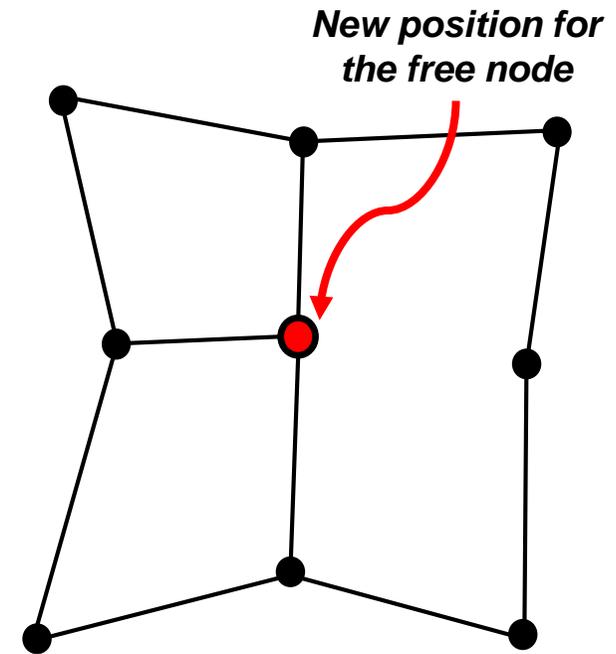
Objective: Improve the quality of the local mesh by minimizing an objective function



Local mesh



?



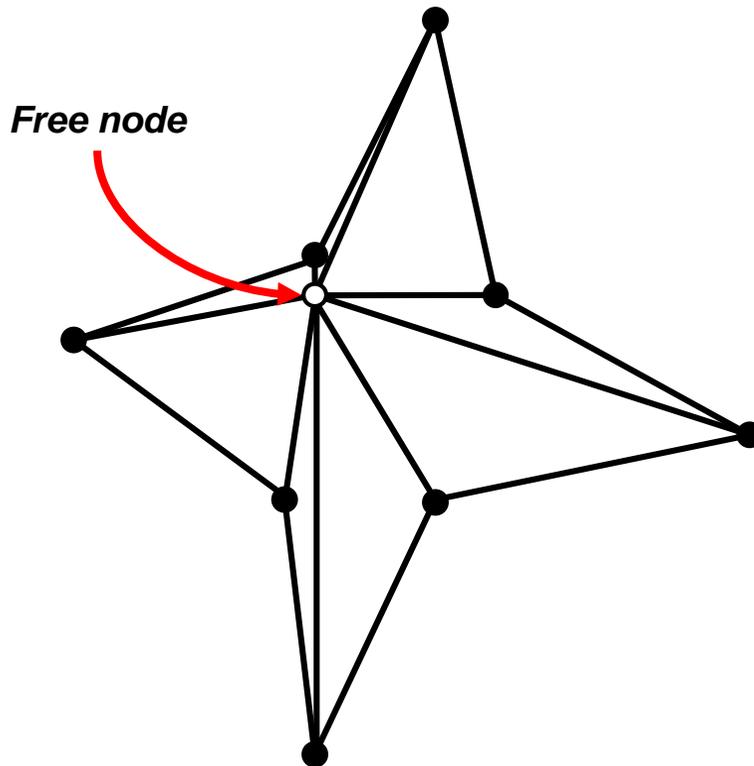
Optimized local mesh

Simultaneous Untangling and Smoothing

Case of plane triangulations (CMAME 2003)

Local optimization

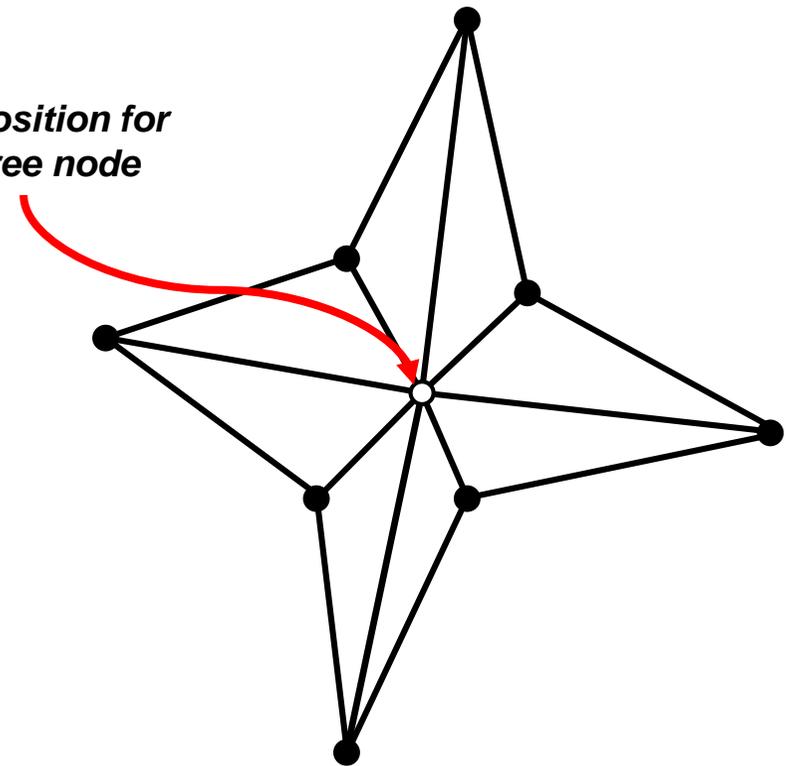
Objective: Improve the quality of the local mesh by minimizing an objective function



Local mesh



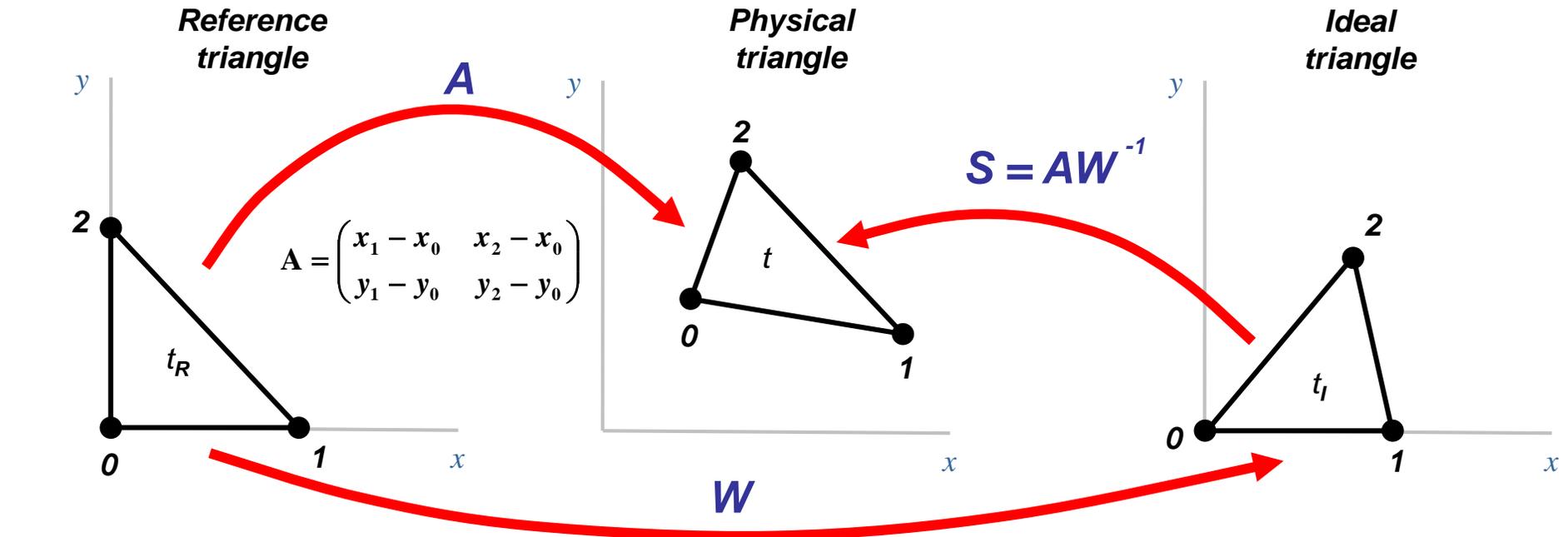
New position for the free node



Optimized local mesh

Simultaneous Untangling and Smoothing (CMAME 2003)

Weighted Jacobian Matrix on a Plane



$t_I \xrightarrow{S} t$ $S = AW^{-1}$: Weighted Jacobian matrix

*An algebraic quality metric of t
(mean ratio)*

$$q = \frac{2\sigma}{\|S\|^2} = \frac{1}{\eta}$$

where: $\|S\| = \sqrt{\text{tr}(S^T S)}$
 $\sigma = \det(S)$

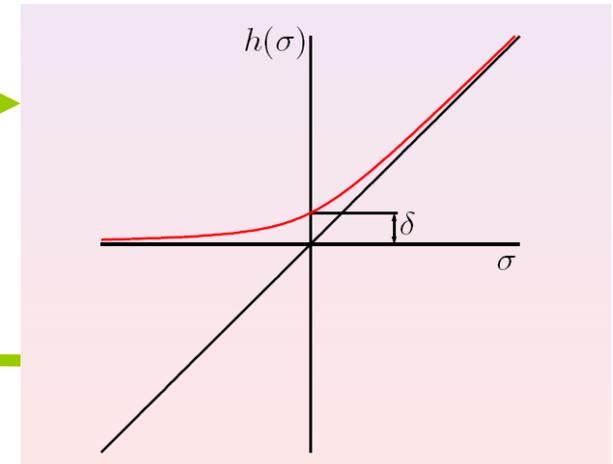
Simultaneous Untangling and Smoothing (CMAME 2003)

Local objective function for plane triangulations

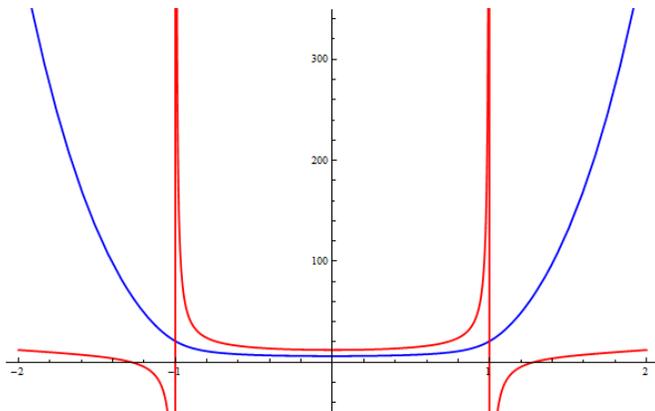
SUS Code: Freely-available in <http://www.dca.iusiani.ulpgc.es/proyecto2012-2014>

Original function: $K(\mathbf{x}) = \sum_{m=1}^M \frac{\|S_m\|^2}{2\sigma_m}$

Modified function: $K^*(\mathbf{x}) = \sum_{m=1}^M \frac{\|S_m\|^2}{2h(\sigma_m)}$



$$h(\sigma) = \frac{1}{2}(\sigma + \sqrt{\sigma^2 + 4\delta^2})$$

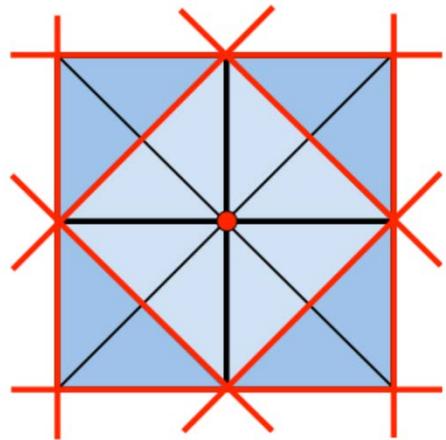
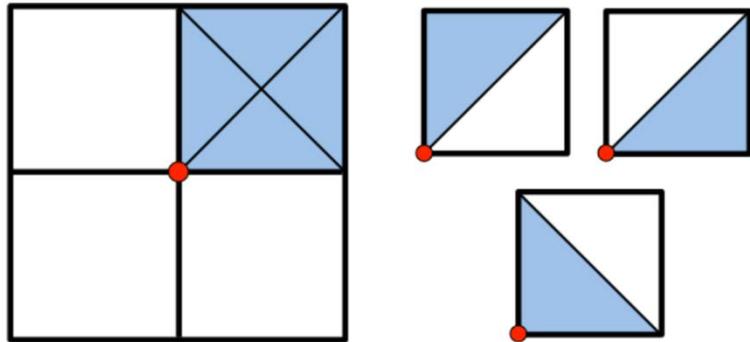


Modified function (blue) is regular in all \mathbb{R}^2 and it approximates the same minimum that the original function (red). Moreover, it allows a simultaneous untangling and smoothing of triangular meshes

Simultaneous Untangling and Smoothing of T-meshes

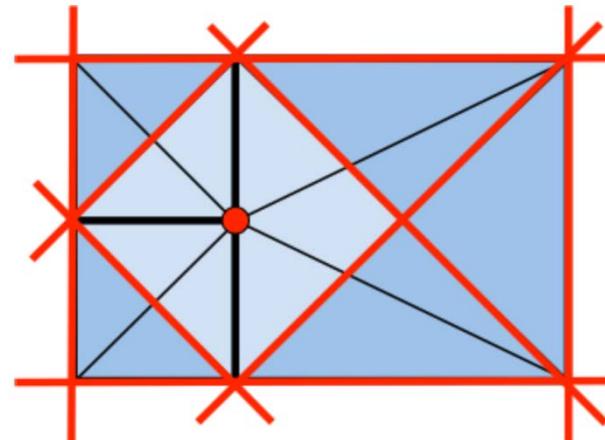
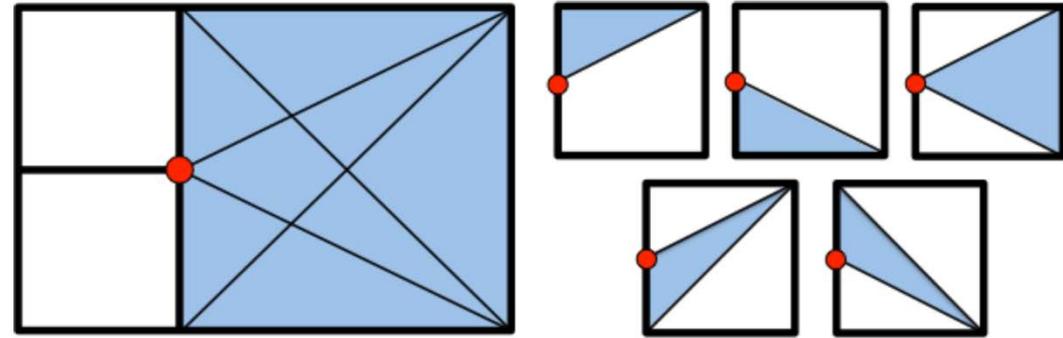
Triangle decomposition of the T-mesh cells

Case 1: Free node is a regular node



Barriers and feasible region for a regular node

Case 2: Free node is a hanging node

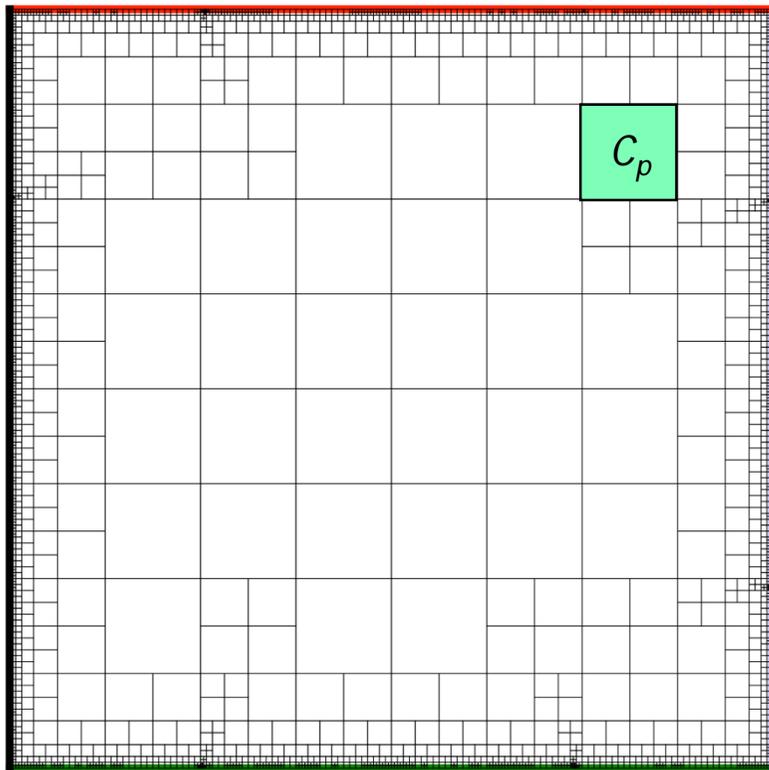


Barriers and feasible region for a hanging node

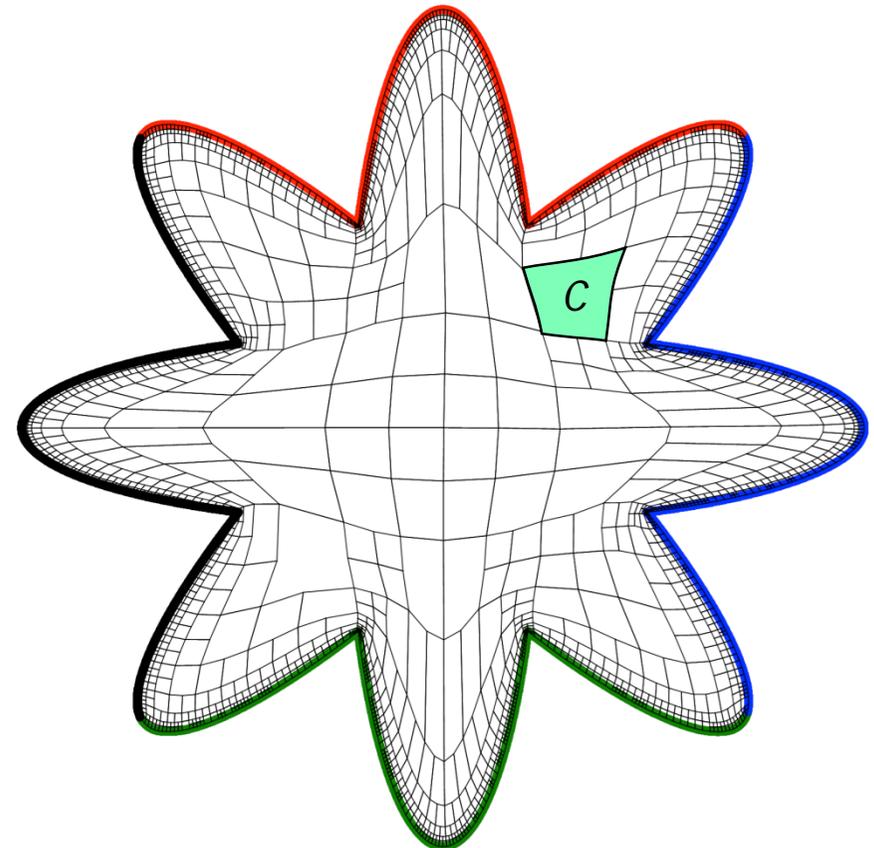
Simultaneous Untangling and Smoothing of T-meshes

