



Building Materials in Dredging , Maritime and Waterfront Construction

**Ir. Bernard Malherbe
Jan De Nul Group**



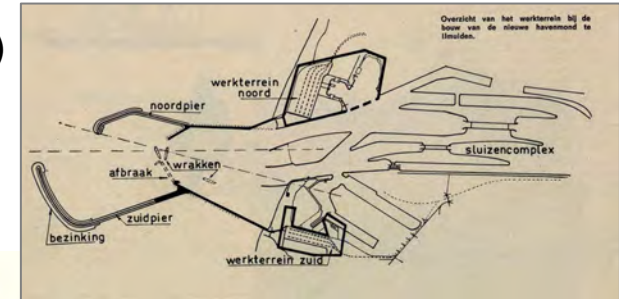
Types of Infrastructures & Constructions

- Breakwaters
- Seadikes & Riverdikes
- Bank- & Reclamation confinement/revetment
- Reclamations
- Quay-walls
- Locks
- Pumping culverts
- Berthing structures (dolphins,...)
- Sinkers
- Pipe – and cable-landfalls
- Beach & coastal protection structures

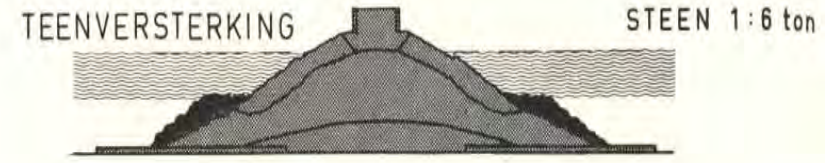
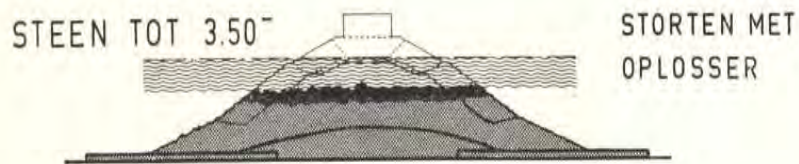
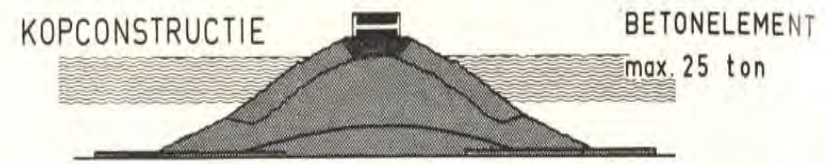
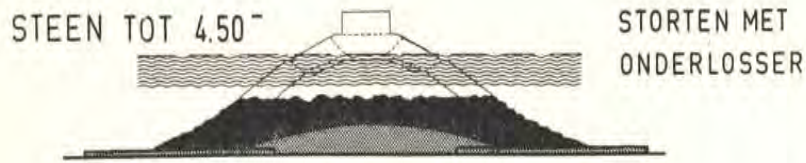
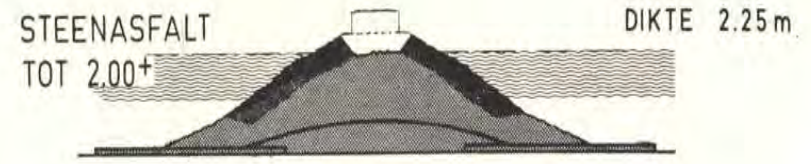
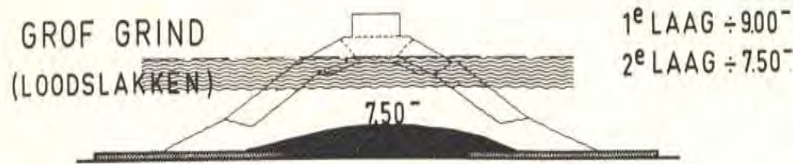
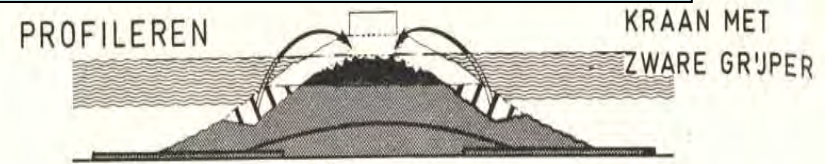
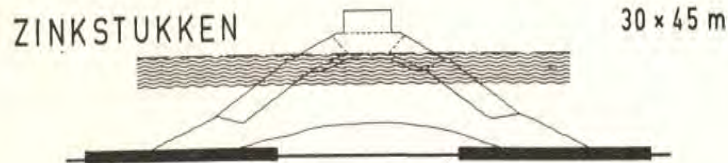




Port of IJmuiden (Nederland)
Construction method for breakwater extension: North & South Pier (1965)



Construction Stages of Rubble-Asphalt Breakwater



Underpart Breakwater

Upperpart Breakwater

Construction Method of IJmuiden breakwaters



13. De twee belangrijkste concepties van de Combinatie IJmuiden: onderlossers en hefpontons met kraan, beide geadviseerd en in opdracht van Rijkswaterstaat ontworpen.



To Poulseur (nabij Luik) staat een trein gereed voor vervoer van stenen naar IJmuiden.

Interopbouw van klein naar groot materiaal.

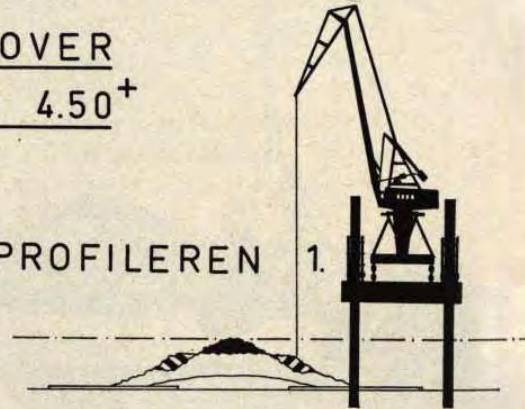
Construction method of IJmuiden's breakwaters

Werksituatie van de kraanhefeilanden.

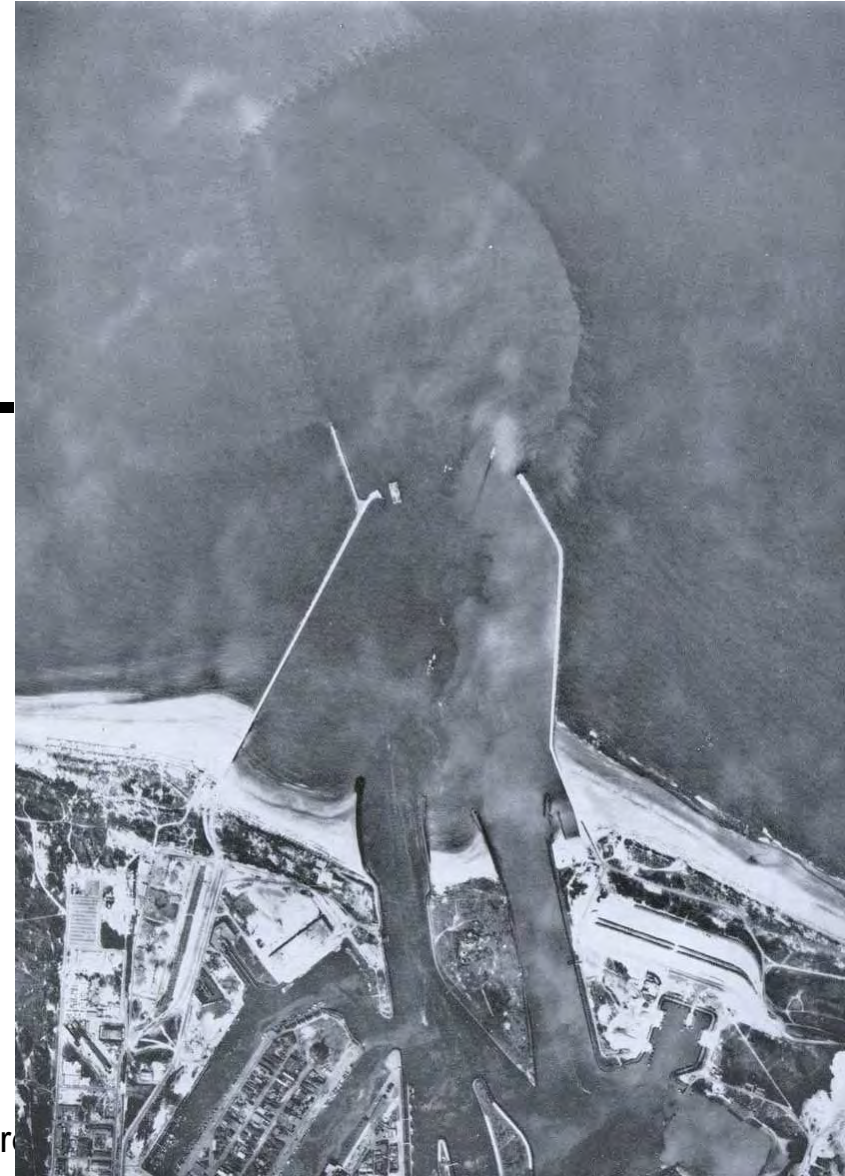
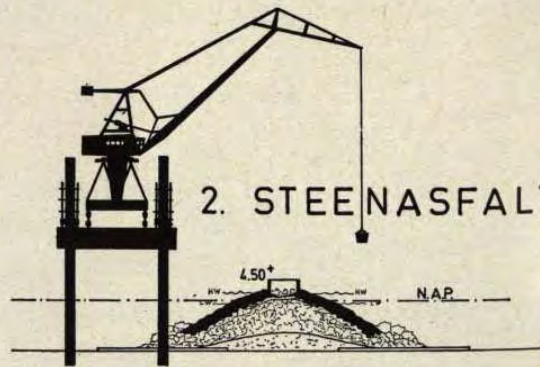
TRANSPORT OVER
HOGE DAM OP 4.50⁺



PROFILEREN 1.



2. STEENASFALT



Maritime & Dr

Port of Zeebrugge (Belgium) 1903-2003



Anno 1976



Anno 1990



Anno 2003

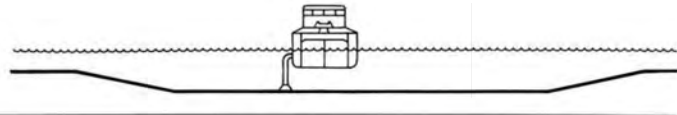


De positie van afzinkposten, zinkstuk en stenslurter gedurende het afzinken.

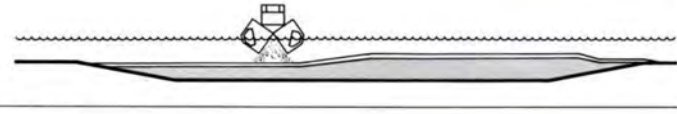


Construction sequence of Zeebrugge breakwaters

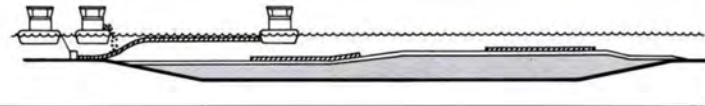
1. De sleuf uitbaggeren met sleepzuiger of cutterzuiger



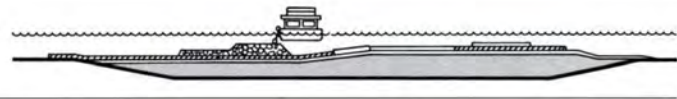
2. Grind storten op het geklepte zand



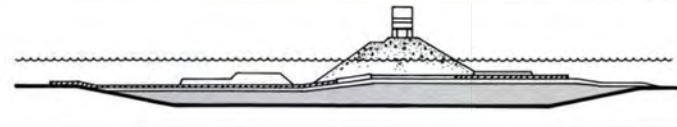
3. Zinkstukken afzinken



4. Bermen voor de bescherming van de damteent storten



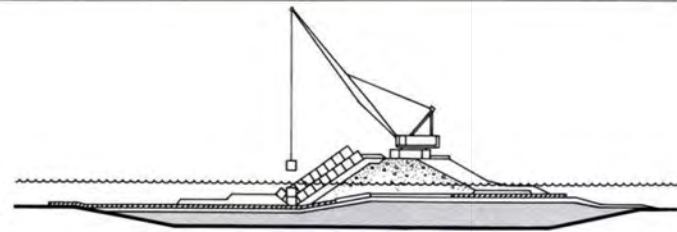
5. De damkern opbouwen met T.V. of 1-3 ton



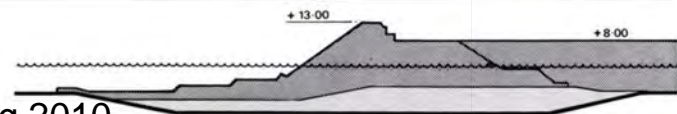
6. De 1-3 ton secundaire beschermlaag plaatsen



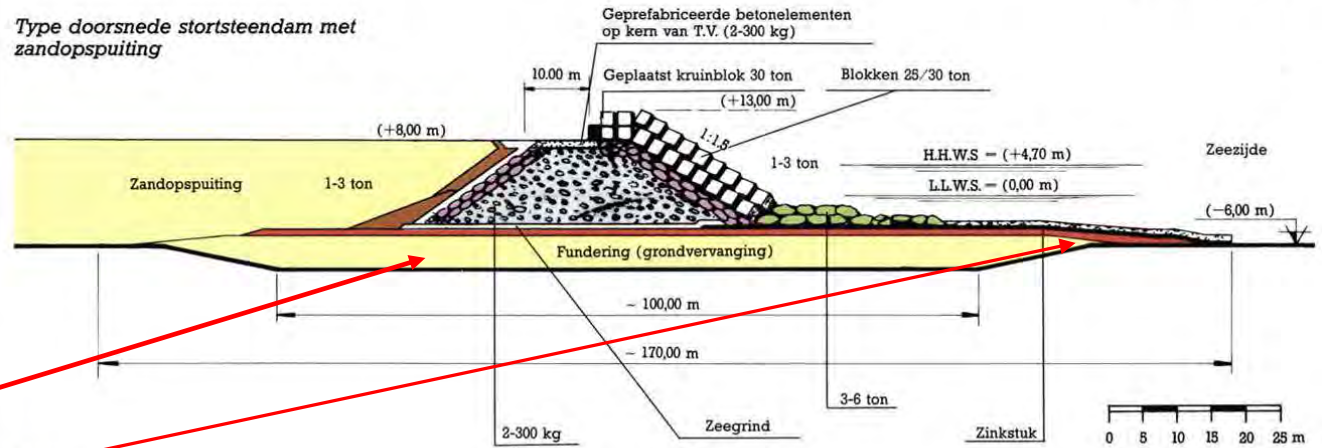
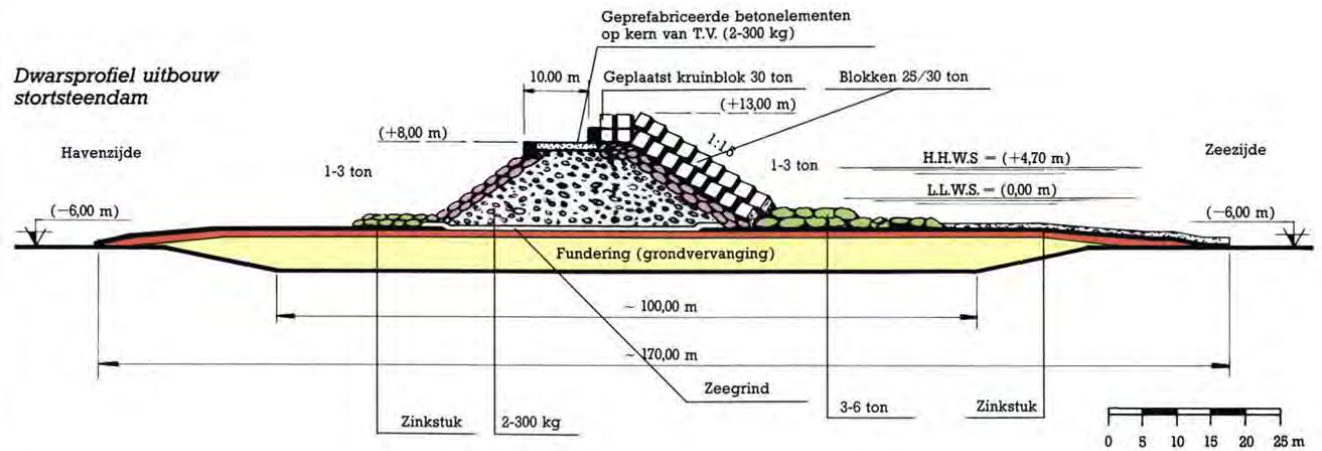
7. 25-30 ton betonblokken plaatsen



8. De kruin afwerken en eventueel zandopslag in de afzinkposten.



**Engineering design
of Zeebrugge
Rubble-Mound
Breakwaters on soft
soil: soil-
replacement and
erosion protection**



- Legende:
-  Geklept zand
 -  Erosiegrind
 -  Zinkstukken met steenballast
 -  Bermen in breuksteen van 3 à 6 ton voor de zeewaartse kant en 1 à 3 ton voor de havenzijde
 -  Filter tussen steen en zandopspuiting
 -  De damkern wordt met tout-venant gebouwd
 -  De damkern wordt afgedekt met breuksteen van 1 à 3 ton
 -  De zeewaartse kant van de dam wordt tegen golfaanval beschermd door het plaatsen van betonblokken van 25 tot 70 ton.



**Dredging of soft soil-replacement
trench & Construction of breakwater's
core**



Een zinkstuk op de zate.

Construction and placement of willow fascines for erosion protection of soft soil-replacement

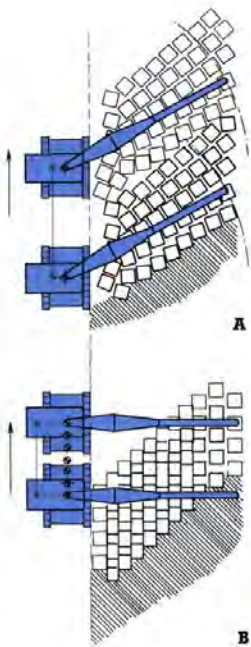


Maritime 8

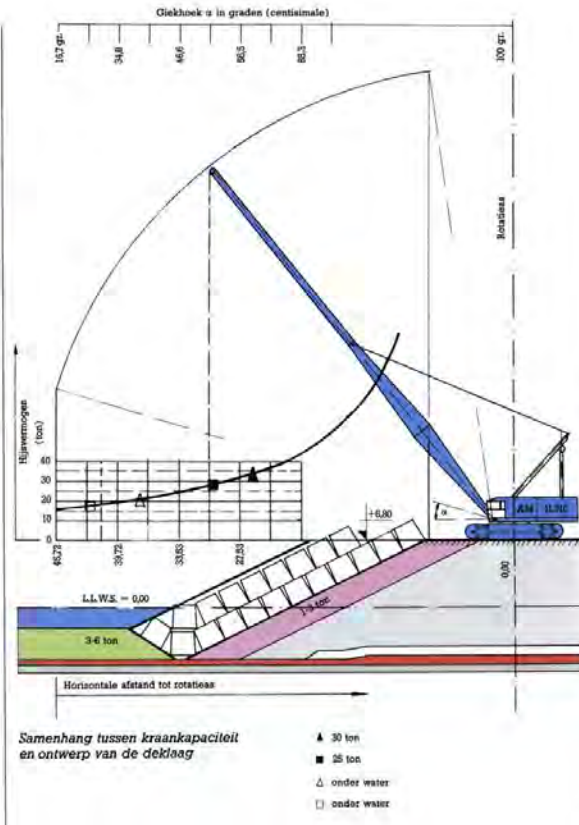
De positie van afzinkpontons, zinkstuk en steenstorters gedurende het afzinken.

Zeebrugge Port Extension: sequence of Rubble Mound Breakwater construction



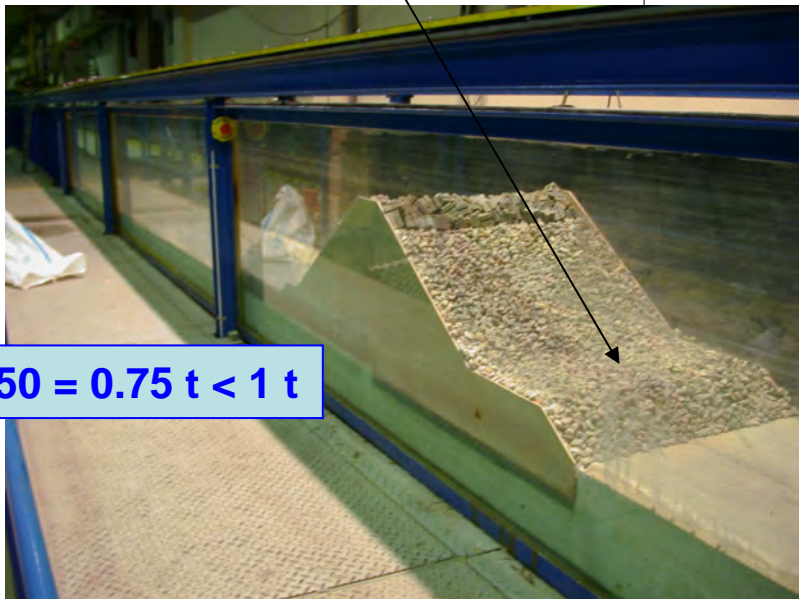
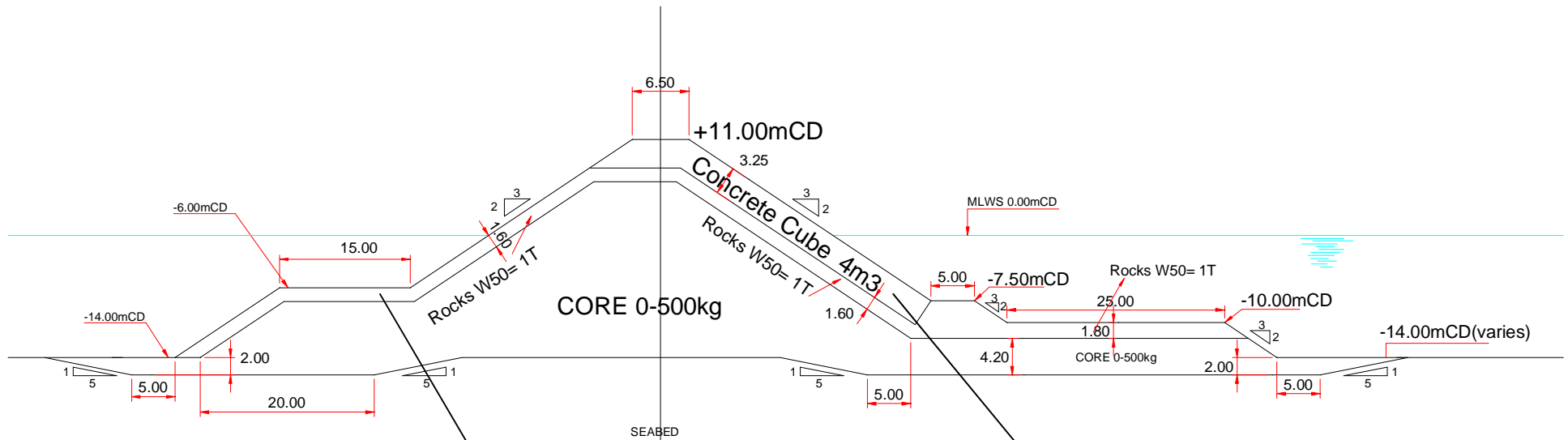


Plaatsingspatronen.

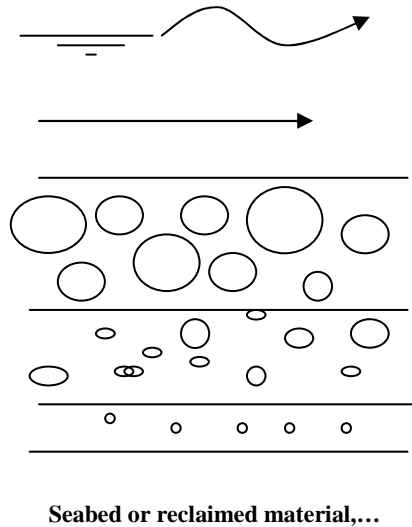


Zeebrugge Port Extension: placement of 25t to 28 t concrete armor units of Rubble Mound Breakwaters

Melchorita Breakwater, PERU LNG (anno 2007)



First engineering rule in maritime construction: Terzaghi filter rules



Armouring Layer

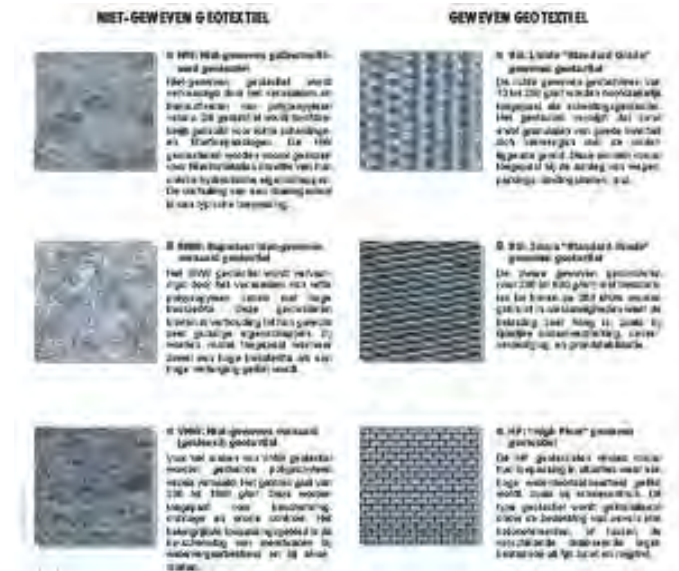
Underlayer

Filterlayer (mineral or geotextile)

Seabed or reclaimed material,...

Geotextile:

- woven fabric
- Non-woven fabric
- Material: PP, HDPE,...