Optimization is guided by the parametric T-mesh

Physical cell C must be as similar as possible to the counterpart in the parametric space C_p



Parametric T-mesh

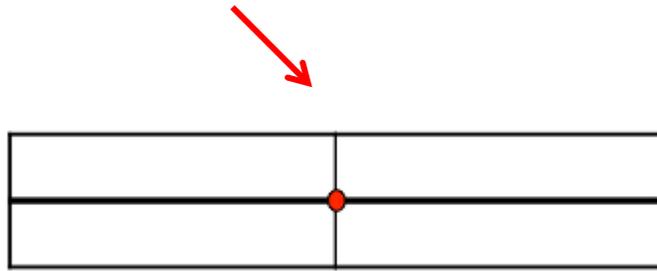


Optimized physical T-mesh

Simultaneous Untangling and Smoothing of T-meshes

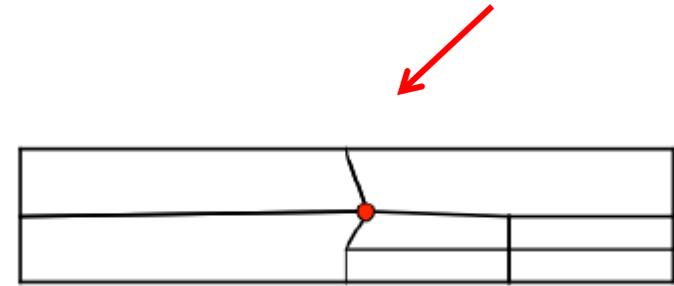
Problems appears with the non-weighted objective function K^*

*Satisfactory result for a conformal submesh using K^**



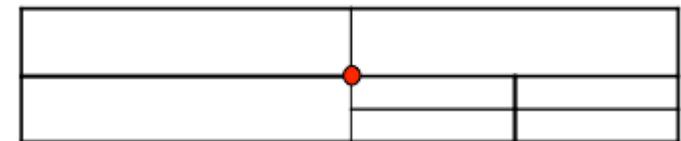
(a)

*Not satisfactory result for a non-conformal submesh using K^**



(b)

Desirable result: Orthogonal mesh for a non-conformal case (weighted objective function K_{τ}^)*



(c)

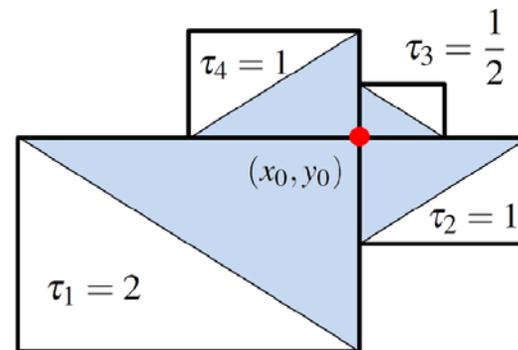
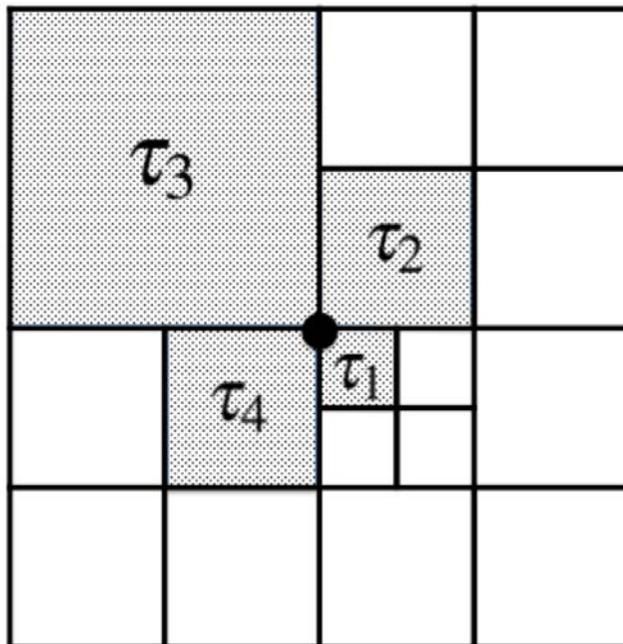
Simultaneous Untangling and Smoothing of T-meshes

Solution by using weighted objective functions (regular node)

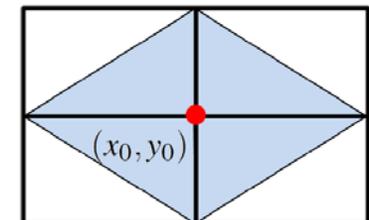
$$K_{\tau}^*(\mathbf{x}) = \tau_1 \sum_{m=1}^3 \frac{\|S_m\|^2}{2h(\sigma_m)} + \tau_2 \sum_{m=4}^6 \frac{\|S_m\|^2}{2h(\sigma_m)} + \tau_3 \sum_{m=7}^9 \frac{\|S_m\|^2}{2h(\sigma_m)} + \tau_4 \sum_{m=10}^{12} \frac{\|S_m\|^2}{2h(\sigma_m)}$$

All possible weights for balanced quadtrees:

$$\Rightarrow \tau_1 = 1, \tau_2 = \tau_4 = 2 \text{ y } \tau_3 = 4$$



Non-conformal mesh



Conformal mesh

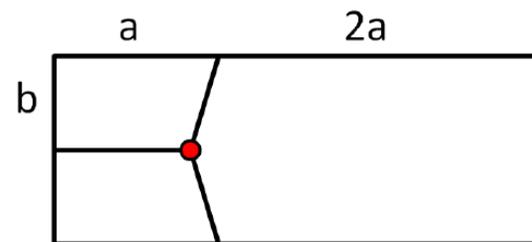
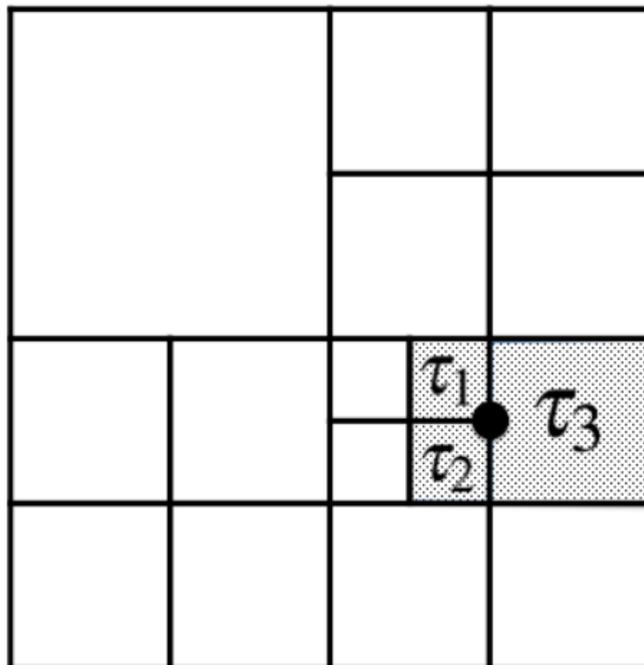
Simultaneous Untangling and Smoothing of T-meshes

Solution by using weighted objective functions (hanging node)

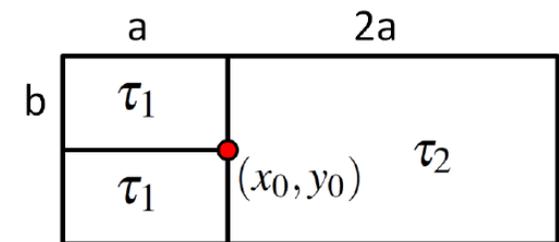
$$K_{\tau}^*(\mathbf{x}) = \tau_1 \sum_{m=1}^3 \frac{\|S_m\|^2}{2h(\sigma_m)} + \tau_2 \sum_{m=4}^6 \frac{\|S_m\|^2}{2h(\sigma_m)} + \tau_3 \sum_{m=7}^{11} \frac{\|S_m\|^2}{2h(\sigma_m)}$$

All possible weights for balanced quadtrees:

$$\longrightarrow \tau_1 = \tau_2 = 1 \text{ y } \tau_3 = \frac{8}{5}$$



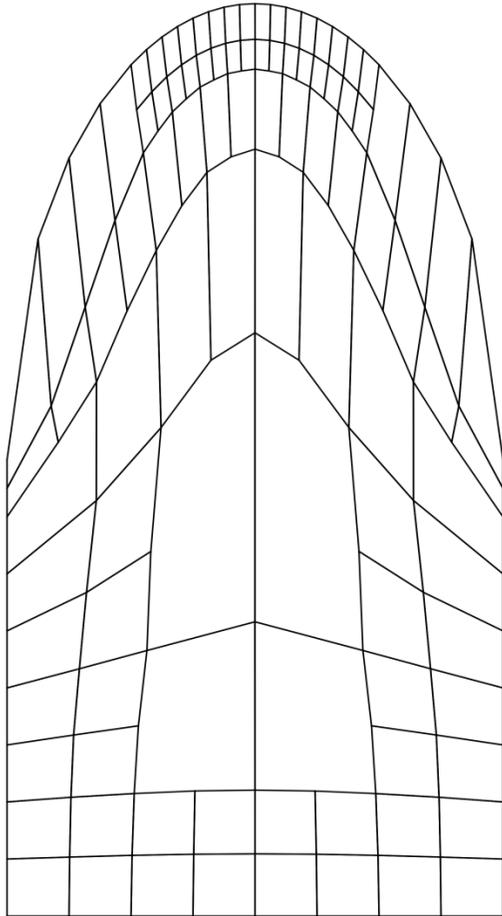
Optimized mesh
without weights



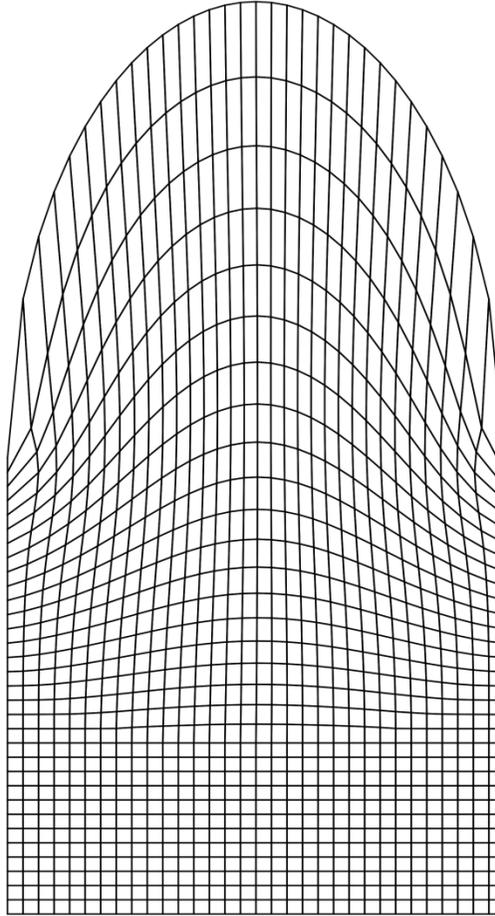
Optimized mesh
with weights

Objective Functions Comparison

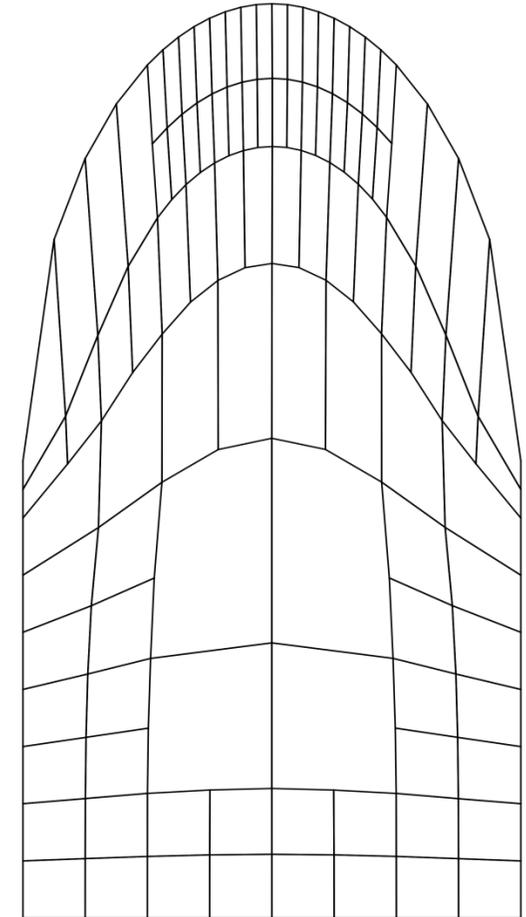
k^* (without weights) versus k_{\square}^* (with weights)



T-mesh optimized with K^*
(without weights)



Uniform mesh optimized with K^*

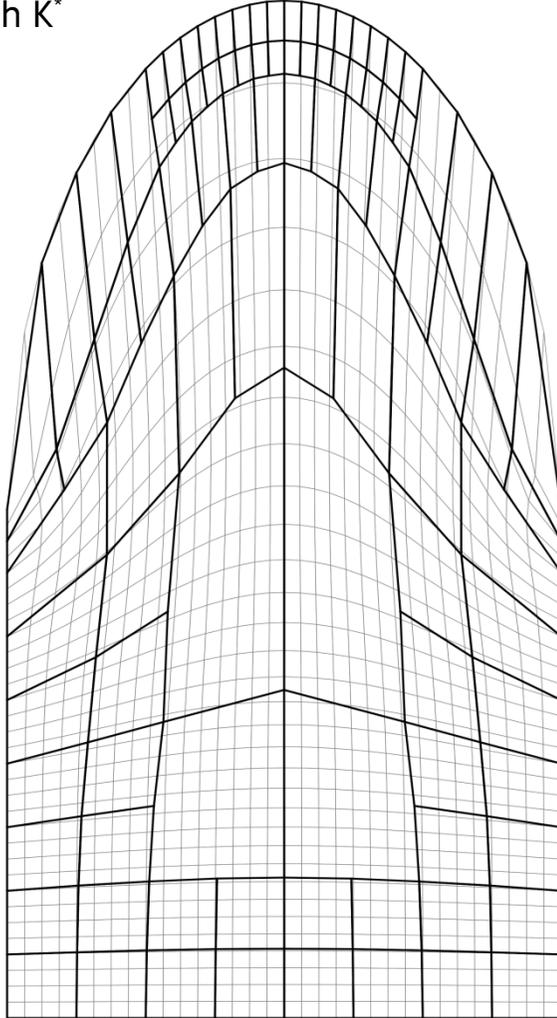


T-mesh optimized with K_{\square}^*
(with weights)
Close to uniform mesh positions

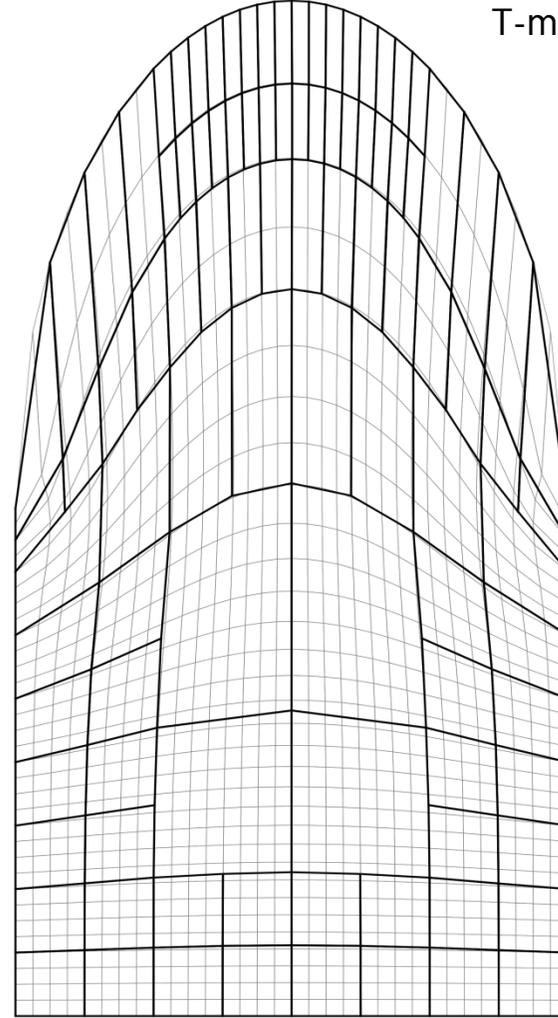
Objective Functions Comparison

k^* (without weights) versus k_{\square}^* (with weights)