Permeable but sand-tight construction:

$d_{15} \text{ upperlayer} / d_{85} \text{ underlayer} < 5$ (bulk of underlayer cannot migrate trough pores of upperlayer)

$d_{50} \text{ upperlayer} / d_{50} \text{ underlayer} = 15 \dots 60$

$d_{15} \text{ upperlayer} / d_{15} \text{ underlayer} = 5 \dots 40$

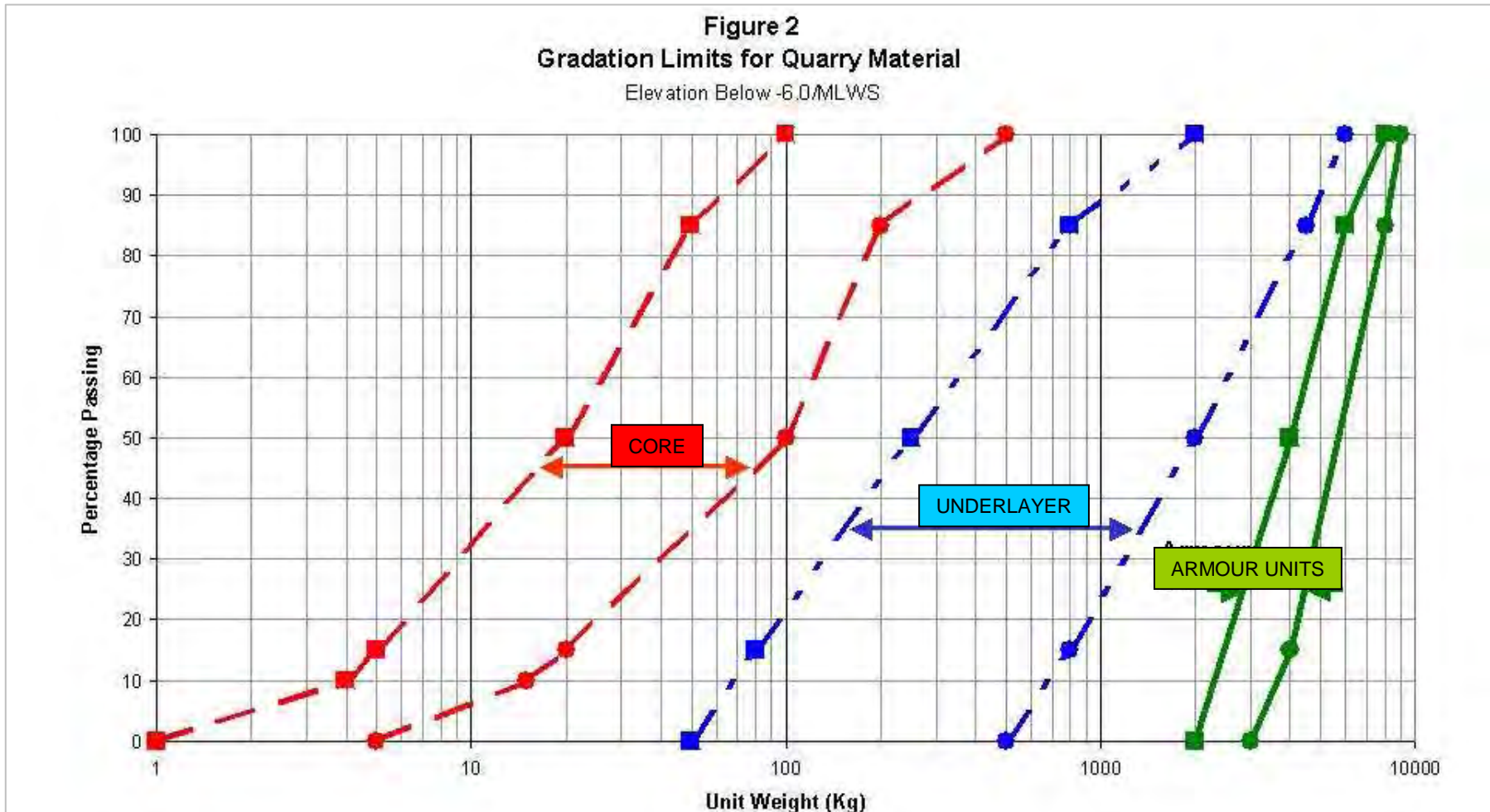
Layer thickness:

Filter-layer (e.g. gravel-sand): $> 0,10\text{m}$

Underlayer & Armour Layer: $3 \dots 5 \times d_{50}$

Maritime & Dredging 2010

Gradation of Maritime Construction Materials



UNIFIED SOIL CLASSIFICATION (ASTM D-2487-98)

MATERIAL TYPES	CRITERIA FOR ASSIGNING SOIL GROUP NAMES			GROUP SYMBOL	SOIL GROUP NAMES & LEGEND
COARSE-GRAINED SOILS >50% RETAINED ON NO. 200 SIEVE	GRAVELS >50% OF COARSE FRACTION RETAINED ON NO. 4. SIEVE	CLEAN GRAVELS <5% FINES	Cu>4 AND 1<Cc<3	GW	WELL-GRADED GRAVEL
			Cu>4 AND 1>Cc>3	GP	POORLY-GRADED GRAVEL
		GRAVELS WITH FINES >12% FINES	FINED CLASSIFY AS ML OR CL	GM	SILTY GRAVEL
	SANDS >50% OF COARSE FRACTION PASSES ON NO. 4. SIEVE	CLEAN SANDS <5% FINES	Cu>6 AND 1<Cc<3	SW	WELL-GRADED SAND
			Cu>6 AND 1>Cc>3	SP	POORLY-GRADED SAND
		SANDS AND FINES >12% FINES	FINED CLASSIFY AS ML OR CL	SM	SILTY SAND
FINE-GRAINED SOILS >50% PASSES NO. 200 SIEVE	SILTS AND CLAYS LIQUID LIMIT<50	INORGANIC	PI>7 AND PLOTS>'A' LINE	CL	LEAN CLAY
			PI<4 AND PLOTS<'A' LINE	ML	SILT
	SILTS AND CLAYS LIQUID LIMIT>50	INORGANIC	PI PLOTS >'A' LINE	CH	FAT CLAY
			PI PLOTS <'A' LINE	MH	ELASTIC SILT
		ORGANIC	LL (oven dried)/LL (not dried)>0.75	OL	ORGANIC CLAY OR SILT
			LL (oven dried)/LL (not dried)>0.75	OH	ORGANIC CLAY OR SILT
HIGHLY ORGANIC SOILS		PRIMARILY ORGANIC MATTER, DARK IN COLOR, AND ORGANIC ODOR	PT	PEAT	

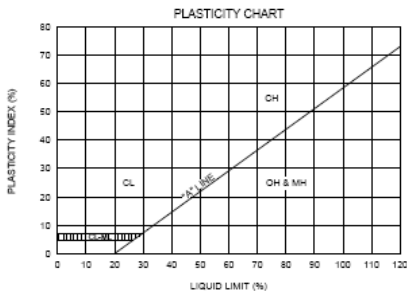
OTHER MATERIAL SYMBOLS	
Poorly Graded Sand with Clay Clayey Sand Sandy Silt Low to High Plasticity Clay Poorly Graded Gravelly Sand Topsoil Well Graded Gravel with Clay Well Graded Gravel with Silt	Sand Silt Well Graded Gravelly Sand Gravelly Silt Asphalt Boulders and Cobble

SAMPLE TYPES

- Split Spoon
- Shelby Tube
- Rock Core
- Grab Sample

ADDITIONAL TESTS

- | | | |
|---|---|--|
| CA - CHEMICAL ANALYSIS (CORROSIVITY) | (200) - (WITH % PASSING NO. 200 SIEVE) | |
| CD - CONSOLIDATED DRAINED TRIAXIAL | | SW - SWELL TEST |
| CN - CONSOLIDATION | | TC - CYCLIC TRIAXIAL |
| CU - CONSOLIDATED UNDRAINED TRIAXIAL | | TV - TORIVANE SHEAR |
| DD - DIRECT SHEAR | | UC - UNCONFINED COMPRESSION |
| FP - POCKET PENETROMETER (TSF) | | (1.5) - (WITH SHEAR STRENGTH IN KSF) |
| (3.0) - (WITH SHEAR STRENGTH IN KSF) | | UU - UNCONSOLIDATED UNDRAINED TRIAXIAL |
| RV - R-V ALUE | | |
| SA - SIEVE ANALYSIS: % PASSING #200 SIEVE | | WA - WASH ANALYSIS |
| VA - WATER LEVEL (WITH DATE OF MEASUREMENT) | (200%) - (WITH % PASSING NO. 200 SIEVE) | |



PENETRATION RESISTANCE (RECORDED AS BLOWS / 0.5 FT)			
SAND & GRAVEL		SILT & CLAY	
RELATIVE DENSITY	BLOWS/FOOT*	CONSISTENCY	COMPRESSIVE STRENGTH (TSF)
VERY LOOSE	0 - 4	VERY SOFT	0 - 0.25
LOOSE	4 - 10	SOFT	0.25 - 0.50
MEDIUM DENSE	10 - 30	FIRM	0.50 - 1.0
DENSE	30 - 50	STIFF	1.0 - 2.0
VERY DENSE	OVER 50	VERY STIFF	2.0 - 4.0
		HARD	OVER 4.0

* NUMBER OF BLOW OF 140 LB HAMMER FALLING 30 INCHES TO DRIVE A 2 INCH O.D. (1-3/8 INCH I.D.) SPLIT-BARREL SAMPLER THE LAST 12 INCHES OF AN 18-INCH DRIVE (ASTM-1586 STANDARD PENETRATION TEST).

Determining parameters for:

• Non-cohesive grains:

- grain-size distribution
- volume-mass & specific density
- permeability

• Cohesive grains:

- water content (w) & Atterberg Limits (SL, PL, LL)
- Plasticity-Index : $PI = LL - PL$
(PI = high > Clay; PI = low > Silt)
- Liquidity Index: $LI = (w - PL) / (LL - PL)$
- Activity : $A = PI / (\% < 0,075\text{mm})$
(A < 0,75 Inactief; A 0,75-1,25: Normal; A > 1,25: Active)
- shear resistance, cohesion
- deformation properties (compressibility,...)
- permeability

LGSJL 11/11/07 - GINTI US LAB GPJ - 8/26/08

A. Natural Building Materials

Clay

- **What is Clay ?**

For geologists, Clay is a fine-grained sediment, constituted of mainly aluminosilicate minerals (> 45 %), that are plate or flake-like grains with equivalent Stoke's diameters of 0,020 mm en 0,0001 mm.

For geotechnicians, Clays are soils constituted of particles with equivalent Stoke's diameters lesser than 0,002mm. Geotechnicians distinguish between under- normal or over-consolidated Clays, depending upon their consolidation degree as a function of their overburden history.

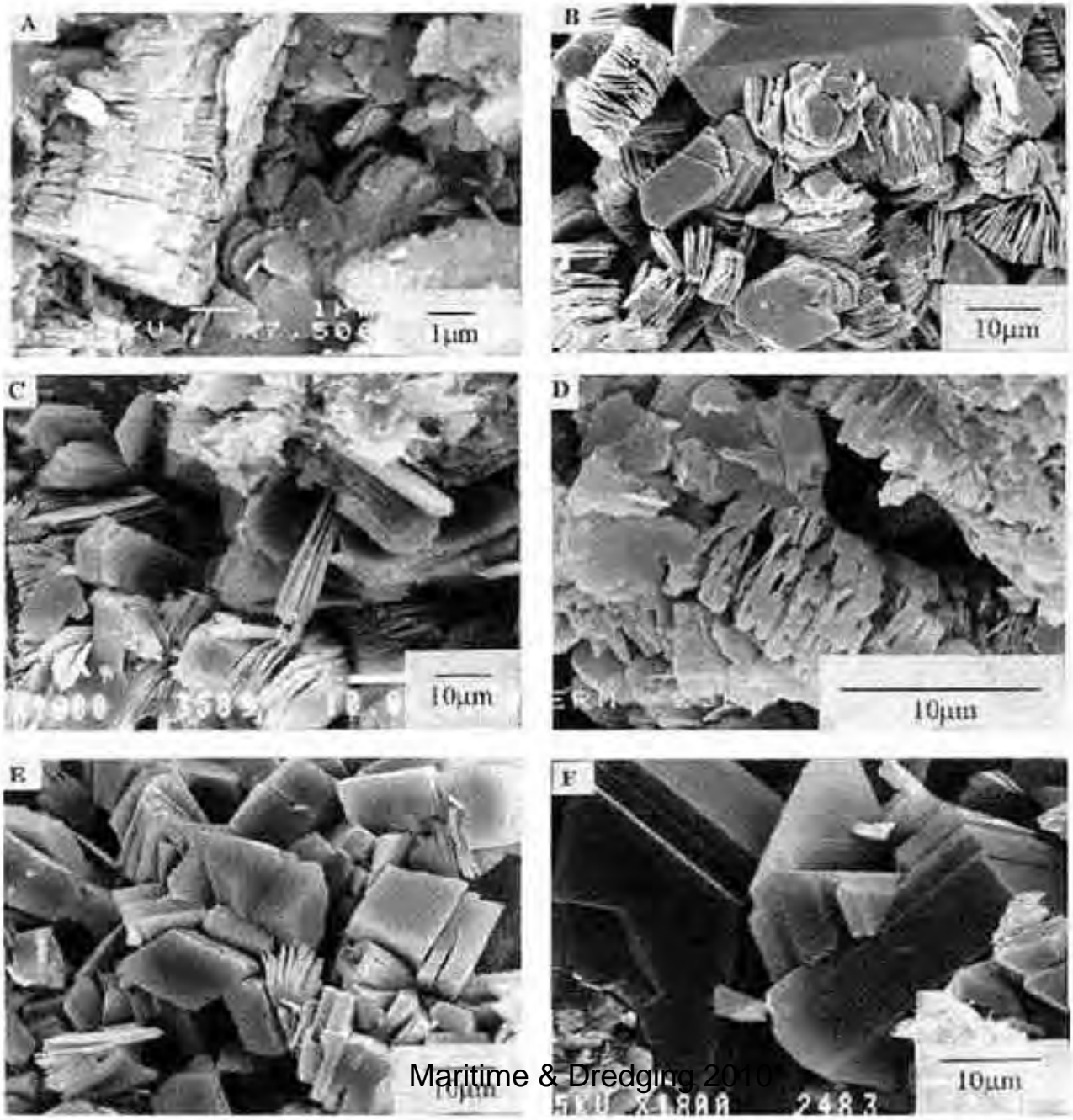
- **Typical geotechnical properties of Clays**