T-mesh optimized with K^*
(without weights)



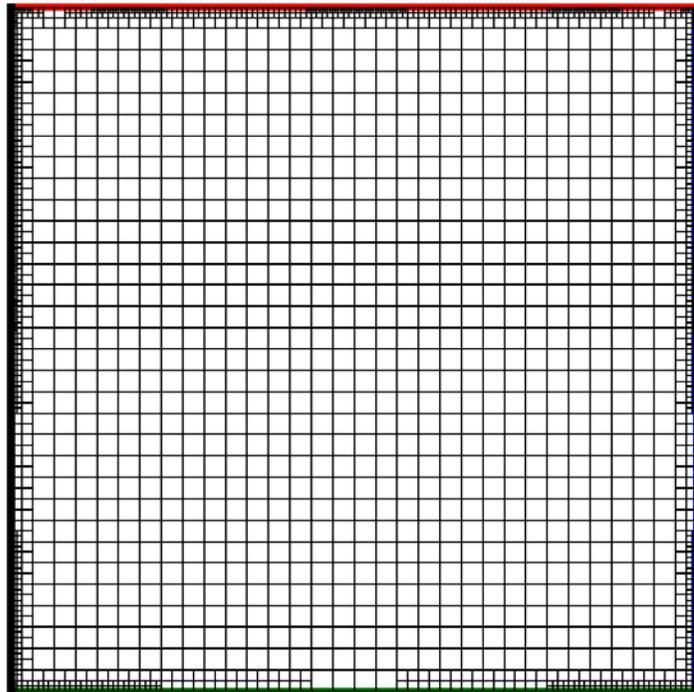
T-mesh optimized with K_{\square}^*
(with weights)



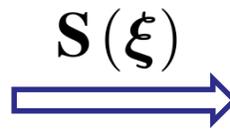
Simultaneous Untangling and Smoothing of T-meshes

T-mesh transformation along the SUS process: Example

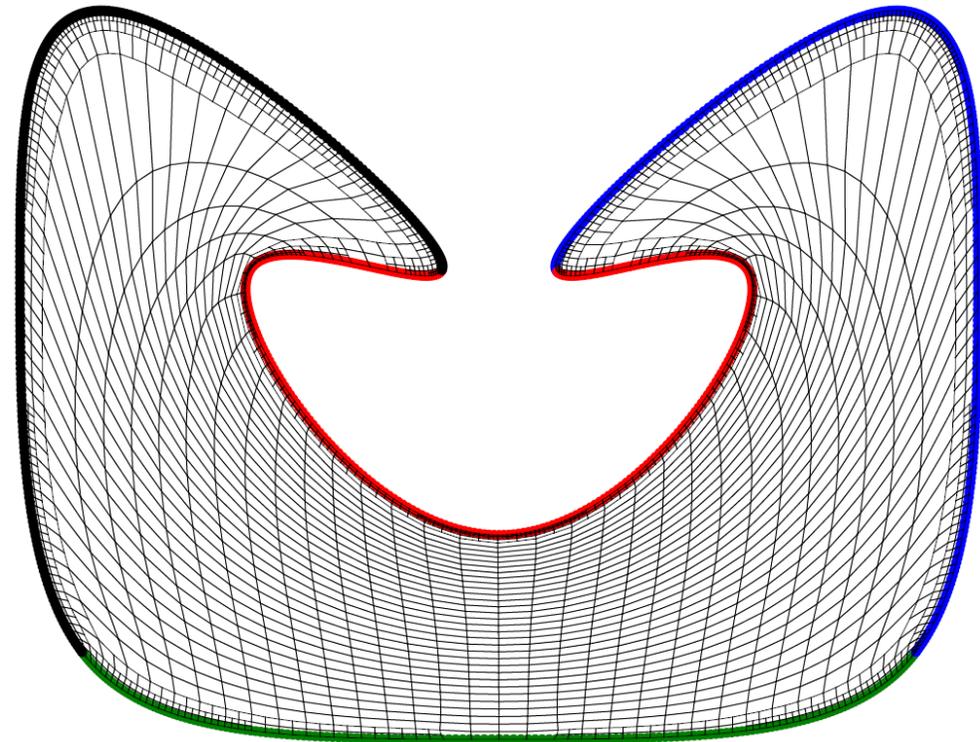
T-mesh



Parameter space



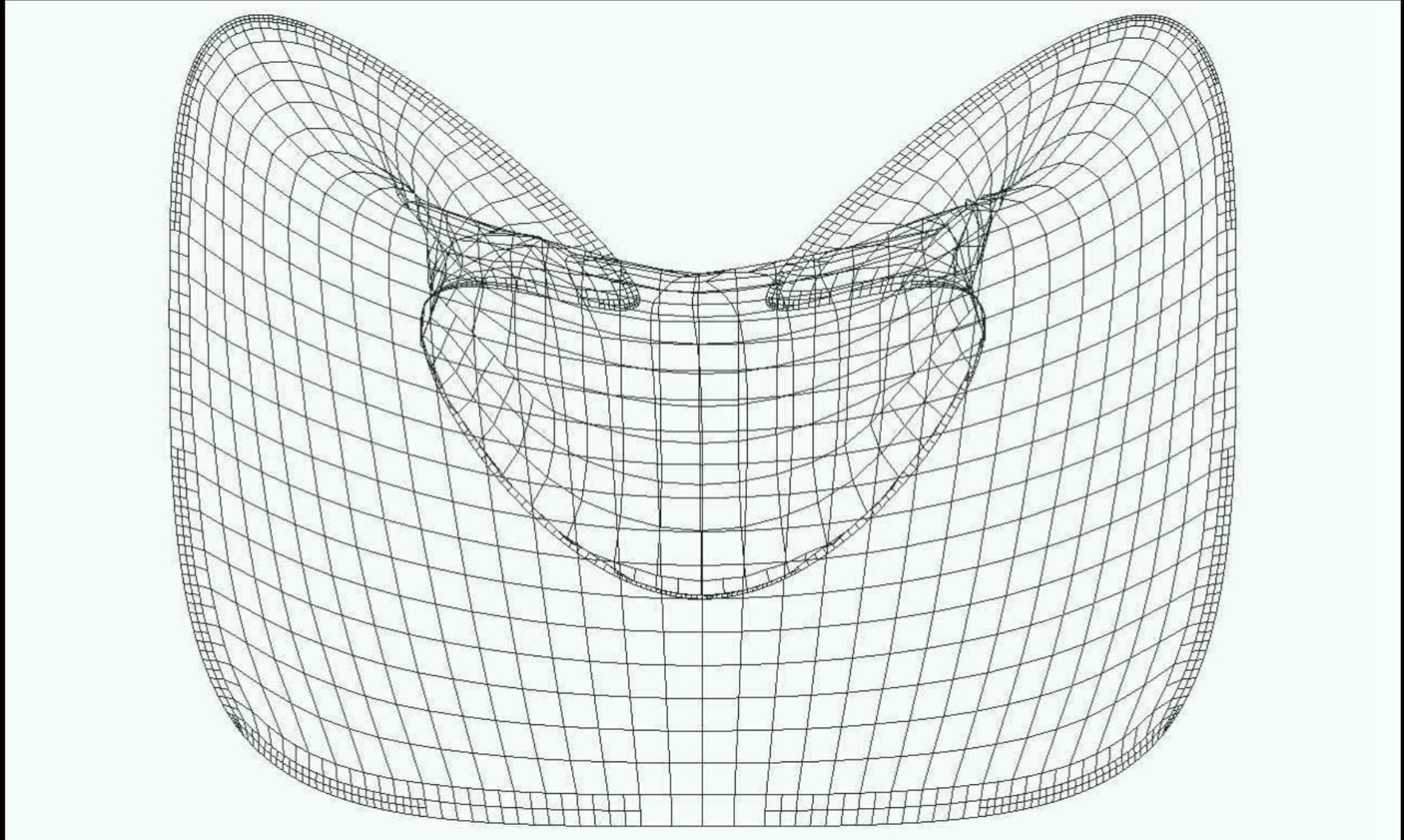
T-spline



Physical space

Simultaneous Untangling and Smoothing of T-meshes

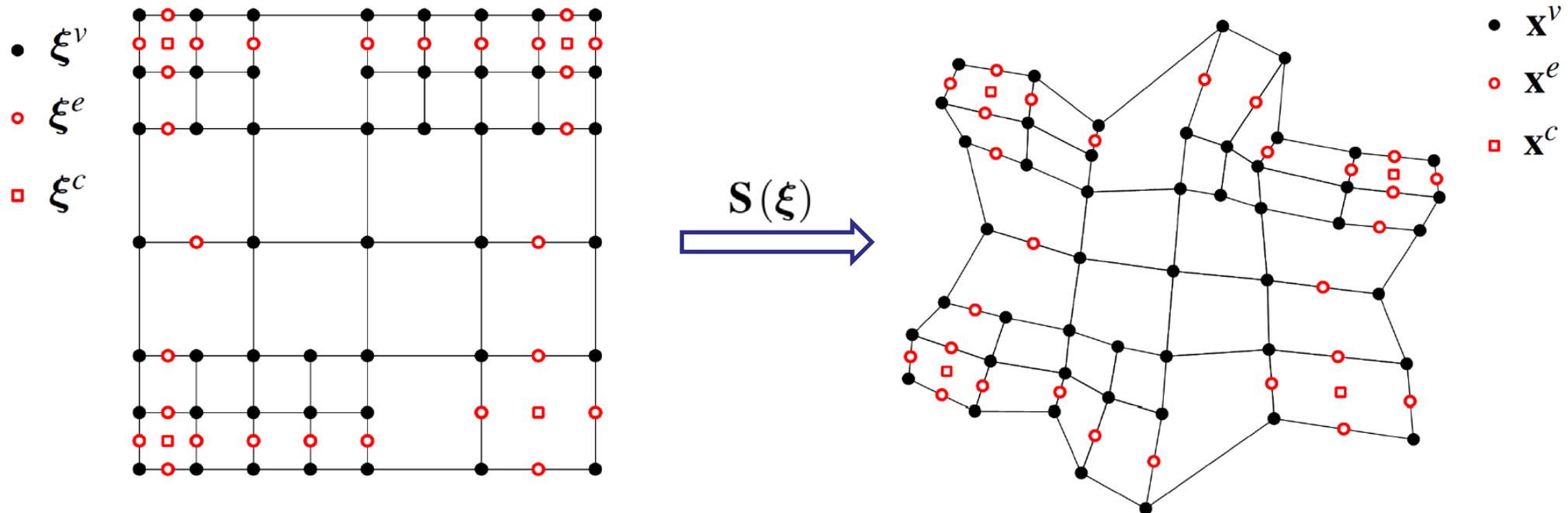
T-mesh transformation along the SUS process: Video



T-spline Parameterization

Determination of control points by imposing interpolation conditions

$$S(\xi) = \sum_{\alpha \in A} P_{\alpha} R_{\alpha}(\xi)$$

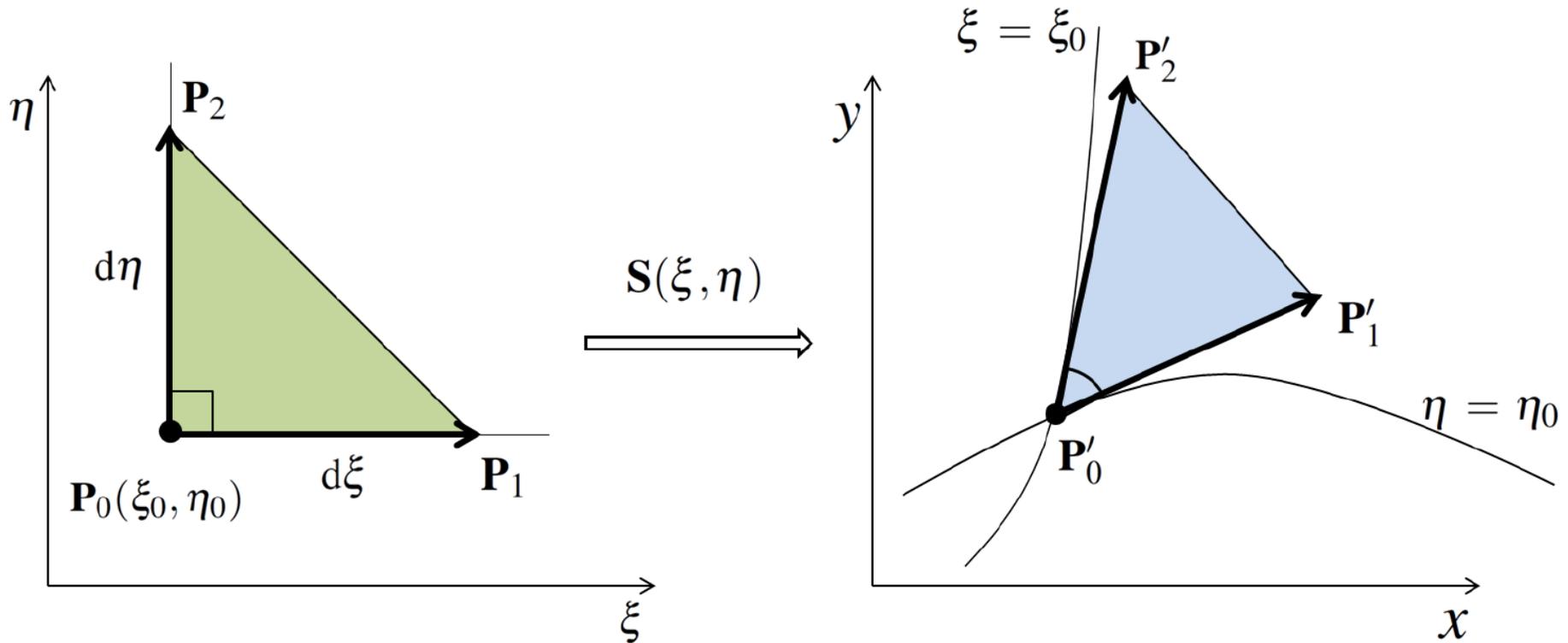


Mean Ratio Jacobian $J_r(\xi)$ of Parametric Transformation

A quality metric of the T-spline mapping at any point P_0

$$-1 \leq J_r(\xi) = \frac{2 \det(J)}{\|J\|^2} \leq 1$$

where J is the jacobian matrix of the T-spline mapping S

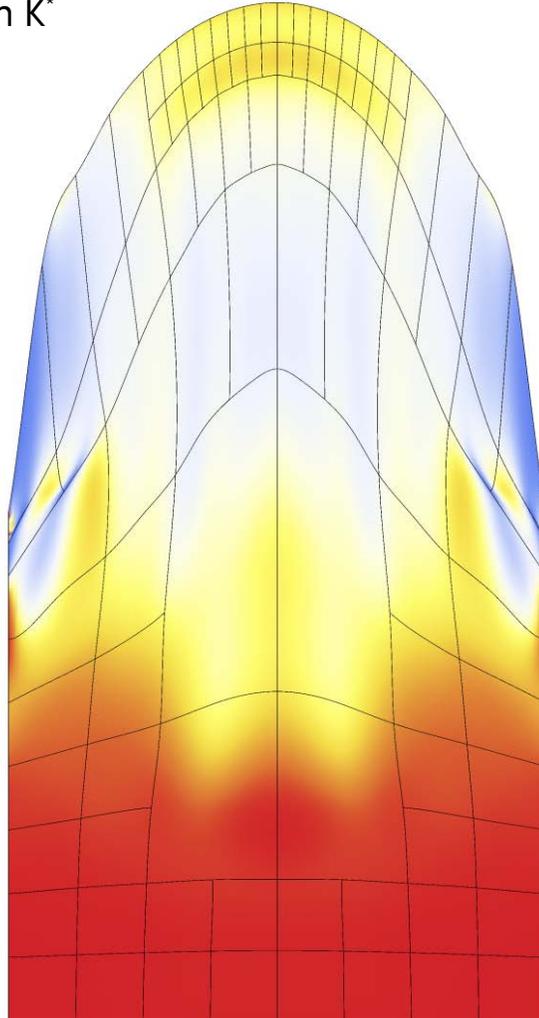


Objective Functions Comparison

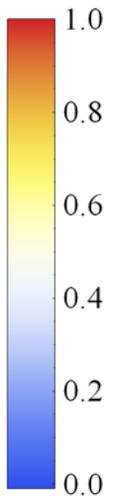
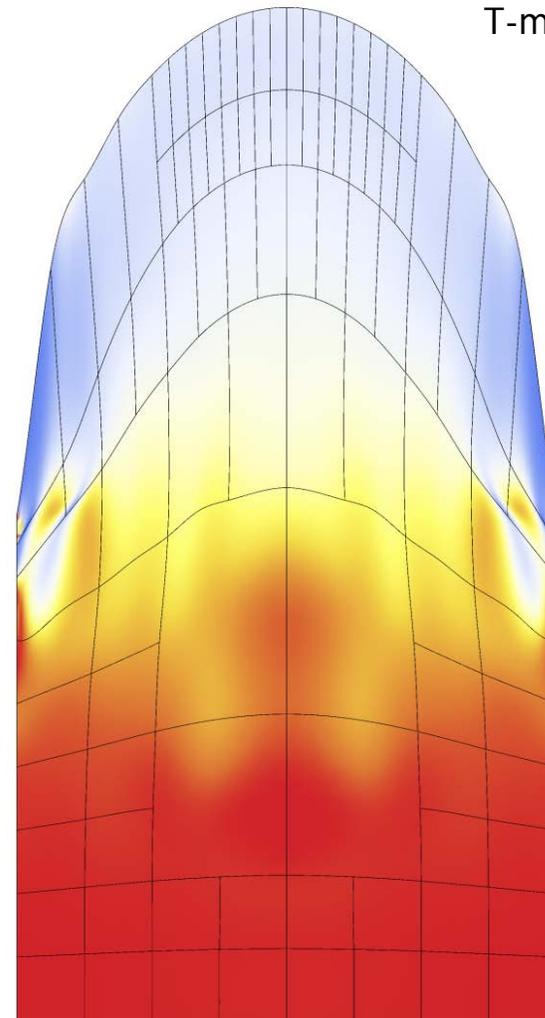
k^* (without weights) versus k_{\square}^* (with weights)

Mean ratio Jacobian

T-mesh optimized with K^*
(without weights)

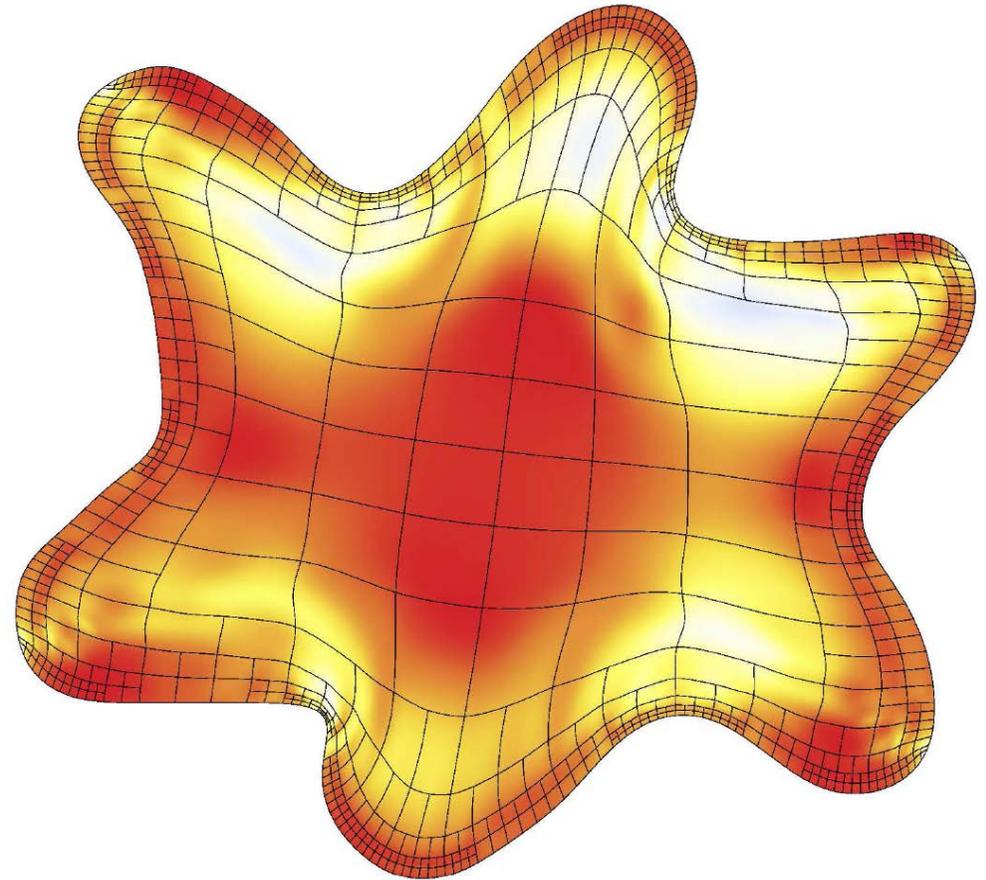
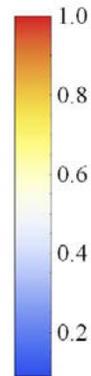
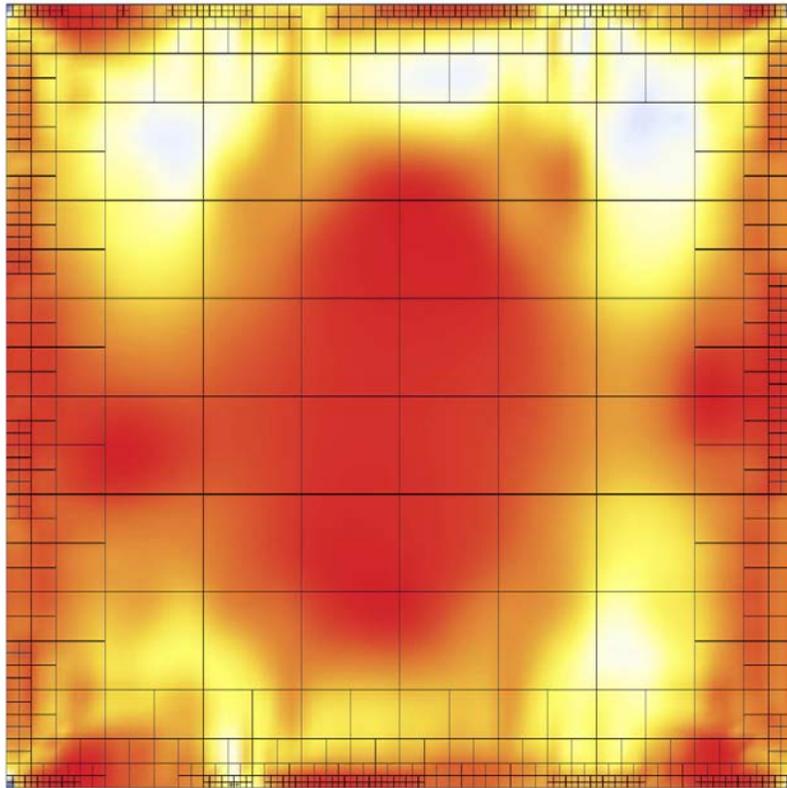


T-mesh optimized with K_{\square}^*
(with weights)



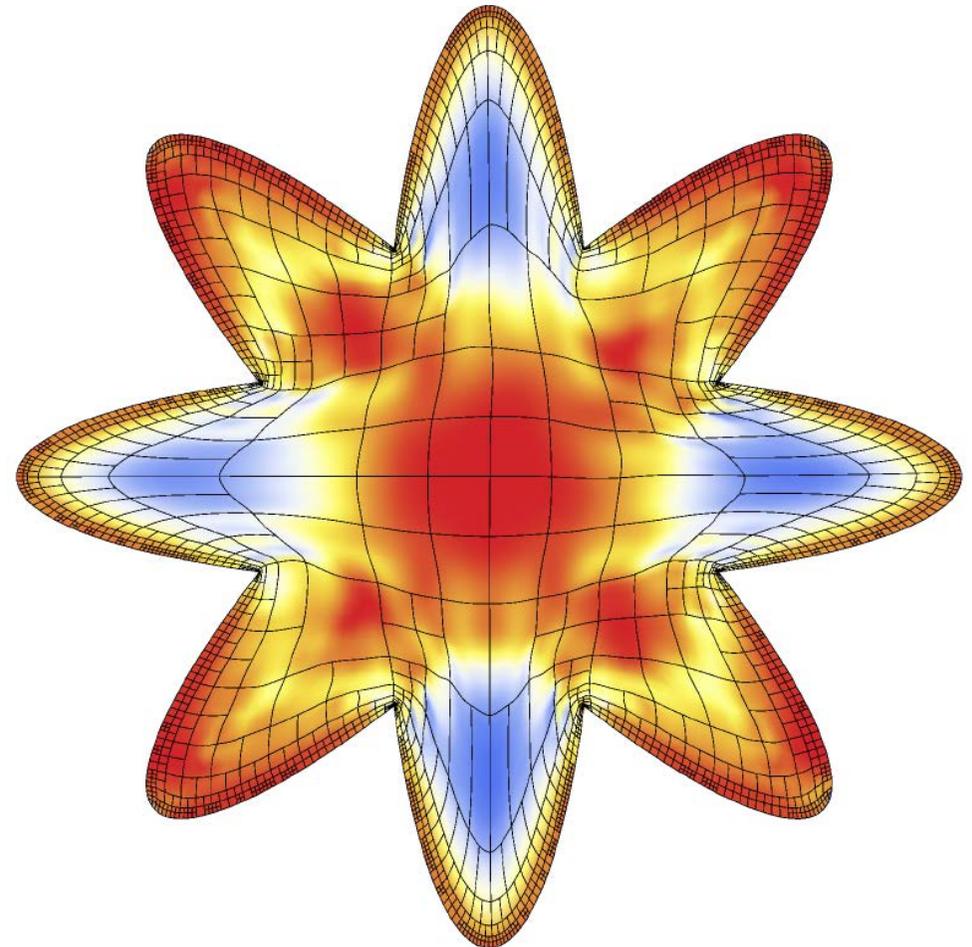
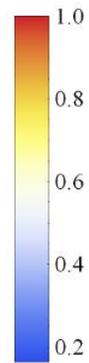
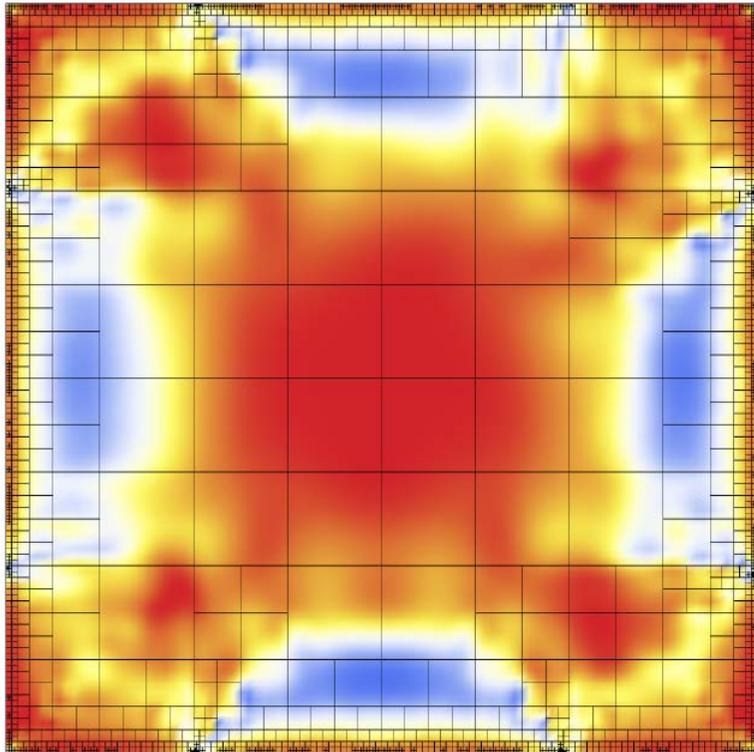
Applications: Isogeometric Modeling

The Spot (Mean Ratio Jacobian)



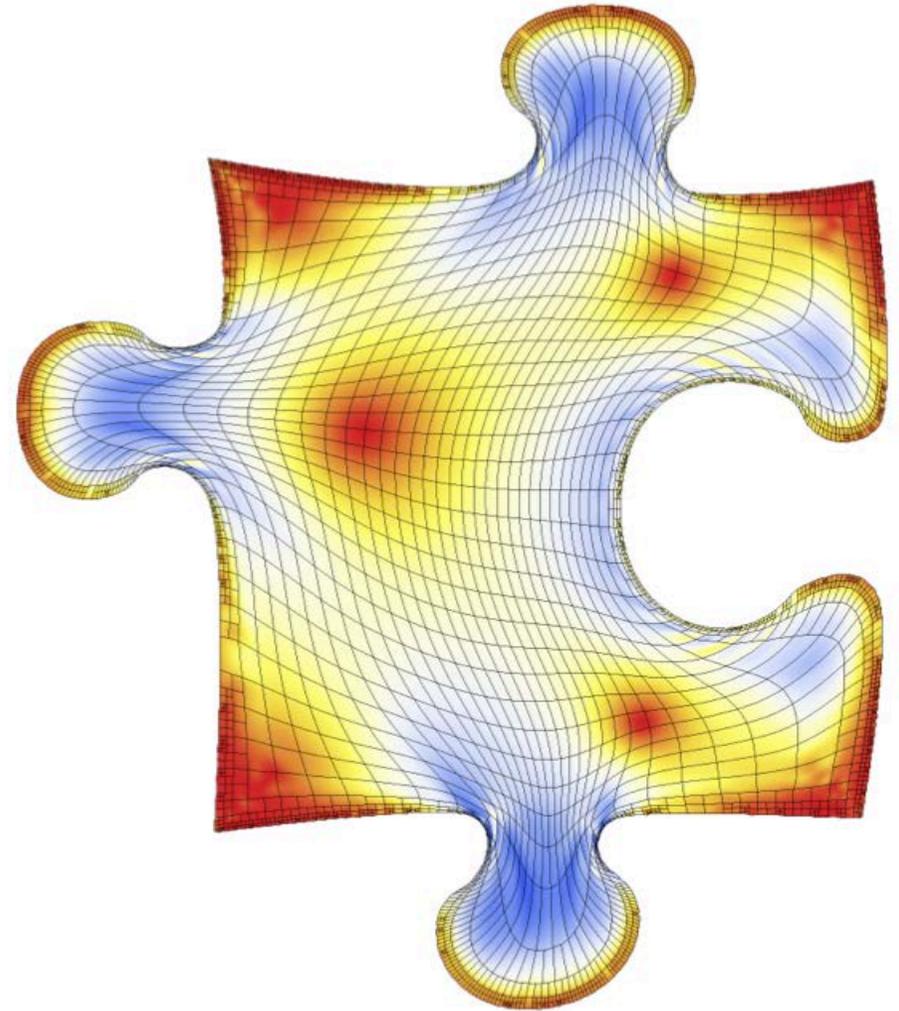
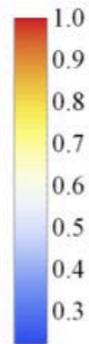
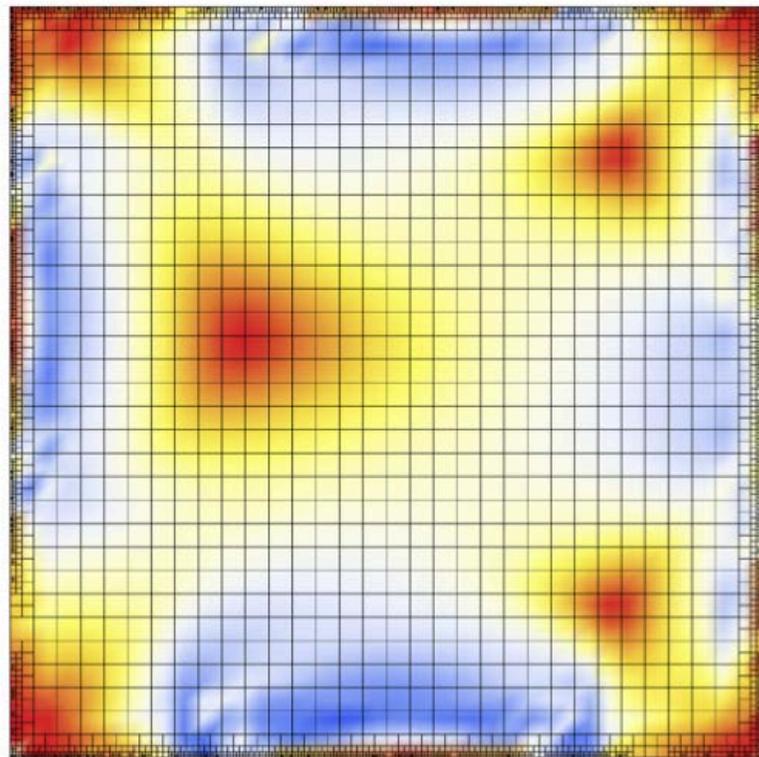
Applications: Isogeometric Modeling

The Flower (Mean Ratio Jacobian)