Low water-content : $w < 35 \%$

Low permeability : $k < 10^{-11} \text{ m/sec}$

High cohesion : $c_u = 10 \text{ tot } 150 \text{ kPa}$

Electronic microscope shots of Clay Minerals Illite & Kaolinite

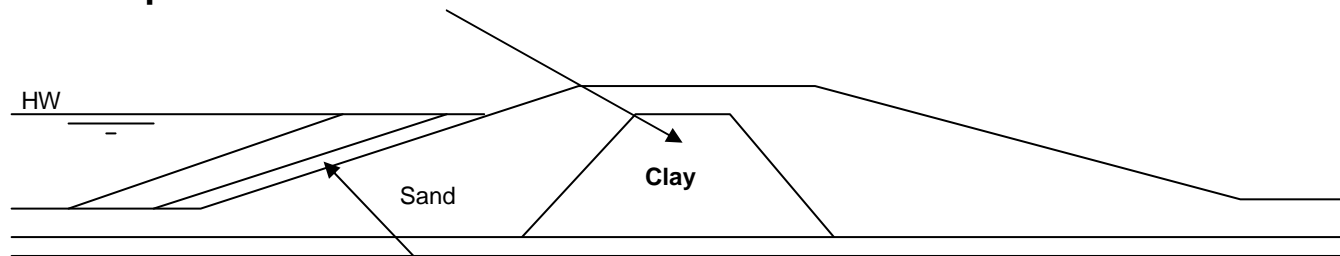


Maritime & Dredging 2010

Clay as Building Material

- **Domain of application of Clays**

- **Impermeable cores of dikes**



- **Impermeable revetment of water-retention dikes**

- **Colmatation layer of upland disposal facilities, ponds,...**

- **Workability of Clay depends upon**

- Plasticity**

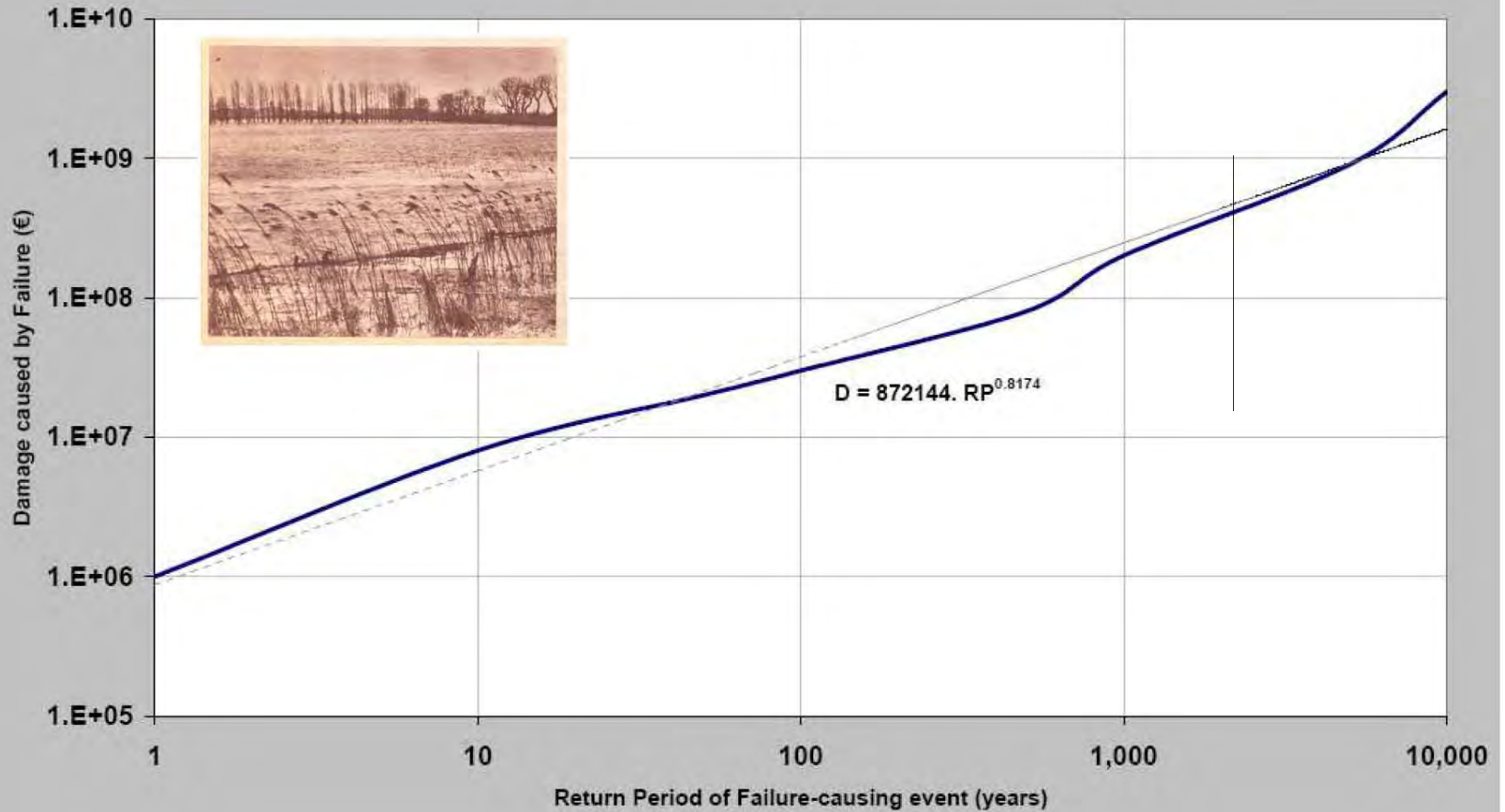
- Natural water-content close to PL**

Waterfront-dikes as water-retention structures: body of sand with clay-core

- **Deltaplan (Netherlands)**
- **Sigma Plan (Belgium)**



Waterfront Engineering :
Risks (of failure-induced damage) = Probability (of failure) x Damage (resulting from failure)



— Water-retention dikes

Mud



- **What is Mud ?**

Mud is a mixture-sediment : a mixture of fine sand, silt - particles (0,063mm to 0,002mm) and clay-minerals. Generally Mud has a high content in organic fractions (2 to 10 %) and CaCO_3 (till 35 %).

Mud is the typical sediment for estuaria, shallow seas and sheltered deposition areas. Mud has generally a high water-content. Mud is the building material for what will become Clay after consolidation.

Mud is a cohesive sediment with low shear-strength. Till recently, Mud was considered as inappropriate for recycling or re-use.

- **Geotechnical properties of Mud:**

High water- content : $w = 100$ to 250 %, , beyond LL

Medium to high cohesion: $c_u = 1$ tot 30 kPa

Flocculation (aggregation to larger particles, called Flocks)

Sand-admixture (co-precipitation in flocks)

Transition sediment between suspensions and soil: classic geotechnical laws do not apply...rheology is the science of stress-strain behaviour for such Non-Newtonian Fluids. Parameters influencing shear-strength: initial rigidity (yield stress) , dynamic viscosity and thixotropy (typical for Bingham fluids, a particular form of Non-Newtonian fluids)

Mud as Building Material

After dewatering (accelerated consolidation by lagooning, sun-drying, filter-pressing, chemical dewatering,....), Mud can reach dry-volume-masses of 500 to 600 kgds/m³ (bulk-densities of order of 1,45 to 1,60).

Dewatered Mud can be re-used as an impermeable, cohesive, shapeable building-material with low-permeability: landscaping voor sight or sound-screen, fill-material with high deformation properties,.....

Gravitational dewatering by lagooning (load : 400 to 600 kgds/m²)

Mechanical dewatering by chamber filter-presses.

Chemical dewatering by admixture of CaO (8 to 16 %): exothermic reaction (evaporation) and water-adsorption.

Lagooning of Dredged mud, Ring-canal in Ghent, Belgium

ENVISAN Grondverwerkingscentrum
Hulsdonk

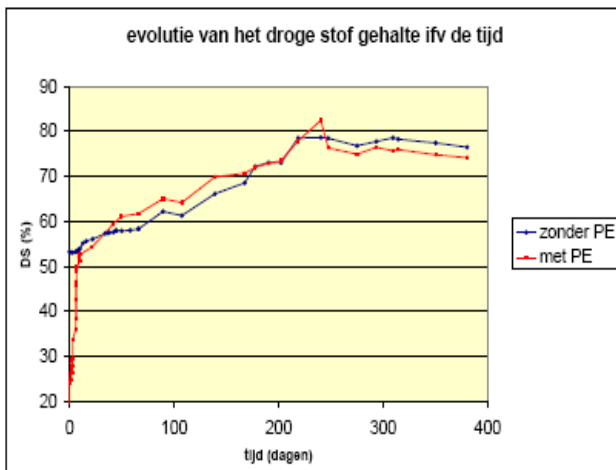


Day 1: just after filling the experimental lagoon with fresh Mud

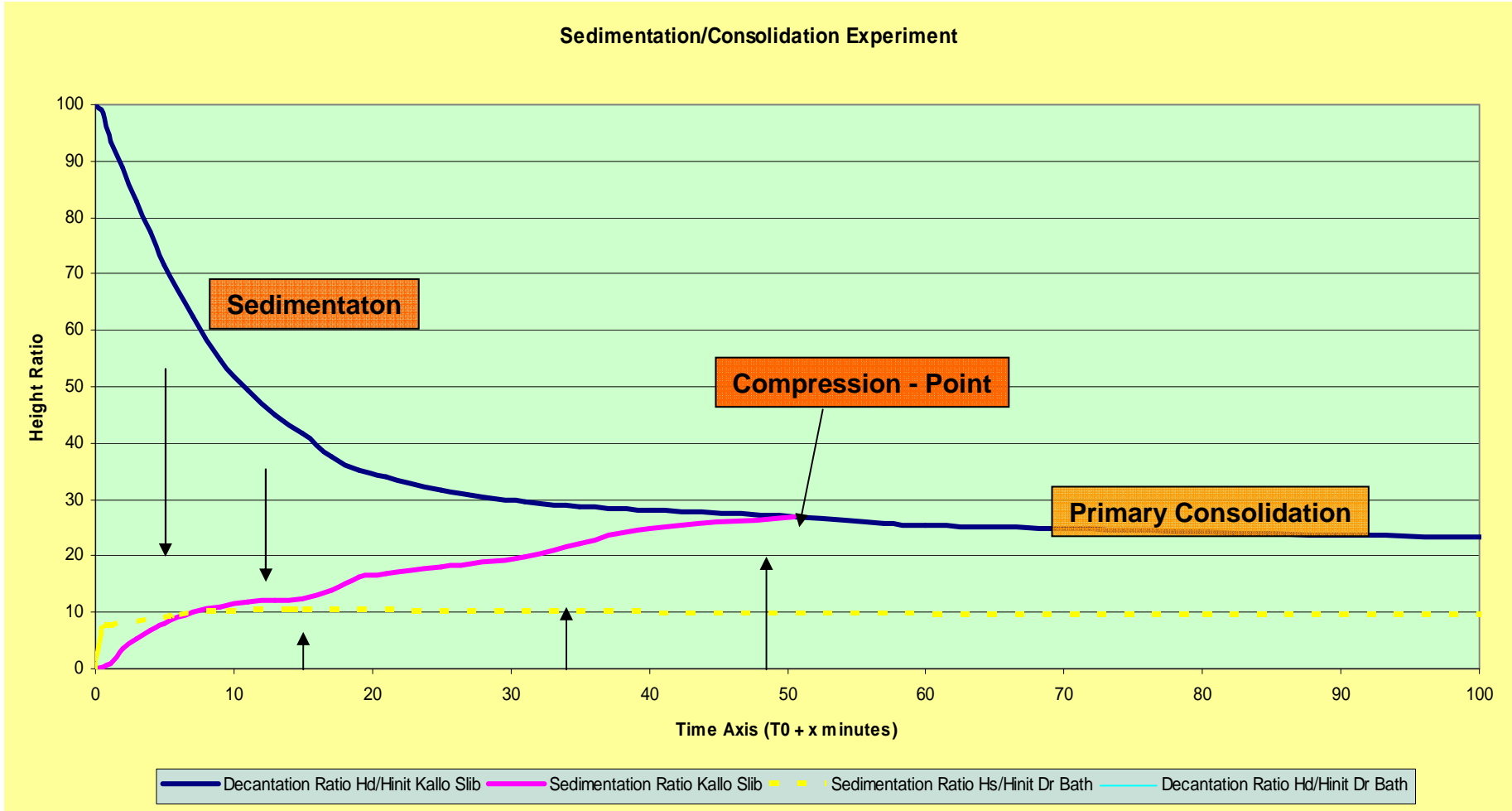


Day 36: Crust-drying with superficial cracks

Day 100: After crust-revolving



Decantation and Consolidation Properties of Mud



Sand

- **What is Sand ?**

Sand is typically a detrital sediment, constituted of individual particles and with a relatively low intergranular cohesion. The particles have equivalent Stoke's diameters of 0,063 mm to 2 mm.