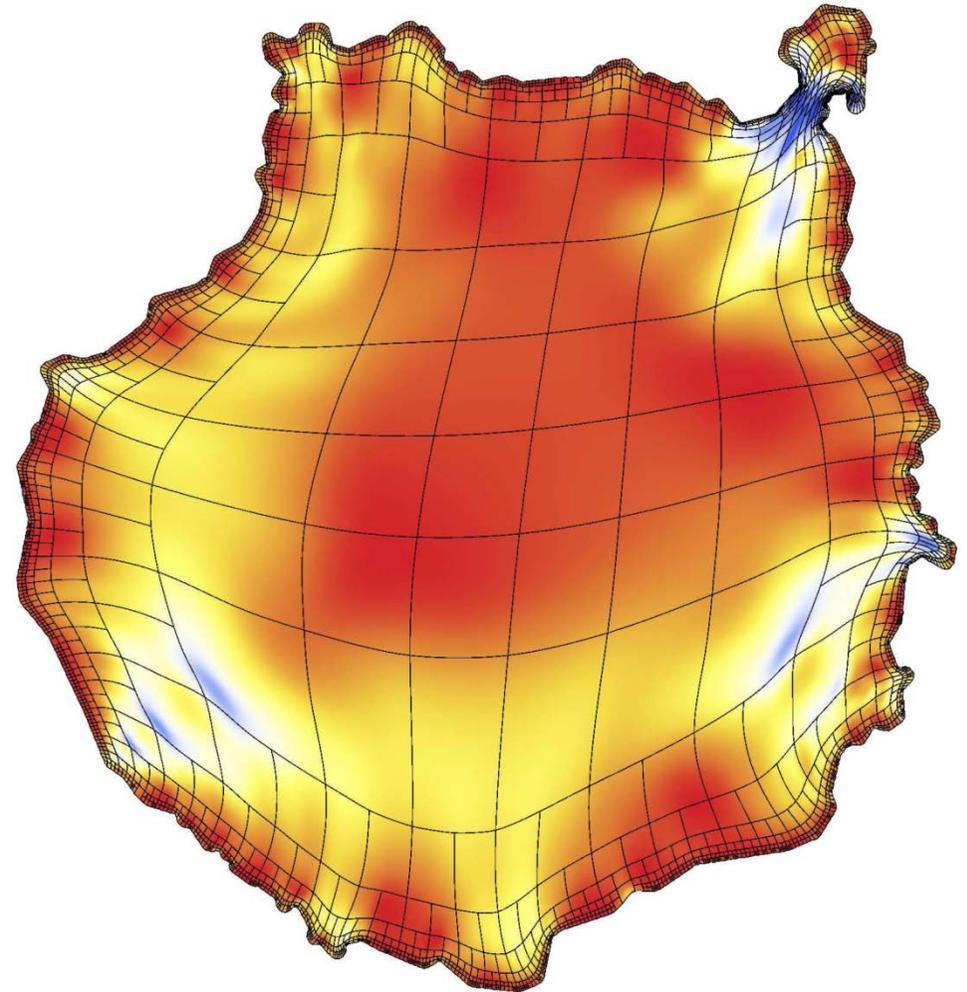
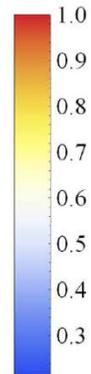
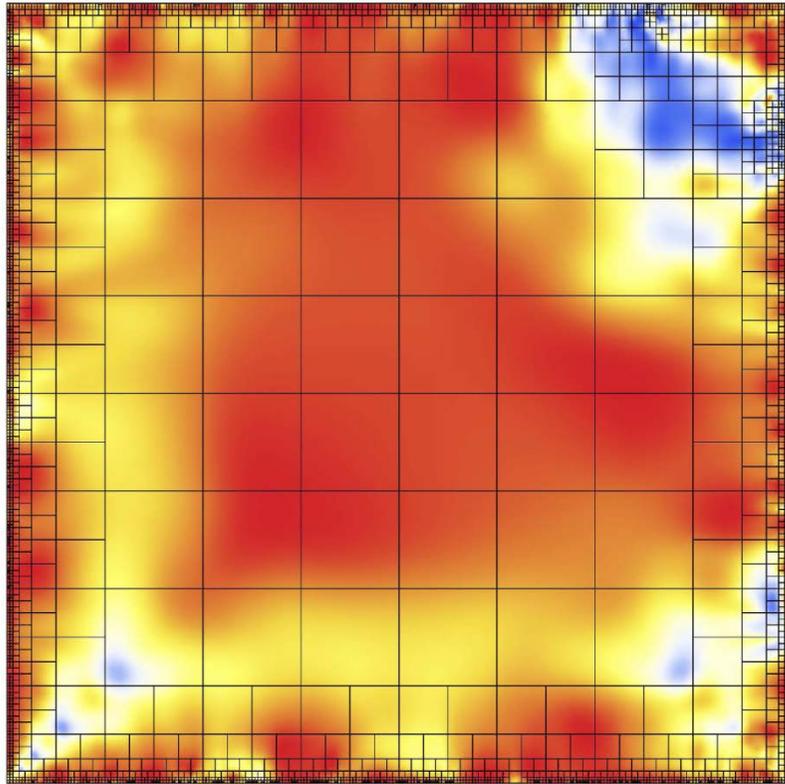
Applications: Isogeometric Modeling

Puzzle Piece (Mean Ratio Jacobian)



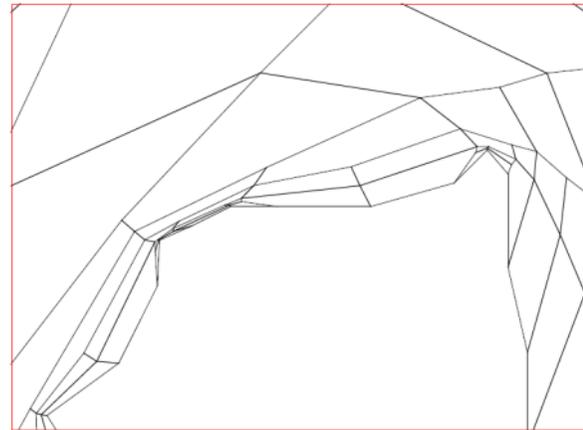
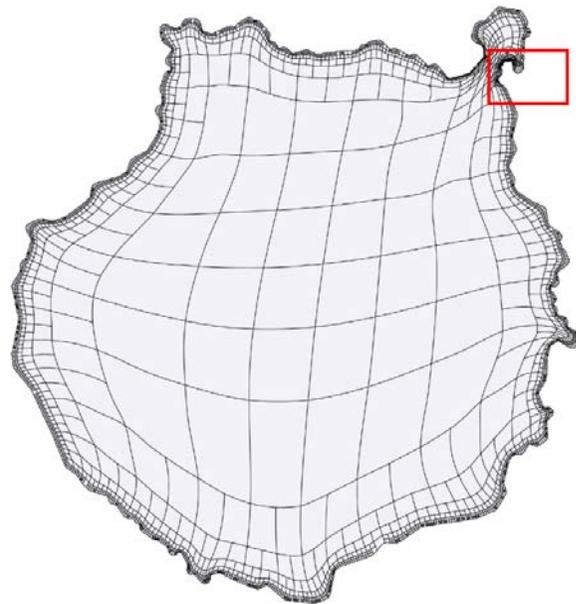
Applications: Isogeometric Modeling

Gran Canaria Island (Mean Ratio Jacobian)

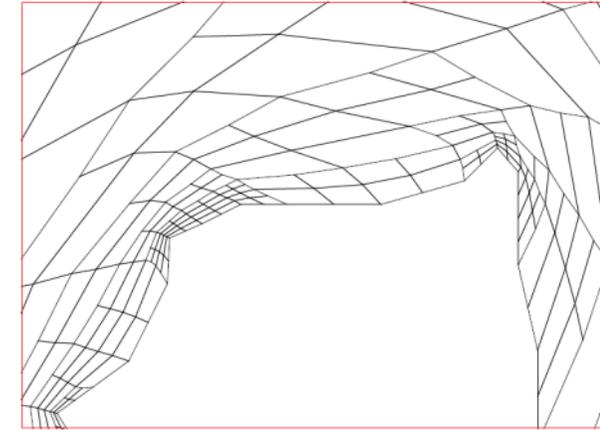


Applications: Isogeometric Modeling

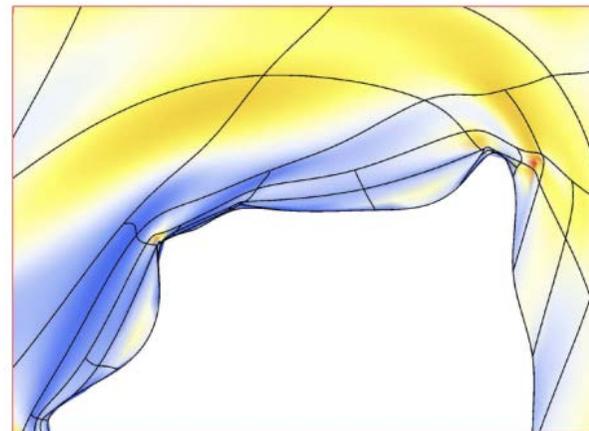
Gran Canaria Island (adaptive refinement to improve the mean ratio Jacobian)



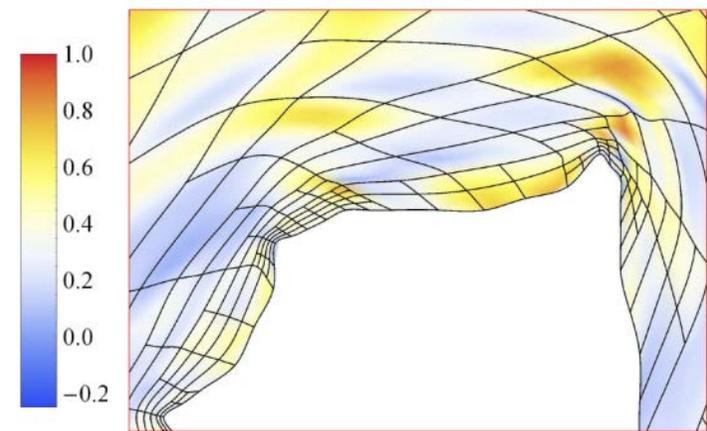
Initial T-mesh



Refined T-mesh



Initial T-spline & Mean ratio Jacobian

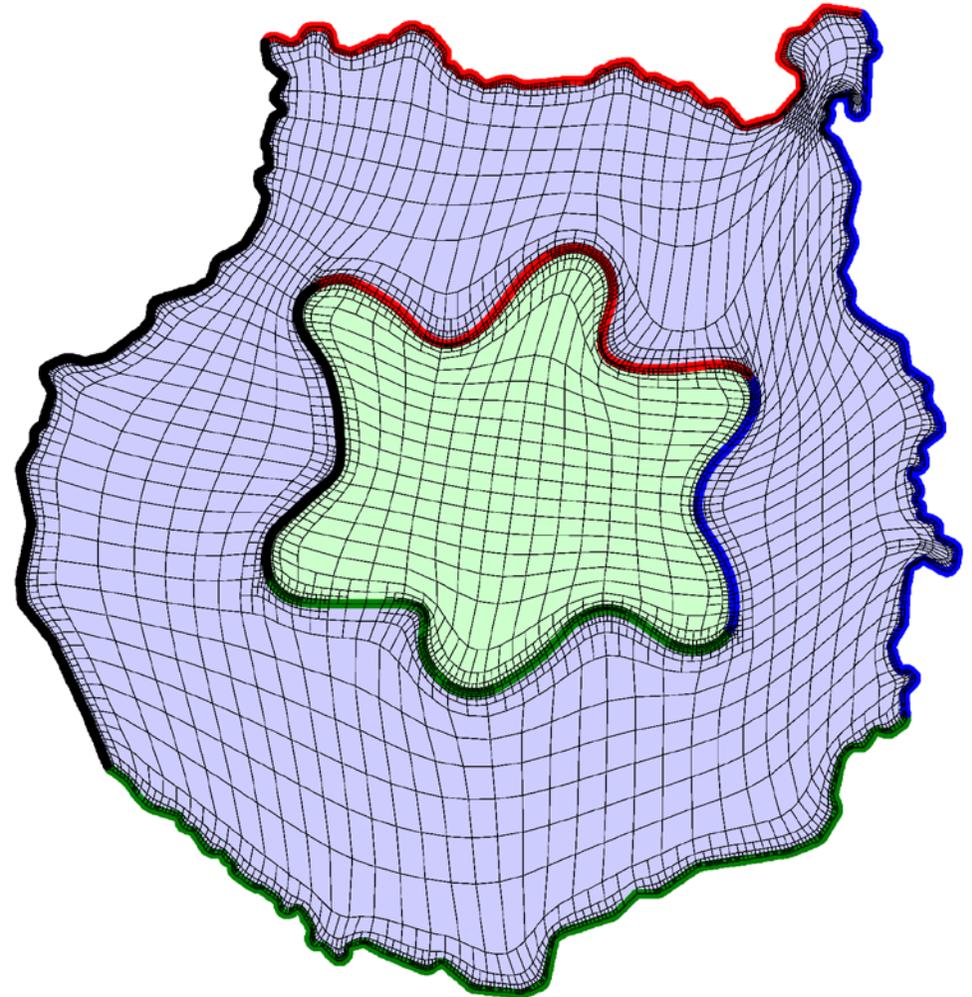
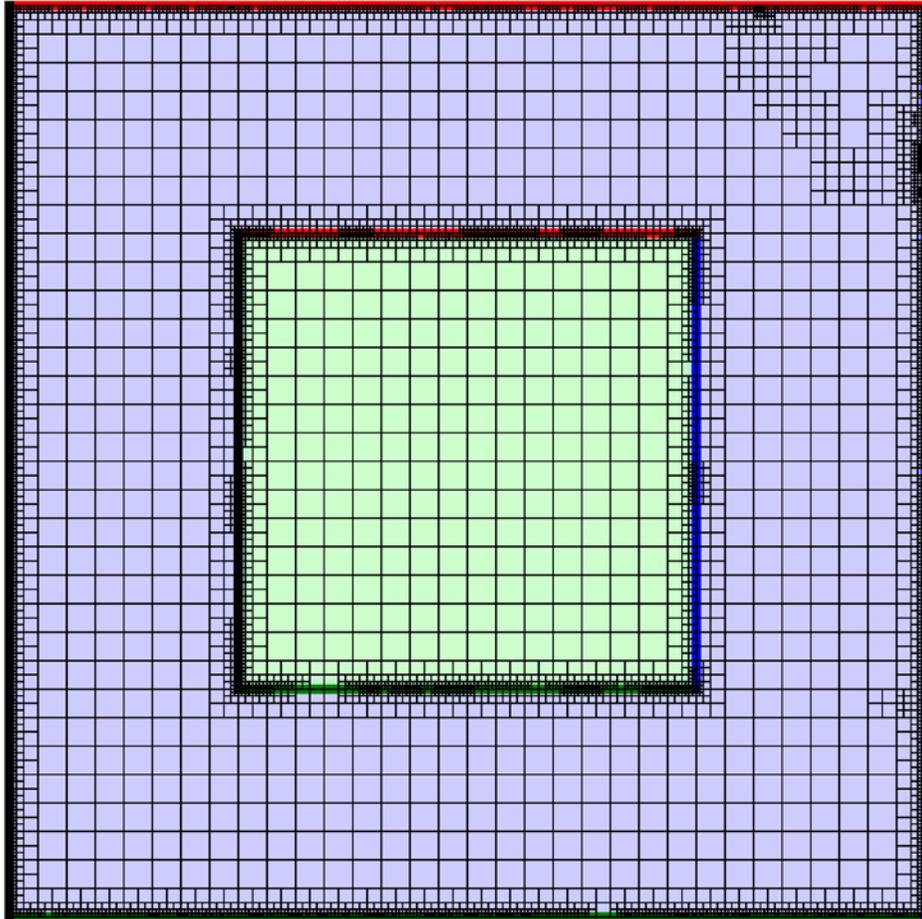


Refined T-spline & Mean ratio Jacobian

*No negative Jacobian
after refinement!*

Applications: Isogeometric Modeling

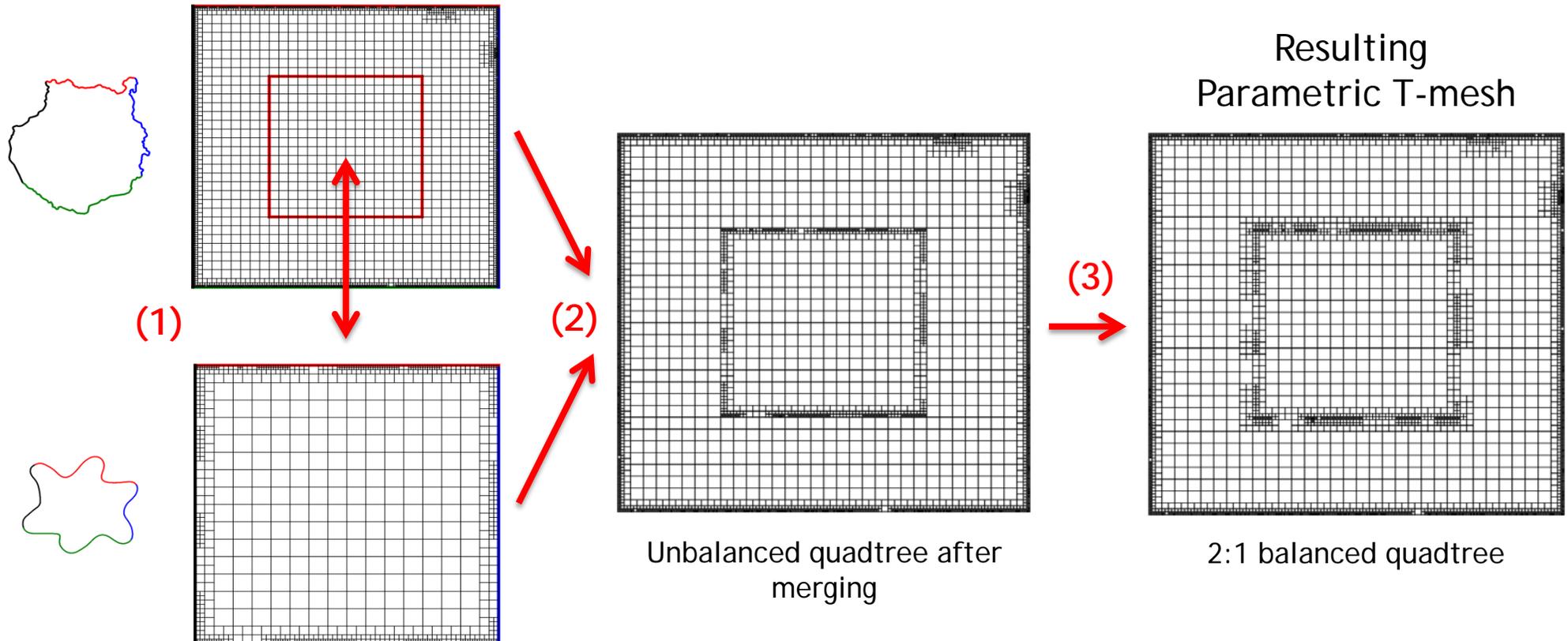
Geometries with several materials



Applications: Isogeometric Modeling

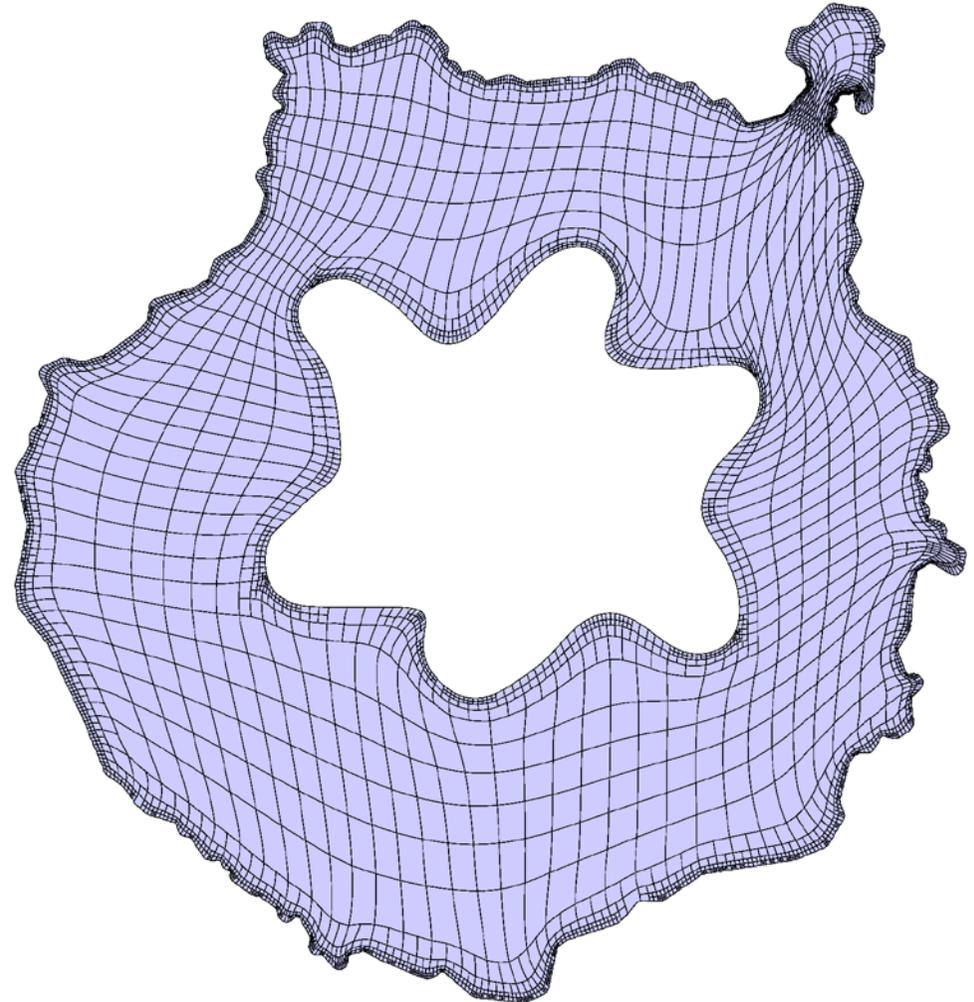
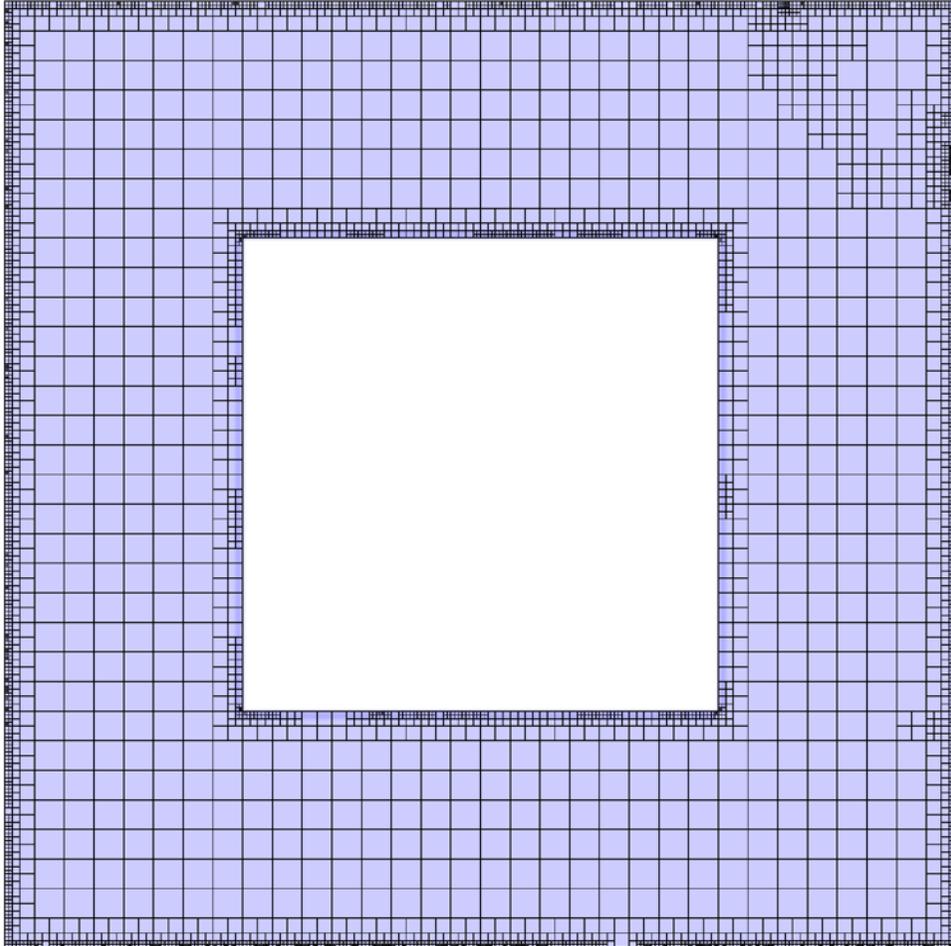
Strategy for embedded planar geometries: Three steps

1. Individual quadtree approximation for each geometry (they can be processed in parallel)
2. Insert a quadtree in a region of another quadtree
3. Balance the resulting quadtree



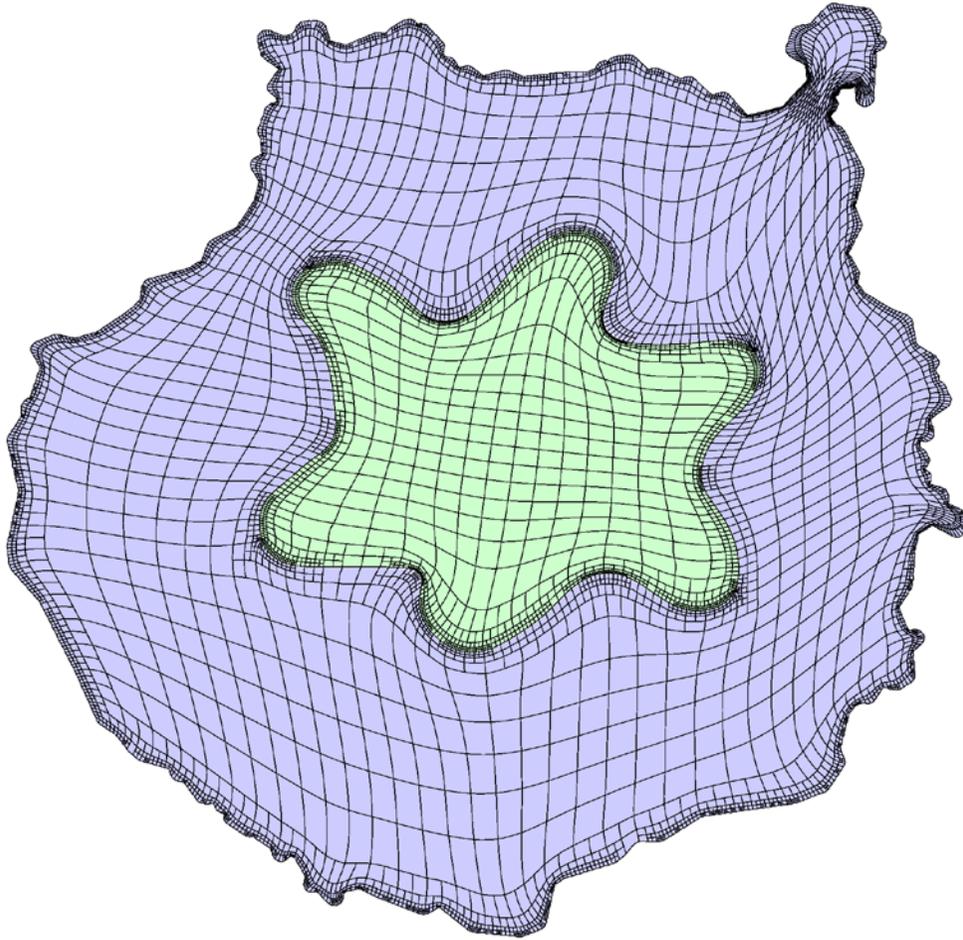
Applications: Isogeometric Modeling

Geometries with holes

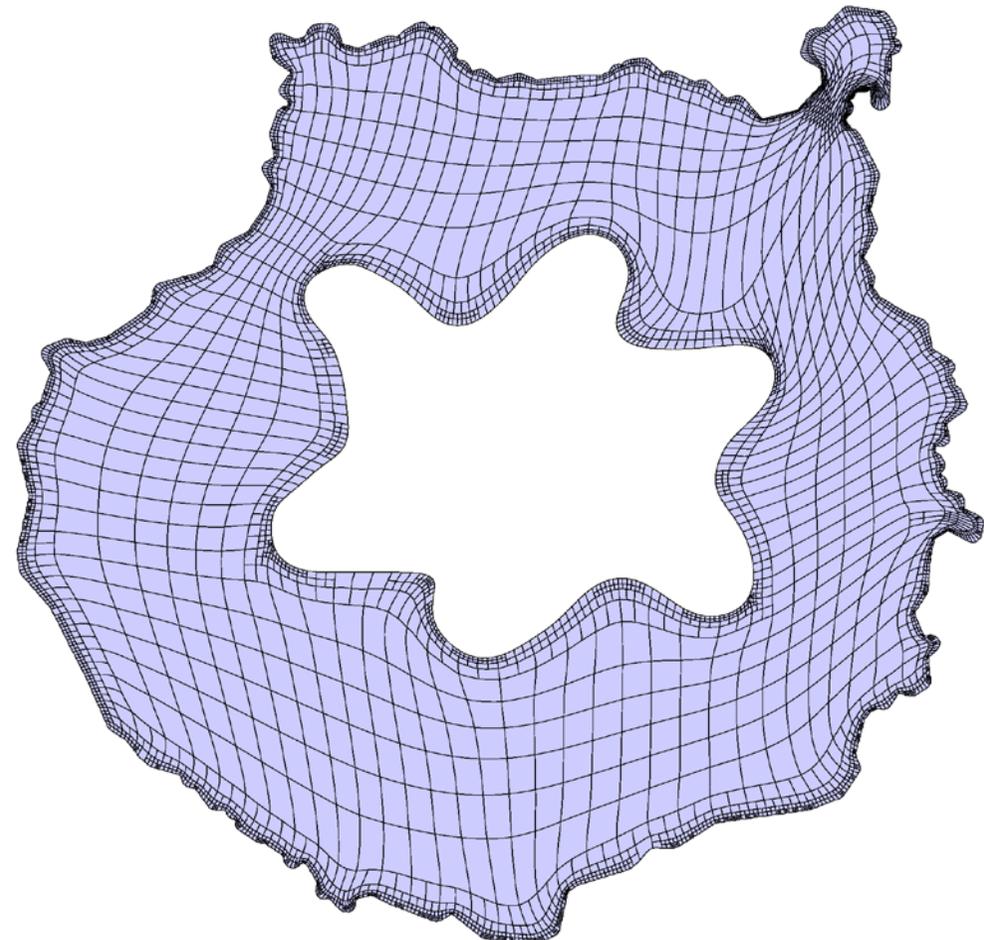


Applications: Isogeometric Modeling

Embedded planar geometries (T-spline representation in physical space)



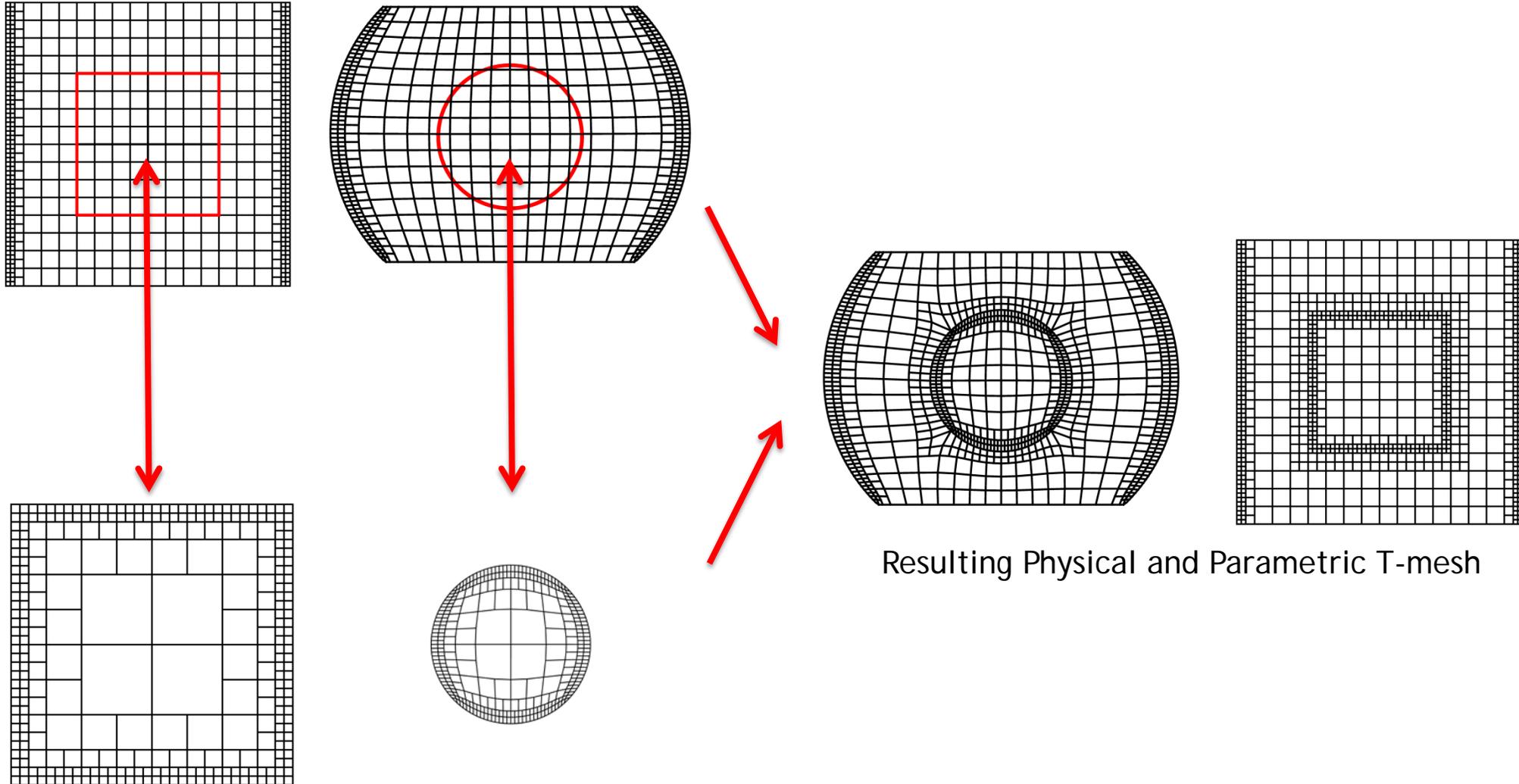
T-spline representation with different materials