Sand-grains are generally mono-mineral particles of Quartz (Si O_2), Feldspars (Al, Mg Si O_4) or of organic origin: these latter are generally coral-fragments, shell-fragments,...constituted of Calcite, Aragonite, (Ca Co_3).

- **Geotechnical properties of sands are:**

Low in-situ water-content : $w < 35 \%$

High permeability : $k > 10^{-6}$ m/sec

Subrounded or rounded grains of 0,063 mm to 2,0 mm

Sorting degree, d_{50} , d_{90} ,....of grain-size distribution

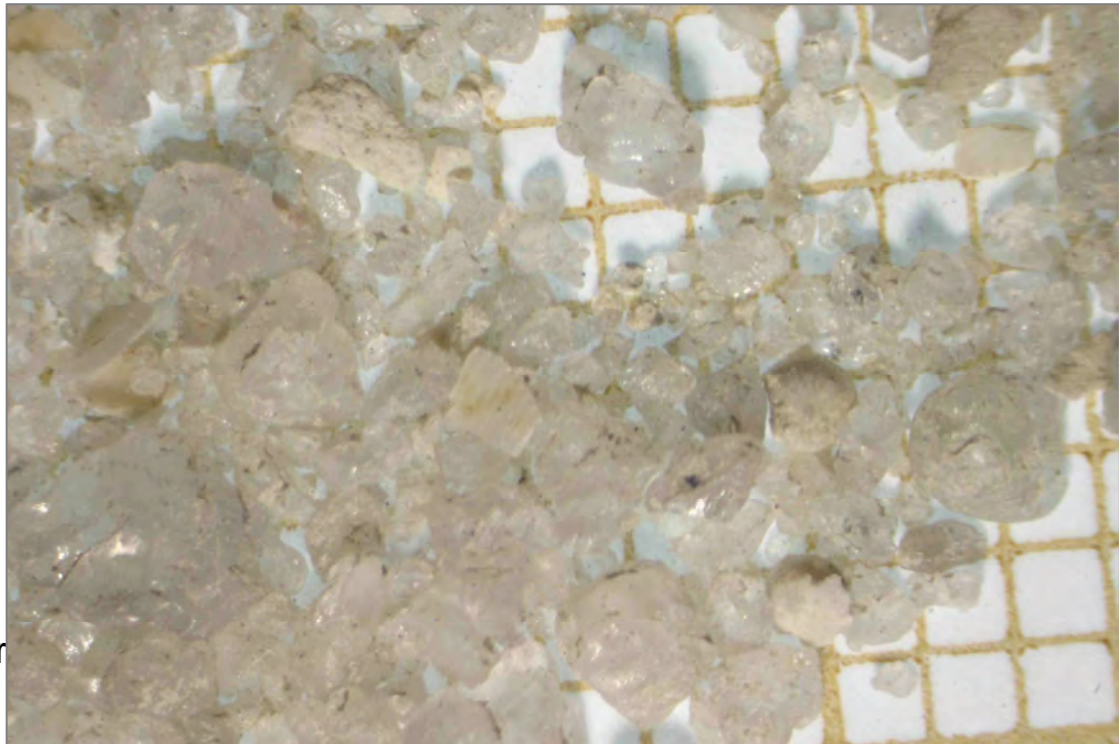
Compaction properties with generally a rapid compaction and a maximum compaction-density corresponding to a typical water-content (Proctor-density)

Angle of Internal Friction (varying between 27° and 40°) , determining shear-strength, equilibrium inflow-slope, active/passive soil stresses,...



Carbonate sand (Dubai)
d50 = 0,654 mm

Quartz sand (S Afrika)
d50 = 0,700mm

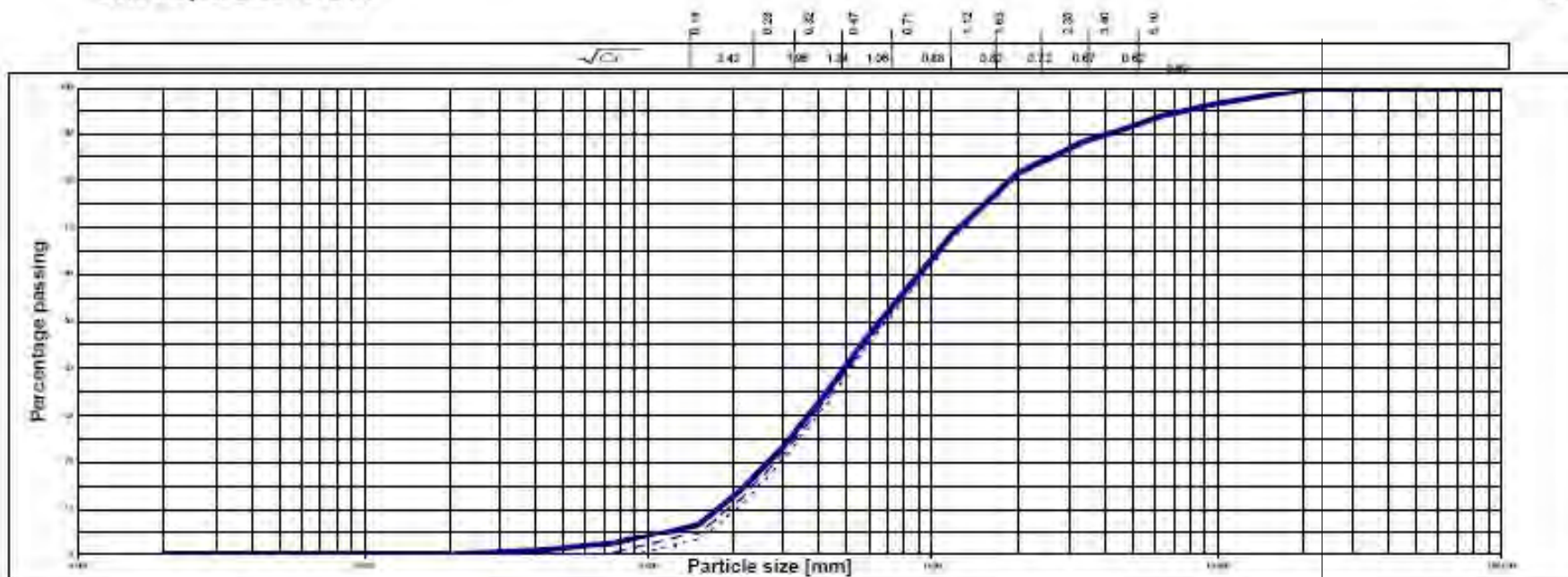


Mar

Grain-size distribution of Carbonate Sand

Sieve analyses Dubai TSHD.xls

15/10/20



Clay	Silt 2%			Sand 79.5%			Gravel 18.5%			C & B
0%	fine 0%	medium 0%	coarse 2%	fine 10.9%	medium 34.4%	coarse 34.3%	fine 11.7%	medium 6%	coarse 0.7%	0%



1	d_{50} [mm]	d_{mf} [mm]	$\sqrt{d_r}$	ψ	$\sqrt{d_r}$ old
full sample	0.654	1.124	1.413	0.814	1.185
without fraction < 0.09 mm	0.691	1.177	1.341	0.843	1.231
without fraction < 0.083 mm	0.675	1.154	1.379	0.831	1.379
reduced fraction < 0.14 mm reduced to 20%	0.654	1.124	1.413	0.814	1.185

Sand as Building Material

Sand is generally easy to excavate, to dredge, to transport and to reclaim (provided it is not too dilatant). Sand is also relatively cheap a building material, and depending upon reserves, hauling distances generally with prices within 4 to 15 €/m³.

Therefore is sand one of the most widely used building materials in waterfront and maritime engineering.

Applications are:

- **Bulk of dikes**
- **Beach-restaurations**
- **Land-reclamations**
- **Dike-reinforcements**
- **Aggregate for concrete**
- **Drainage-layers on disposal facilities**
- **Core of breakwaters**
- **Soil-substitution material**
- **....**



One of the World's largest land-reclamations: Chek Lap Kok airport in Hong Kong (1982)

Hydraulic fill of dredged sand and accelerated consolidation with vertical drains



Land-reclamation at Pulau Tekong, Singapore (740 Mm³, 1999)



Maritime & Dredging 2010

Reclamation of Western Port Area at Zeebrugge (Belgium) for Flanders Container Terminal, FCT

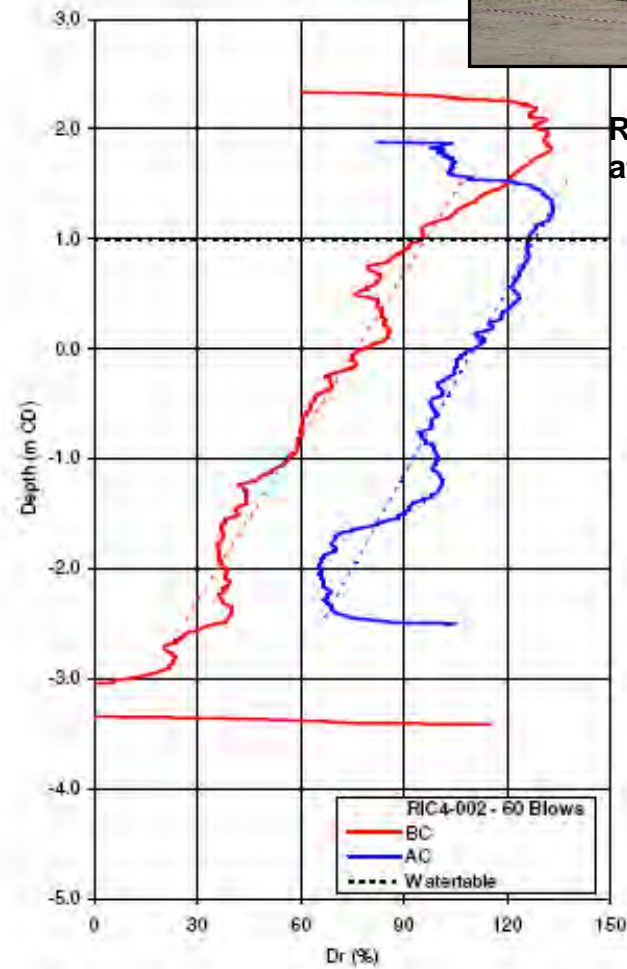
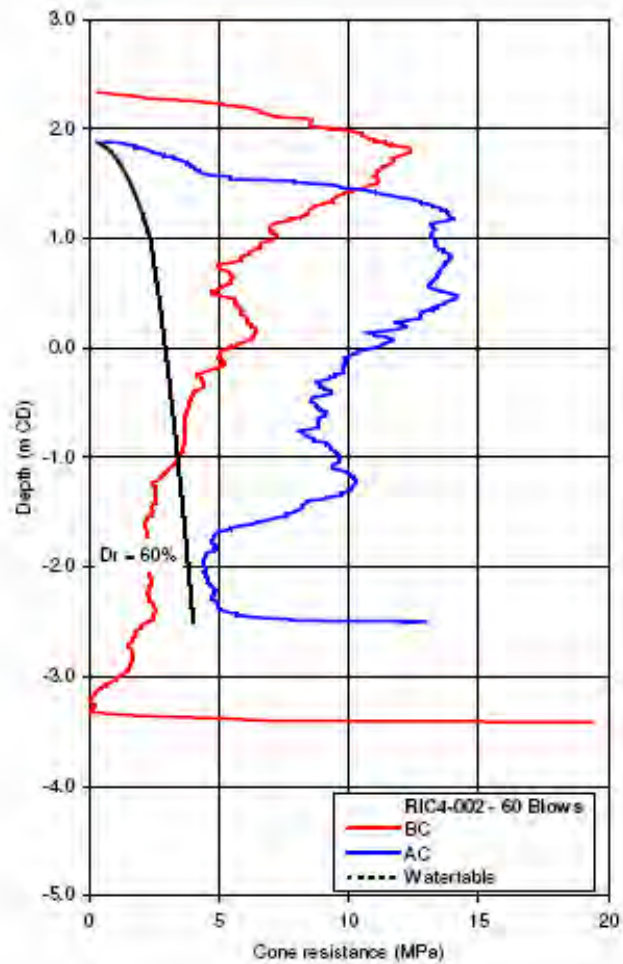