T-spline representation with a hole

Applications: Isogeometric Modeling

Strategy for embedded planar geometries: Other example

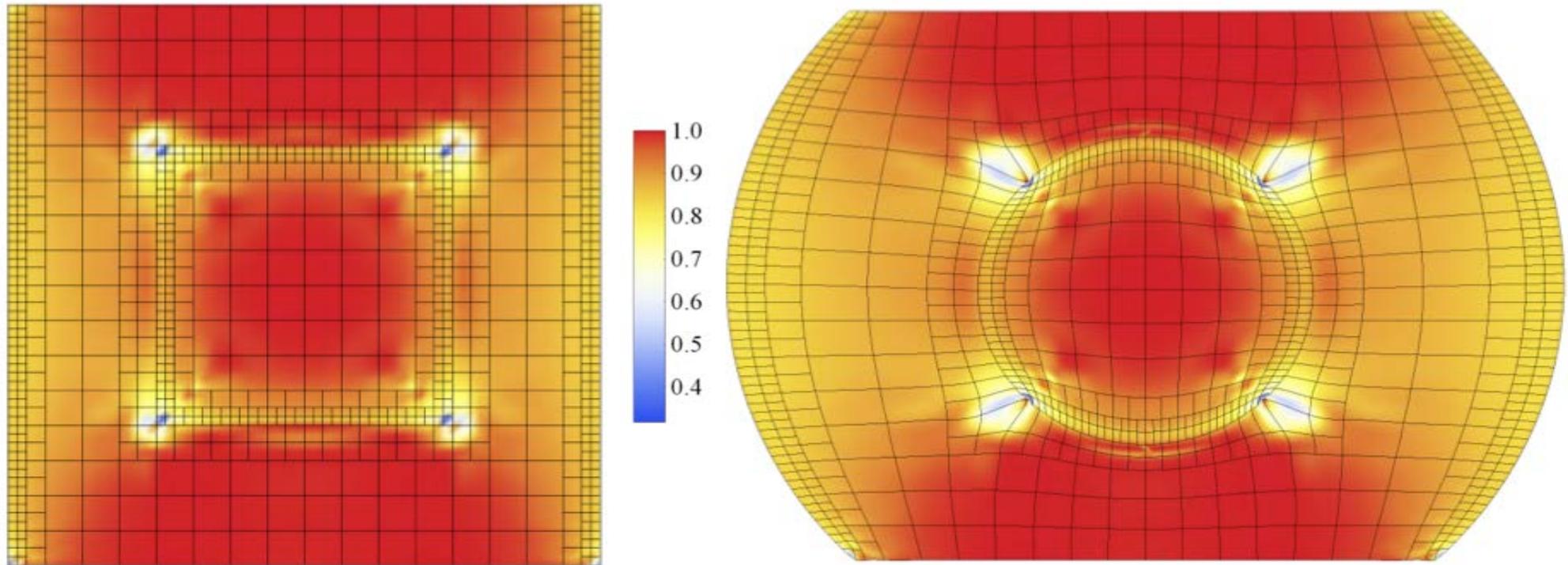


Resulting Physical and Parametric T-mesh

Applications: Isogeometric Modeling

Strategy for embedded planar geometries: Other example

Mean ratio Jacobian

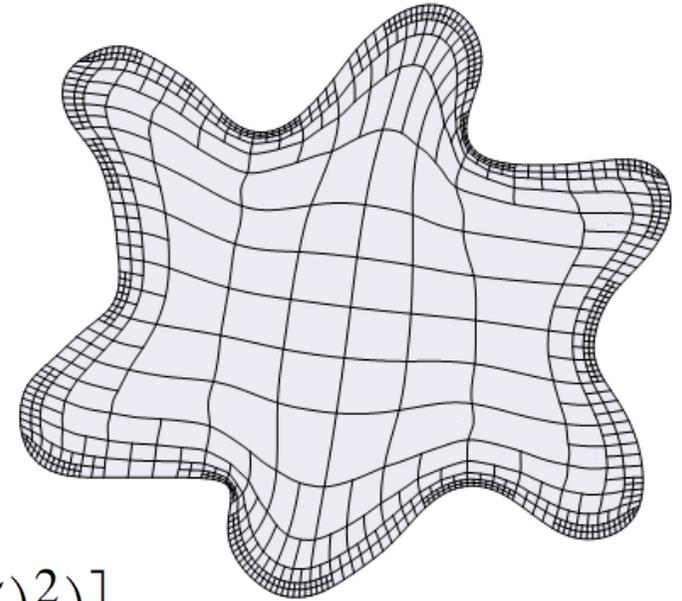


Local Nested Adaptive Refinement

Numerical solution of a Poisson problem

Concentrate source in relation to the initial mesh size

$$\begin{aligned} -\Delta u &= f && \text{in } \Omega, \\ u &= g && \text{on } \partial\Omega. \end{aligned}$$



Exact solution:

$$u(x, y) = \exp \left[-10^3 \left((x - 0.6)^2 + (y - 0.35)^2 \right) \right]$$

Residual-type error indicator:

$$\eta(\Omega_e)^2 = \|h(f + \Delta u_h)\|_{0, \Omega_e}^2 = \int_{\Omega_e} h^2 (f + \Delta u_h)^2 \, d\Omega$$

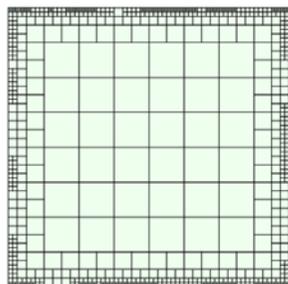
Local Nested Adaptive Refinement

Numerical solution of a Poisson problem

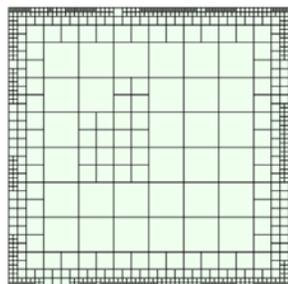


SIANI

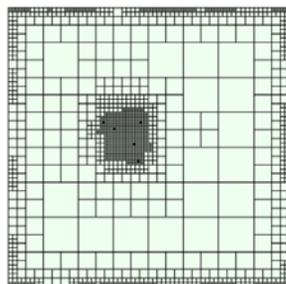
Error indicator : $\eta(\Omega_e)^2 = \int_{\Omega_e} h^2 (f + \Delta u_h)^2 d\Omega$



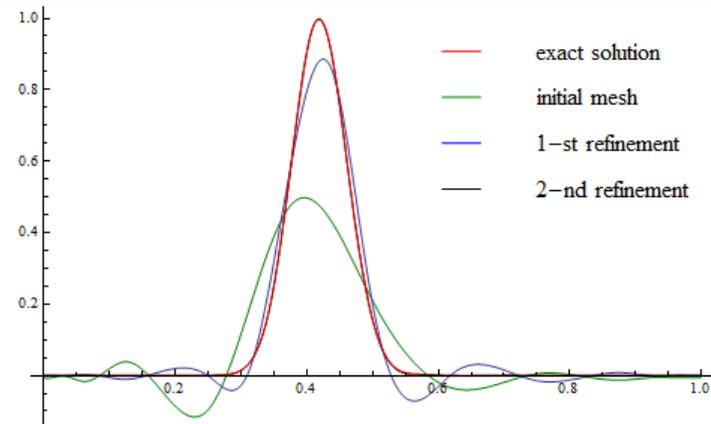
(a) 844 cells, 1456 DOF



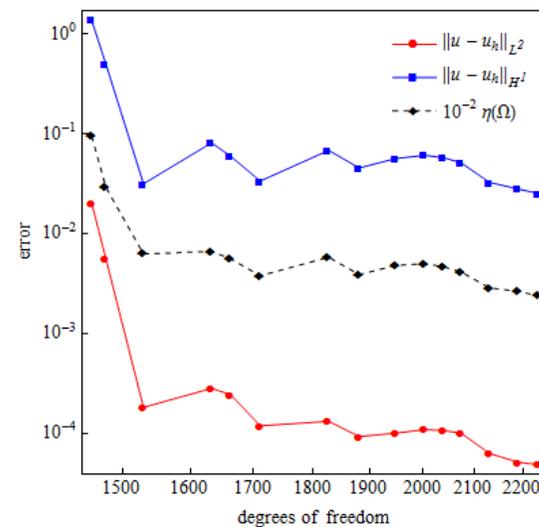
(b) 859 cells, 1476 DOF



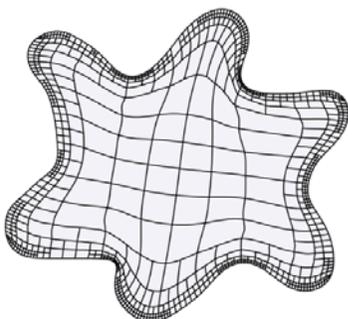
(c) 1552 cells, 2233 DOF



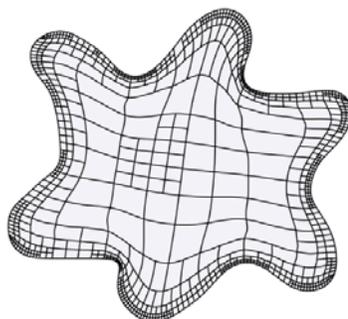
Numerical solution across a section



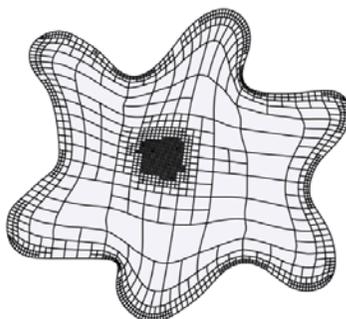
Convergence behavior



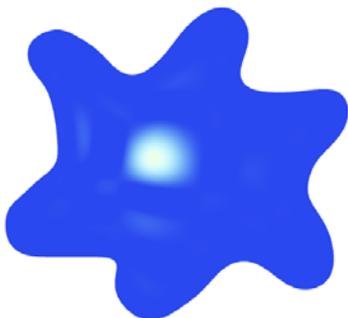
(d) Initial mesh



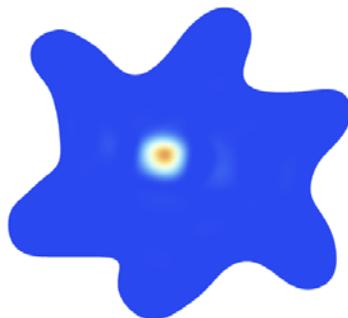
(e) 1-st refinement



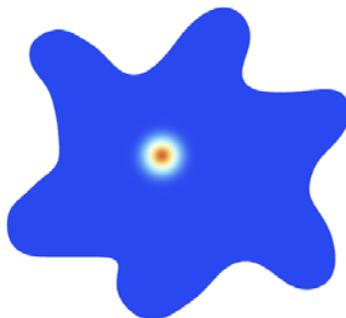
(f) 14-th refinement



(g) Initial solution



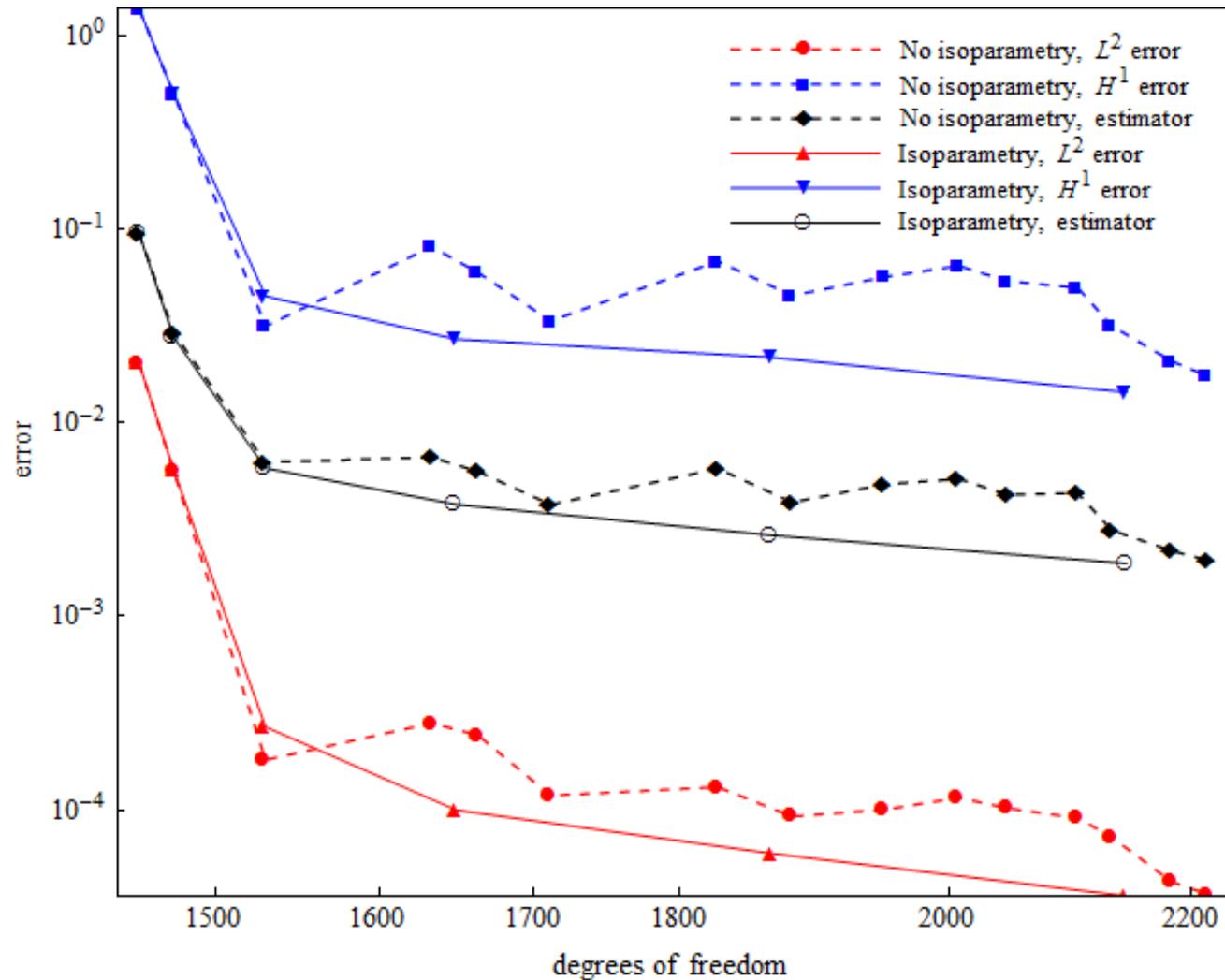
(h) 1-st refinement



(i) 14-th refinement

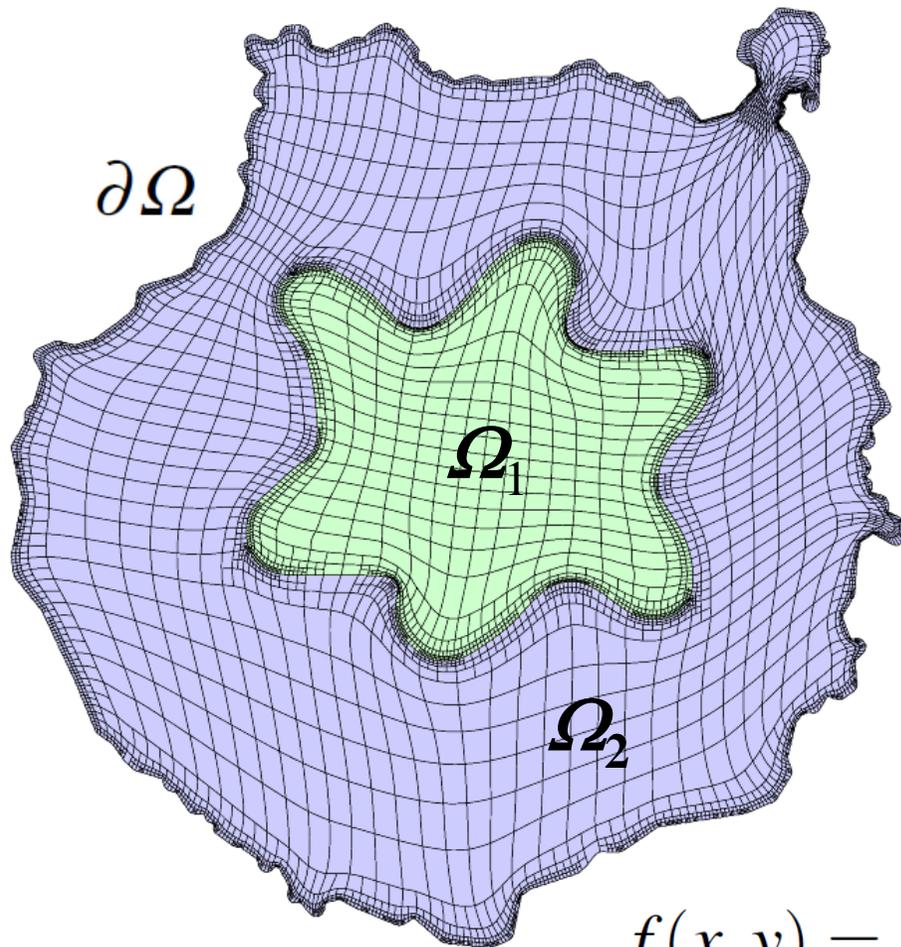
Local Nested Adaptive Refinement

Influence of isoparametry in the convergence behavior



Poisson Problem for a Domain with Two Materials

Statement of the problem



$$\begin{aligned} -\nabla(k(\mathbf{x})\nabla u) &= f && \text{in } \Omega, \\ u &= 0 && \text{on } \partial\Omega \end{aligned}$$

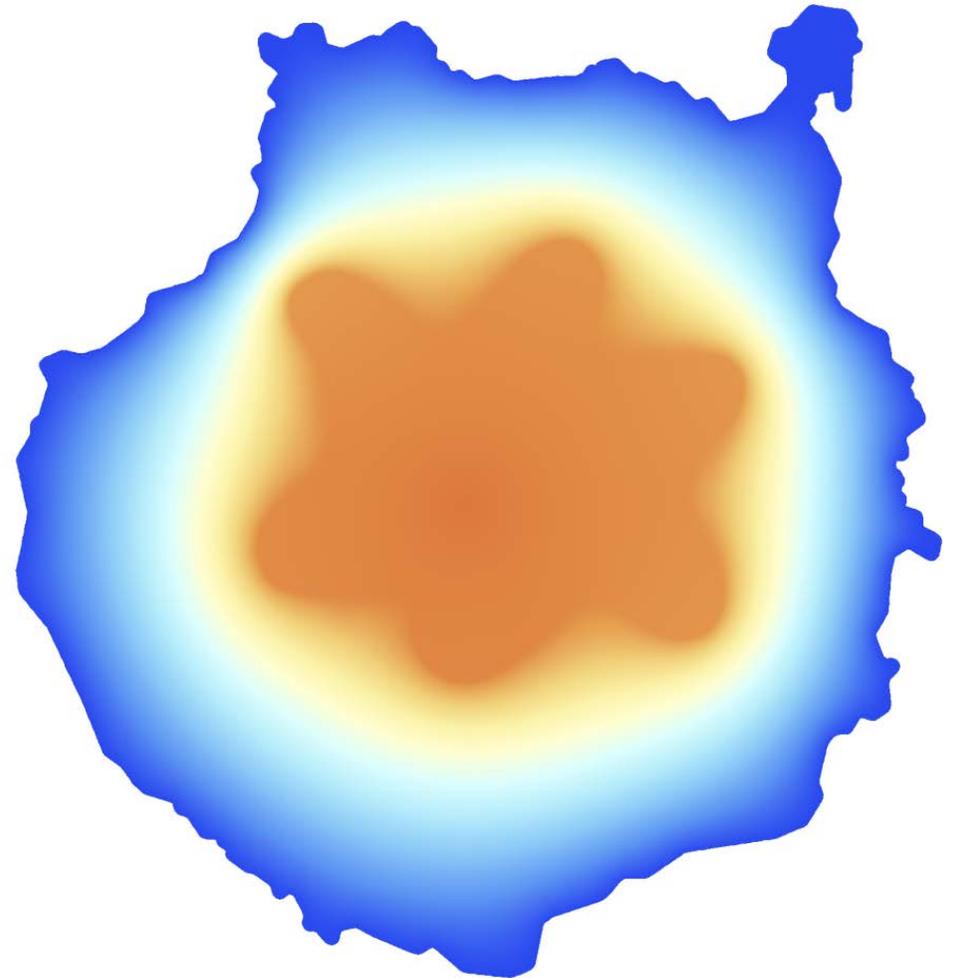
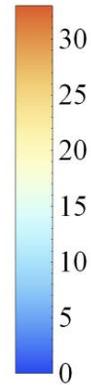
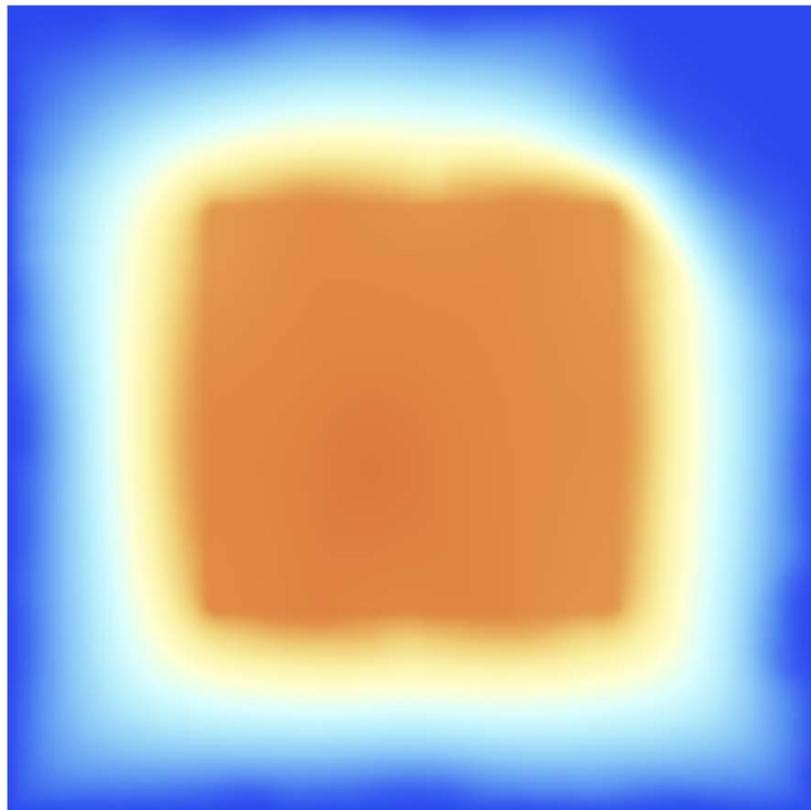
$$k(\mathbf{x}) = \begin{cases} k_1 & \text{if } \mathbf{x} \in \Omega_1 \\ k_2 & \text{if } \mathbf{x} \in \Omega_2 \end{cases}$$

$$k_1 = 1 \gg k_2 = 0.01$$

$$f(x, y) = 10^3 \exp[-10^3((x-0.5)^2 + (y-0.5)^2)]$$

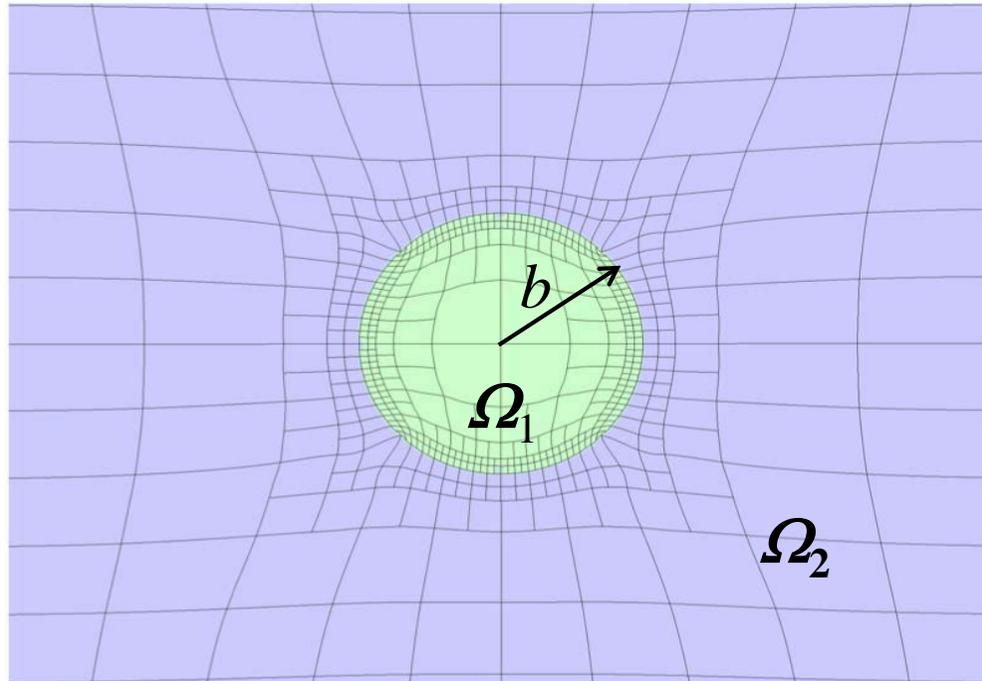
Poisson Problem for a Domain with Two Materials

Numerical solution in parametric and physical domain



Poisson Problem for a Domain with Two Materials

Dielectric cylinder in an uniform horizontal electric field E_0



T-spline detail

$$\begin{aligned} -\nabla(k(\mathbf{x})\nabla u) &= 0 && \text{in } \Omega, \\ u &= g && \text{on } \partial\Omega. \end{aligned}$$

$$k(\mathbf{x}) = \begin{cases} \epsilon_0 \epsilon_r & \text{if } \mathbf{x} \in \Omega_1 \quad \rho < b \\ \epsilon_0 & \text{if } \mathbf{x} \in \Omega_2 \quad \rho \geq b \end{cases}$$

The analytic solution in cylindrical coordinates (ρ, φ) is given by:

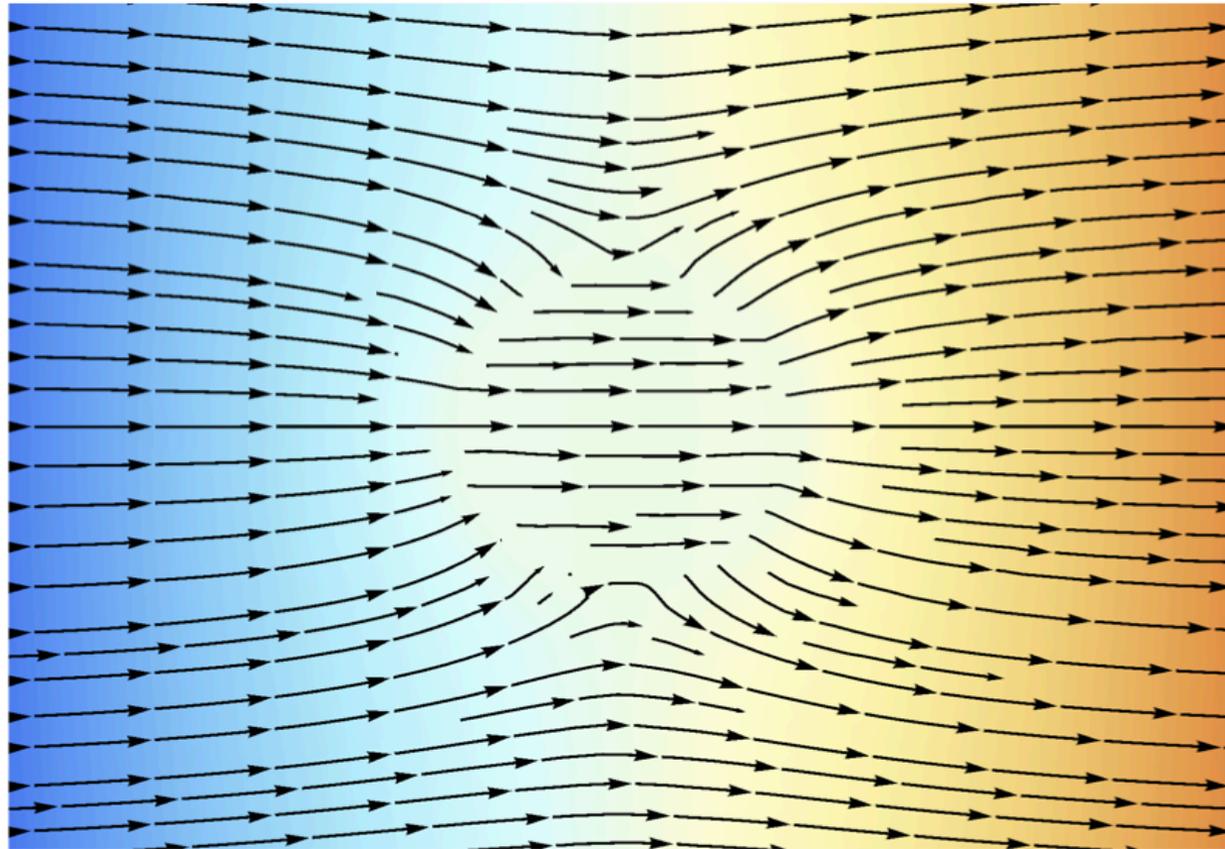
$$u_{\rho < b} = \frac{-2E_0 \rho \cos \varphi}{(\epsilon_r + 1)}$$

$$u_{\rho \geq b} = E_0 \cos \varphi \left(-\rho + \frac{b^2(\epsilon_r - 1)}{\rho(\epsilon_r + 1)} \right)$$

Poisson Problem for a Domain with Two Materials

Dielectric cylinder in an uniform electric field

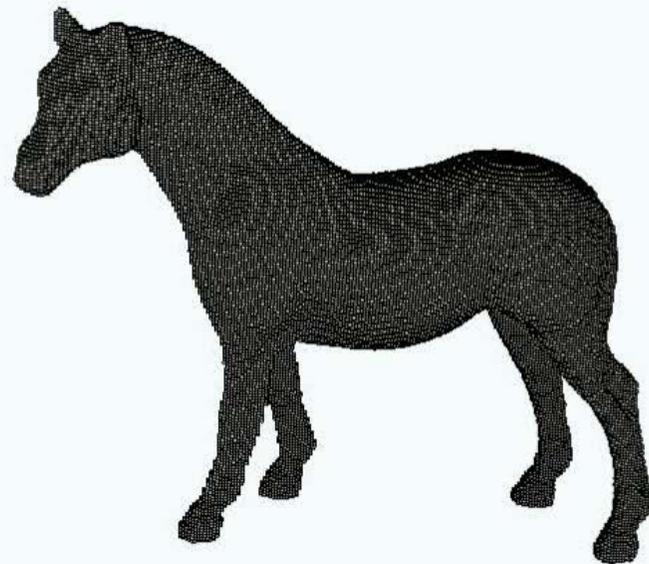
Numerical solution detail (potential and electric field) in physical domain



Comparing with the analytic solution, we have measured a maximum error in the potential of 0.88%.

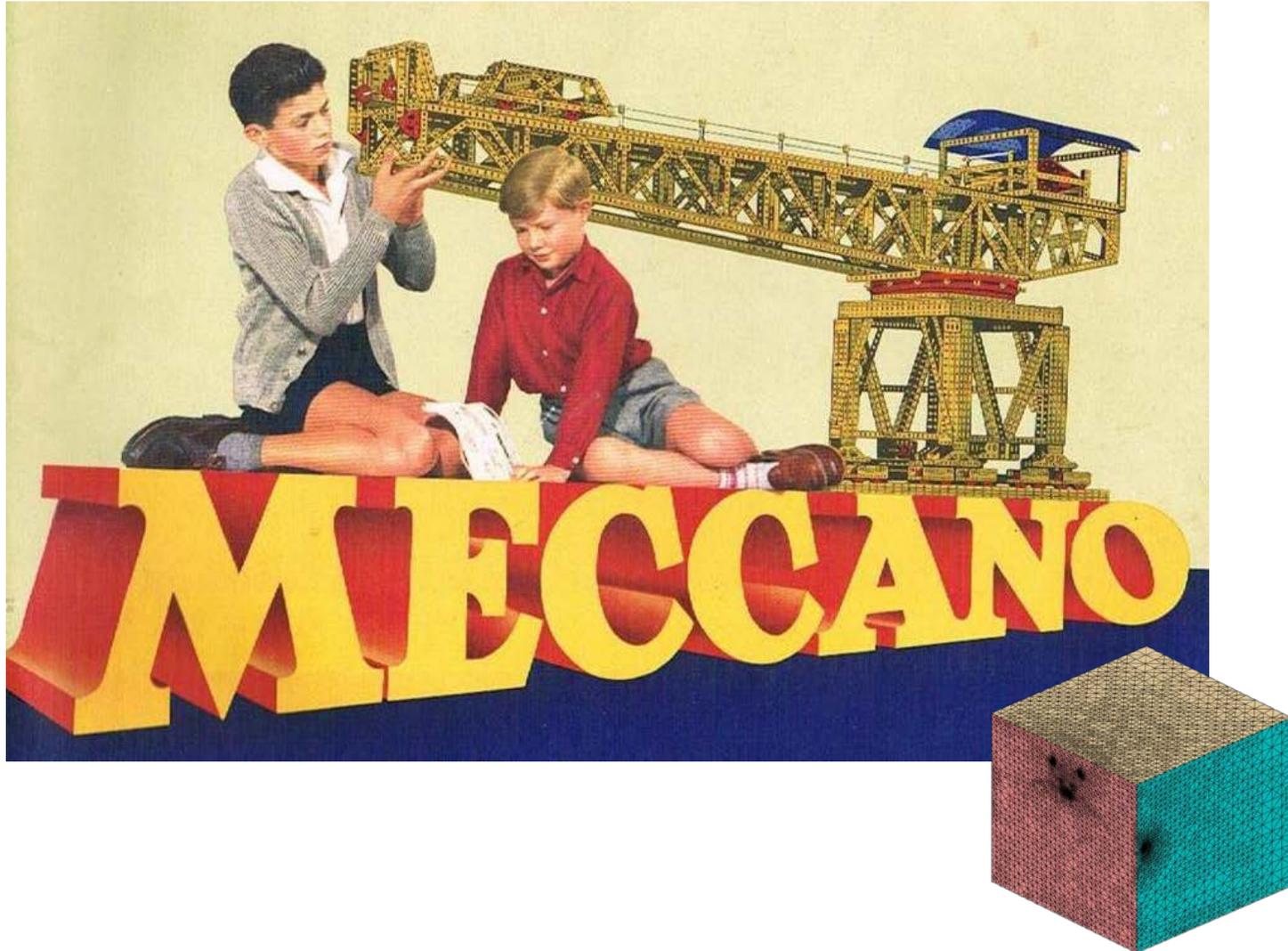
Final Comments and Future Works

Automatic Construction of the Meccano



Final Comments and Future Works

Automatic Construction of the Meccano





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Adaptive T-spline Refinement for Isogeometric Analysis in Planar Geometries

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**Isogeometric Analysis: Integrating Design and Analysis (IGA 2014),
January 8-10, 2014, Austin, Texas, USA**

MINECO y FEDER Project: CGL2011-29396-C03-00

CONACYT-SENER Project, Fondo Sectorial, contract: 163723