Maritime & Dredging 2010

Compaction of hydraulic sand-fills



Rapid Impact Compaction (RIC),
at Ras Laffan Port, Qatar

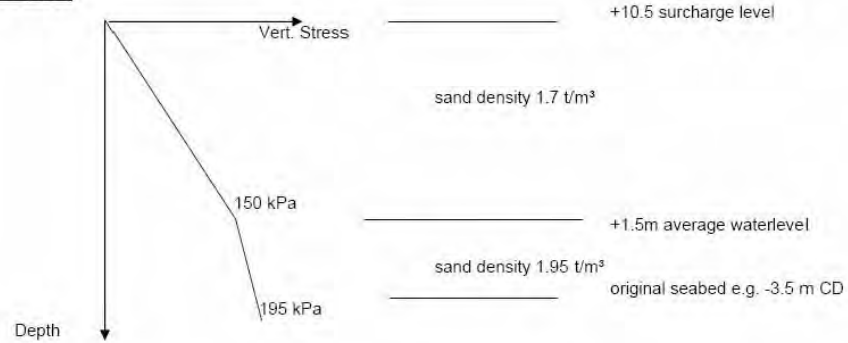


Compaction typical results

VEB #####

Compaction degree of reclaimed and dumped sand

A. Layout



B. Compaction degree

normal values relative density in reclaimed and dumped sand

reclaiming above waterlevel : D: 50%-60%	ϕ : 37.5%-40%
dumping below waterlevel : D 40%-50%	ϕ : 35%-37.5%
reclaiming below waterlevel : D 15%-35%	ϕ : 27.5%-35%

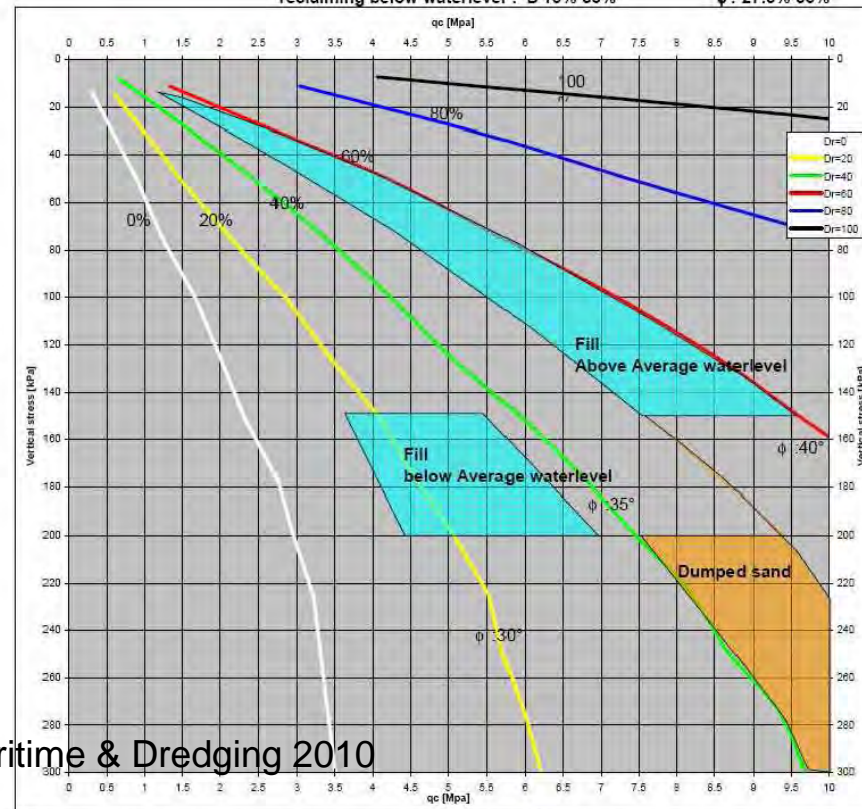
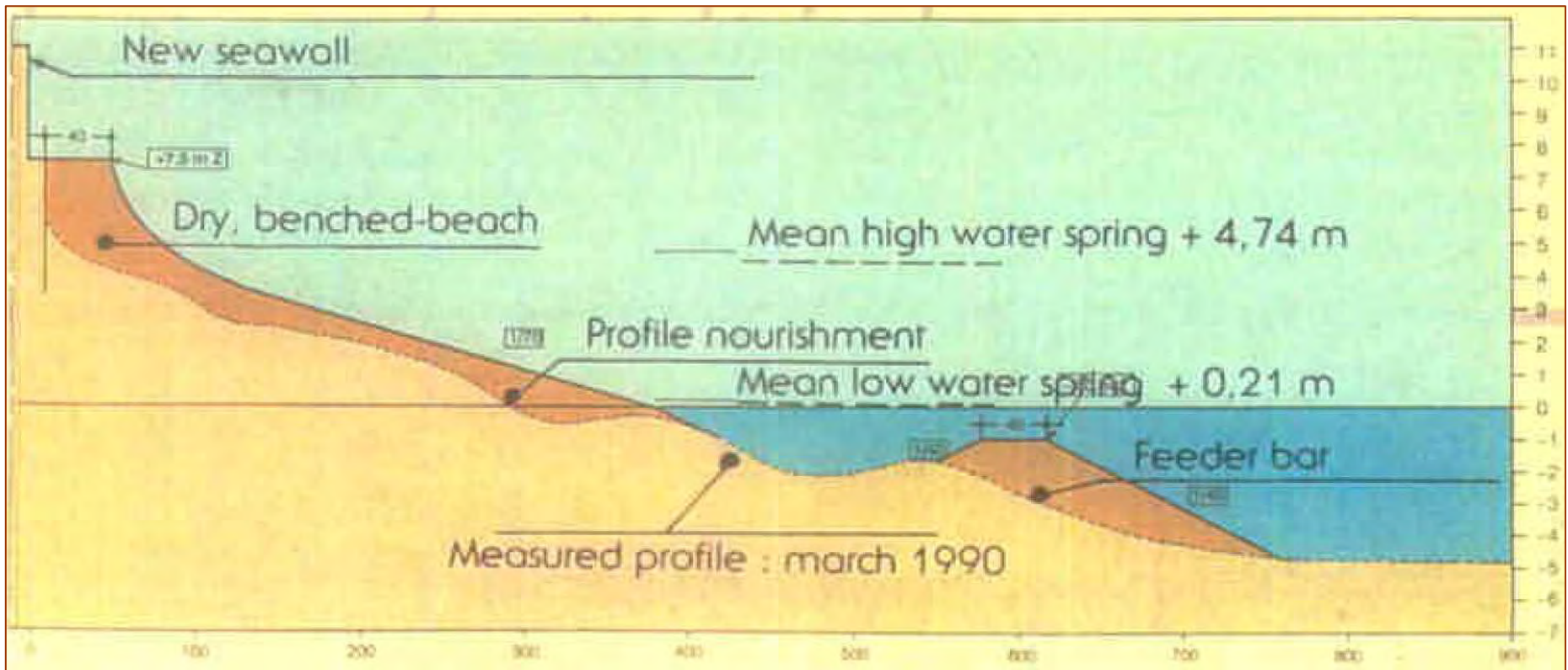


Table 1. According to Schmertzmann(1978) , Villet and Mitchell (1981))

Classic Beach Replenishment: reclaiming supratidal beach at Cancùn, Mexico



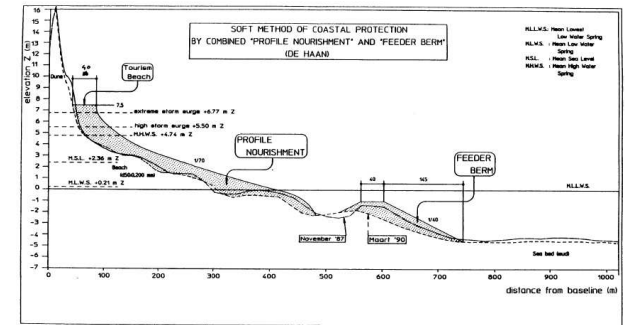
Sand as building material for Coastal Protection: Profile Nourishment and Feeder Berm for “soft” coastal protection at De Haan, Belgium



Dumping Feeder Berm



**De Haan Coastal Protection Works:
a major pioneering achievement.
Less than 5 % losses per year
during the first 10 years.**



Gravel

- **What is Gravel ?**

Gravel is a detrital sediment, constituted of individual particles with almost no intergranular cohesion. Particles have typically equivalent Stoke's diameters between 2 and 64 mm.

Gravel-particles are either mono-mineral particles like Silex (Si O_2), either rock-fragments of Limestone, Granite, Basalt,..

Gravel can also be fabricated by crushing rock

- **Geotechnical properties and determining parameters of gravel are:**

Specific volume-mass: between 2600 and 2800 kg/m³

Grain-shape and form

Sorting-degree of grain-size distribution

Abrasivity

Gravel as Building Material

- **Filterlayer between sand and rubble-mound rock-layers**
- **Ballast material in caissons**
- **Protection-layer of geotextiles**
- **Bedding and blinding layer under concrete blocks, caissons,... (quay-walls)**
- **Back-wedge of gravity quay-walls to decrease active soil pressure**
- **Bank-revetment**
- **Ballasting of fascine-matresses**
- **Backfill of pipeline/cable trenches**
- **Erosion-protection at toe of structures**
- **Gravel-columns for consolidation of low-bearing capacity soils**
- **Soil-substitution material**
- **.....**



Rocks



What is Rock ?

Rock is either an assemblage of crystallized minerals (Igneous and Metamorphic Rocks) or of sediment-particles (Sedimentary rocks) or the result of massive bio-chemical precipitation of specific minerals ((Limestones,...). Rock for waterfront/maritime engineering is produced in quarries, according to specific criteria of grading.

Rock is produced by blasting, break-hammering or cutting geologic rock-formations and grades run from 'Quarry-run' (the rest-product of quarry) to Underlayer Rock and Armour Rock, till individual rock-weights of approx. 10ton.

Rocks to be used in waterfront-engineering such as rubble-mound breakwaters must comply to a number of criteria, such as:

- **homogeneity of rock-formation**
- **high specific density (> 2.400 kg/m³)**
- **limited internal faulting**
- **limited abrasivity and brittleness,...**

Rocks that generally fulfill these criteria are massive Limestones, Granites, Diorites, Quartzite,....

Rocks that often exhibit brittleness are: Basalt, Gabbro,...

Rocks that often exhibit abrasivity are: Calcareous Sandstone...

Advantages of Natural Rock in Waterfront engineering are numerous:

- **Easy to install: smaller fraction can be placed in bulk, coarser fraction (> 1 ton) with standard heavy-duty crawler cranes, hydraulic excavators,...**
- **Easy to maintain**
- **Flexibile adaptative to subsoil settlements or irregularities**
- **Extremely sustainable for limestones, granites,...provided a number of rock-mechanic characteristics-criteria are fulfilled**
- **Manageable prices (between 40 tot 100 €/ton: quarried, transported and installed)**
- **Wide range of grades:**
 - **Fine grades: 30/60 mm, 40/100 mm, 50/150 mm, 90/200 mm**
 - **Medium grades: 5/40 kg, 10/60 kg, 40/200 kg , 60/300 kg**
 - **Coarse grades: 300/1.000 kg, 1.000/3.000 kg, 3.000/6.000 kg, 6.000/10.000 kg**



Granite Quarry, Seychelles



Limestone quarry at Al-Kabra, Saudi Arabia



Quarry operations for producing rocks

Jumbo-Drilling of drill-holes



Loading & transport of blasted rocks



Bulk- placement of breakwater-core, Dubai, UAE

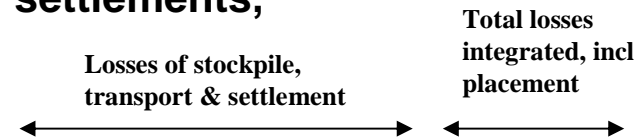


Determining Parameters of Rocks:

- **Color:** for aesthetic or environmental reasons (visual-impact, landscape-integration,...)
- **Specific Density :**
 - **Oven-dry density ρ_d (in kg/m³)**
 - **Density after water-absorption (in kg/m³)**
- **waterabsorption: $W_{ab} = 100 \times \text{Mass of water absorbed/Dry Mass}(\%)$**
- **intrinsic porosity : $Por = ca. W_{ab} \times \rho_d$**
- **weathering degree**
- **homogeneity: internal faulting, layering, veins (Quartz,...),...**
- **compression strength UCS (Uniaxial Compression Strength in MPa)**
- **tensile strength**
- **acoustic properties V_{acc} (m/sec):**
- **abrasion-resistance: inter-rock abrasivity (Micro-Deval test)**
- **resistance to frost/thaw cycli**
- **drop-test resistance**
- **bulk porosity of rock-layer :**
 - **quarry – Run : 33 %**
 - **Filter-Layer (5 – 60 kg): 39 %**
 - **Underlayer (60 kg – 1000 kg): 38 %**
 - **Armour Layer (1000 kg – 10 t): 36 %**

Loss in rock between Quarry weighing-bridge and final placement in breakwater.

(Losses are due to intermediate stockpiling, settlements, losses during placement,...)



Layer	Grade	Theoretical layer-thickness [m]	Percentage of losses %	Practical layer-Thickness [m]	Practical fill density Tons/geomeric design-volume
Core (Quarry-Run)		≥ 1m	5%		2,14
Filter-Layer	5 – 40 kg	0,40	10%	0,44	2,15
Filter-Layer	10 – 60 kg	0,50	10%	0,55	2,15
Under-Layer	60 – 300 kg	0,80	10%	0,88	2,18
Under-Layer	0.3 - 1.0 ton	1,25	10%	1,38	2,18
Armour-Layer	1 - 3 ton	1,80	15%	2,07	2,20
Armour-Layer	3 - 6 ton	2,40	15%	2,76	2,20
Armour-Layer	6 - 10 ton	2,90	15%	3,34	2,20

Rock: some indicative parameter-values

Parameter	Unit	Sandstone	Limestone	Granite	Gabbro	Porphyre
Density	Kg/m3	2200-2600	2700 -2900	2600-2800	2800-3000	2550 -2800
Waterabsorption	%	4,0 – 8,0	0,5 - 3	< 0,5	< 0,2	< 0,5
Compression strength UCS	MPa	20- 80	60 -200	80 - 300	100-400	200-500
Tensile strength	MPa	2-4	2 - 5	2-4	1 - 2	1-2
Sonic velocity	m/sec	4.000	5.000	7.000	8.000	7.500

Tolerances for Rocks used in Breakwaters

Wem = arithmetic average weight
 (the total weight of a sample of one grade, divided by the number of stones)

W50 = mediane weight of one grade
 (50% > / 50%<)

Location	Quarry run, Filter-Layer		Under-Layer & Armour - Layer, (Wem > 300 kg)	
	Wem < 300 kg	Wem > 300 kg	Absolute tolerance	Average tolerance
	[m]	[m]		
Above water	0.20	0.40	0.35 * Dn50	0.30 * Dn50
	-0.20	-0.20	-0.30 * Dn50	-0.25 * Dn50
From 0 tot - 5m	0.50	0.80	0.60 * Dn50	0.50 * Dn50
	-0.30	-0.30	-0.50 * Dn50	-0.40 * Dn50
From - 5 tot -15 m	0.50	1.20	0.60 * Dn50	
		-0.40		
More than -15 m	-0.50	1.50	-0.50 * Dn50	
		-0.50		

Exchange factors between W50 and Wem

Rock-grade	W50	Factor	Wem
	[kg]		[kg]
10 – 60 kg	35	1,30	27
60 – 300 kg	180	1,15	157
0.3 - 1.0 ton	650	1,10	591
1 - 3 ton	2.000	1,05	1.905
> 3 ton		1,00	

Exchange factors from d50 to dn50

Rock-grade	D50	Factor	Dn50
	[m]		[m]
10 – 60 kg	0,28	0,84	0,24
60 – 300 kg	0,48	0,84	0,41
0.3 - 1.0 ton	0,74	0,84	0,63
1 - 3 ton	1,08	0,84	0,91
3 - 6 ton	1,41	0,84	1,19
6 – 10 ton	1,71	0,84	1,45

dn50 = nominal rock-diameter for perfect spheric rock
 $(= \{ W 50 / \rho_s \}^{0,333})$
d50 = average real irregular stone diameter
 $(= \{ W 50 / (\rho_s / 0,60) \}^{0,333})$
d 50 = dn50 / 0,84

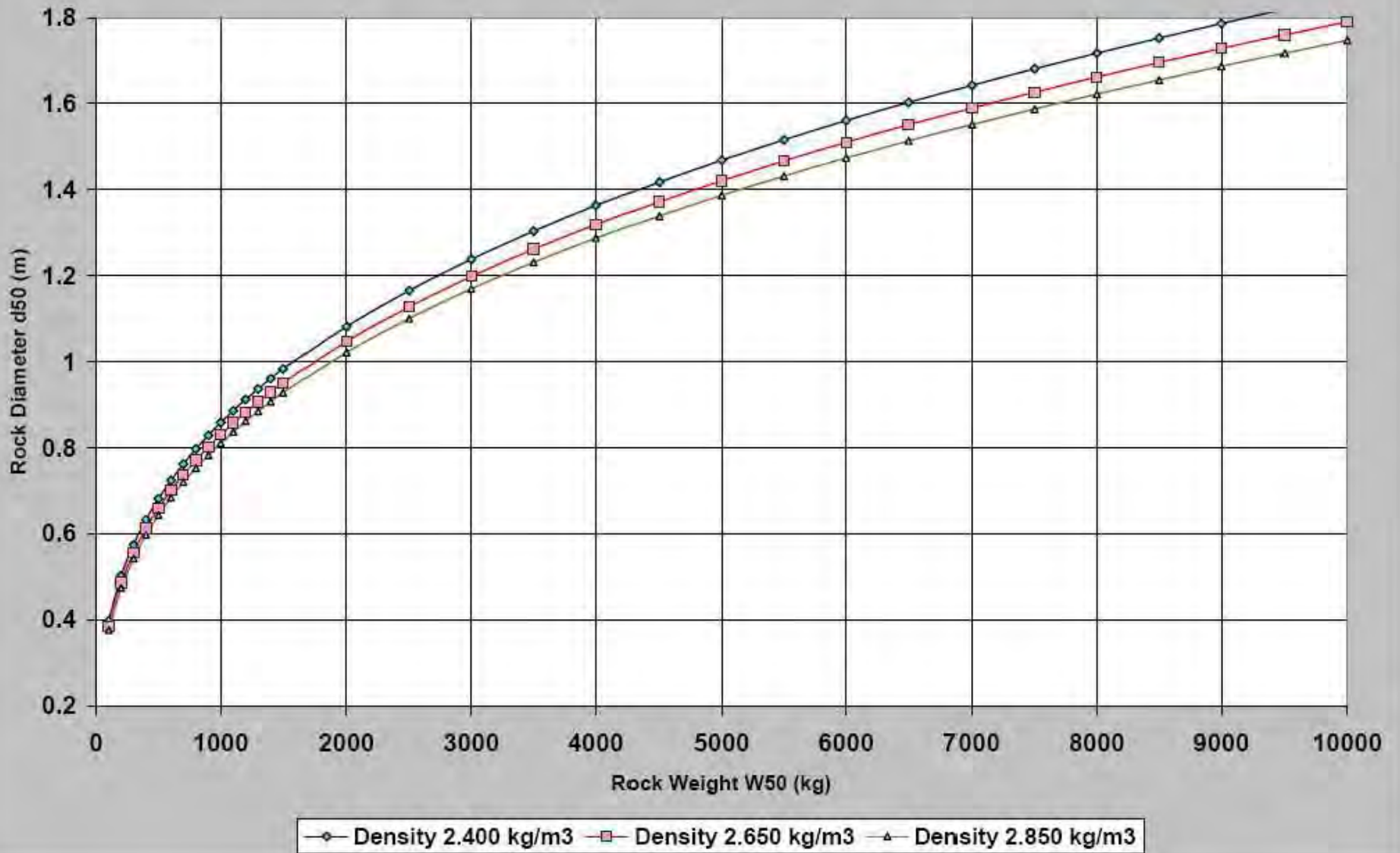
Examples of typical dimensions and weights of Rocks in Breakwaters

Layer	Grade	W 50	ρ_s	Rock volume	D 50
		[ton]	[ton/m ³]	[m ³]	[m]
Filter-Layer	5 – 40 kg	0,023	2,650	0,008	0,242
Filter- Layer	10 – 60 kg	0,035	2,650	0,013	0,280
Under-Layer	60 – 300 kg	0,180	2,650	0,068	0,484
Under-Layer	0.3 - 1.0 ton	0,650	2,650	0,245	0,742
Armour - Layer	1 - 3 ton	2,000	2,650	0,755	1,079
Armour- Layer	3 - 6 ton	4,500	2,650	1,698	1,415
Armour - Layer	6 – 10 ton	8,000	2,650	3,019	1,714

$$D_{50} = \left(\frac{W_{50}}{\rho_s} \cdot \frac{1}{0.6} \right)^{1/3}$$

Form-factor = 0,60

Rock Armour units: relationship between Rock Diameter and Rock Weight



Narrow grading		Wide grading		Very wide grading	
$D_{95}/D_{15} < 1.5$		$1.5 < D_{95}/D_{15} < 2.5$		$D_{95}/D_{15} > 2.5$	
Class	D_{95}/D_{15}	Class	D_{95}/D_{15}	Class	D_{95}/D_{15}
15-20 t	1.1	1-10 t	2.0	10-1000 kg	4.5
10-15 t *	1.1	1-6 t	1.8	10-500 kg	3.5
6-10 t *	1.2	100-1000 kg	2.0	10-300 kg	3.0
3-6 t *	1.3	10-60 kg *	1.8		
1-3 t *	1.4				
0.3-1 t *	1.5				

Table 5.17 Examples of heavy and light gradings

Note:

The gradings indicated with * are standard gradings in accordance with EN 13383 (see Section 3.4.3).

Rock supply works for breakwaters



Breakwater construction using earth-moving equipment and geotextiles



Singapore: Reclamation of Pulau Ubin and Pulau Tekong Islands



Key Figures:

Client : Housing and Development Board

Surface of land to create : 1.480 ha

Volume of Sand to reclaim: 164 Mm³

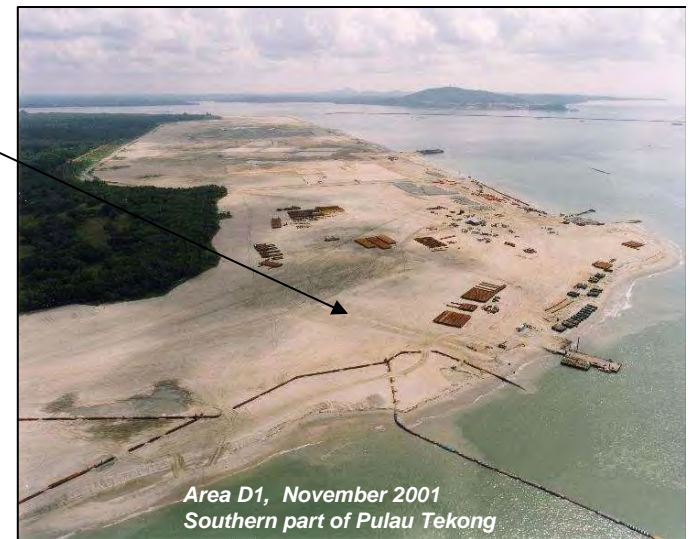
Length of Breakwater : 14.800 m'

Period: 2000 – 2005

Investment : 850 M €



Area A- at Pulau Tekong Kechil, June 2002

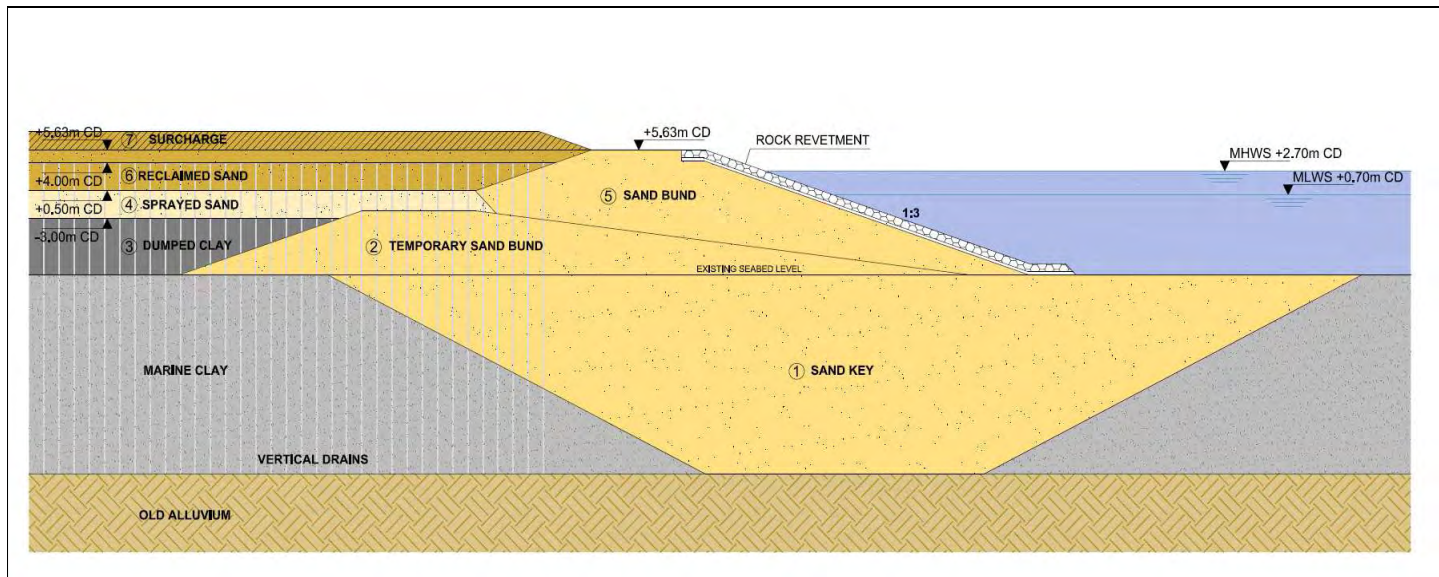


Area D1, November 2001
Southern part of Pulau Tekong

Singapore: Reclamation of Pulau Ubin and Pulau Tekong Islands

Design Elements:

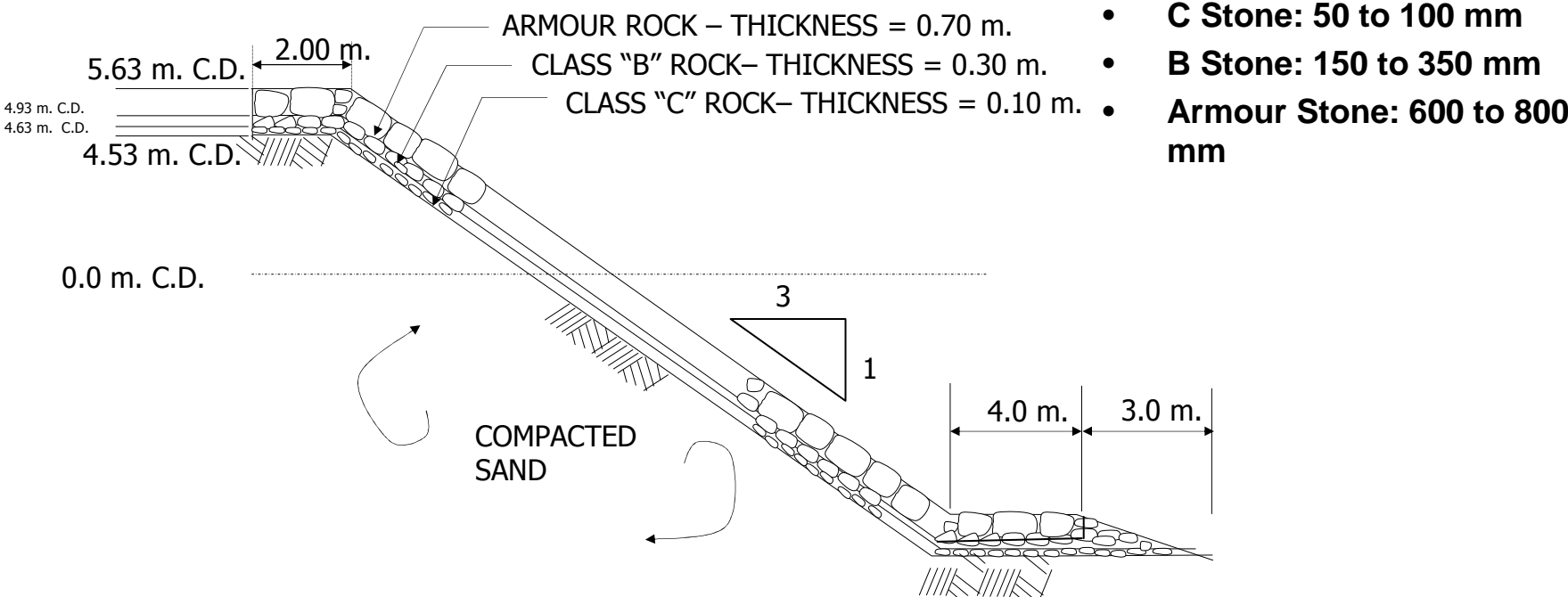
- Storm Surge level: CD + 3m
- Natural waterdepths: CD- 2 to -20m
- Design Wave Height: $H_s = 0,6$ m
- Design Wave Period : $T_m = 2,9$ sec
- $V_{curr} = 1,5$ m/sec



Dredging of soil-substitution trench: sandkey



Singapore, Pulau Ubin and Pulau Tekong Reclamation and Rock-Works



- **C Stone: 50 to 100 mm**
- **B Stone: 150 to 350 mm**
- **Armour Stone: 600 to 800 mm**

Karimun,(Ind) Quarry of Granitic Rock



Sieving, grading, crushing of rock : dressing of the various grades

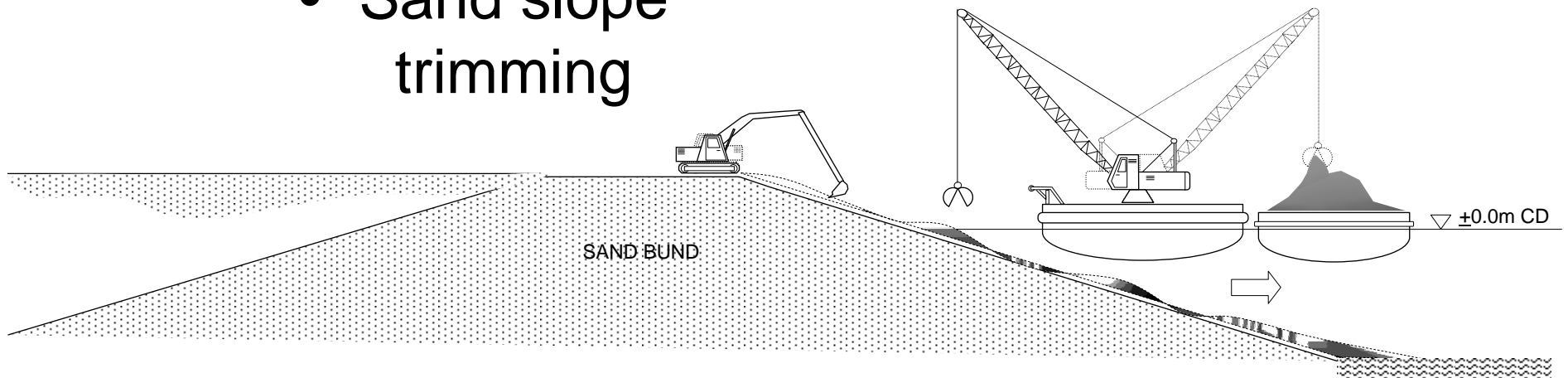


Drop-test of Armour RAU on Underlayer, laying on geotextile



Pulau Ubin : Pulau Tekong: Method Statement

- Sand slope trimming



- Crane barge is used to carry out the sand slope preparation (cut and fill) below water level, while land-based excavator carries out the sand slope preparation above water level.
- Excess sand below $\pm 0.0m$ CD is loaded to a coaming barge or hopper barge and is used for the next area.
- Excess sand above $\pm 0.0m$ CD is loaded to a tipper lorry and is used for the next area.

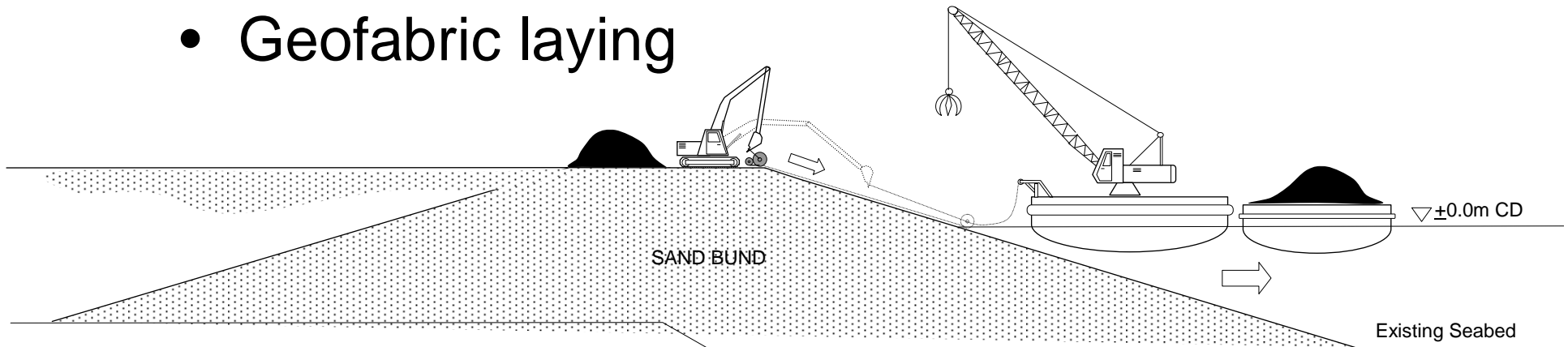
Trimming of Sand-slopes





Pulau Ubin/ Pulau Tekong: Method Statement

- Geofabric laying



- **Class B & C material is stockpiled near the working area for both land and marine prior to placement of the fabric.**
- **Survey pegs at the crest line and at the slope down to the lowest water level are used as guides for the alignment of fabric during placement.**
- **Geo-fabric on roll is positioned at the crest (+4.53mCD) and unrolled down the slope to the water level with the aid of an excavator to control and maintain the proper alignment.**





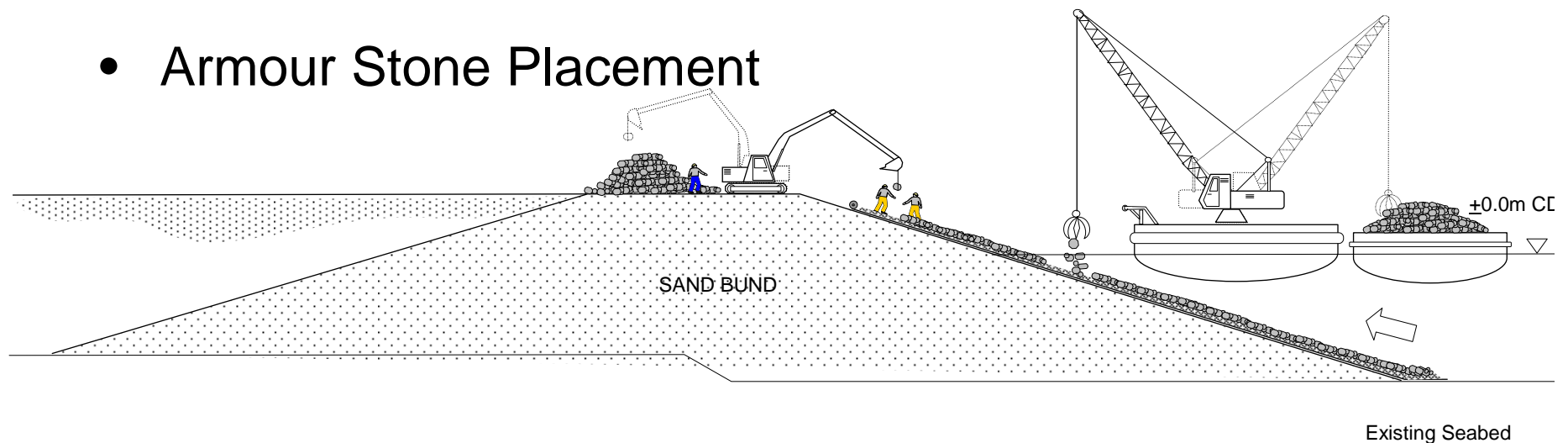






Pulau Ubin/Pulau Tekong: Method Statement

- **Armour Stone Placement**



- **Upon successful inspection of the class 'B' profile, the placement of armour stones follows.**
- **For the lower part of the slope or below water level, armour stones are placed to the designed levels by a floating crane barge or by the hydraulic excavator on the pontoon starting from the bottom.**
- **Above $\pm 0.00\text{m CD}$, each armour stone is placed / pitched tightly and accurately to the lines, levels and slopes as shown on the**











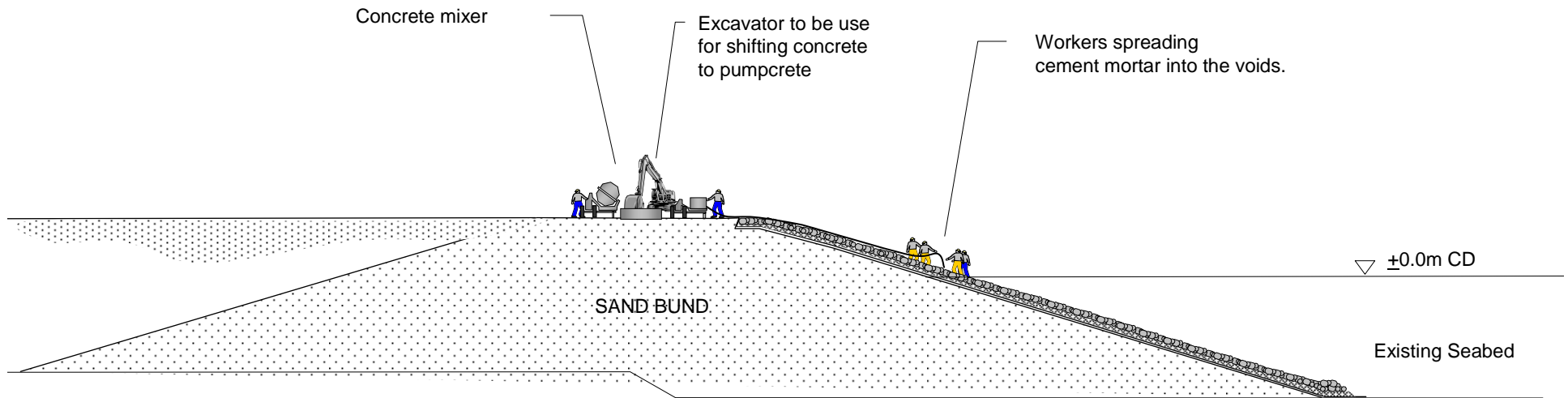






Pulau Ubin/Pulau Tekong: Method Statement

- Cement mortar placement

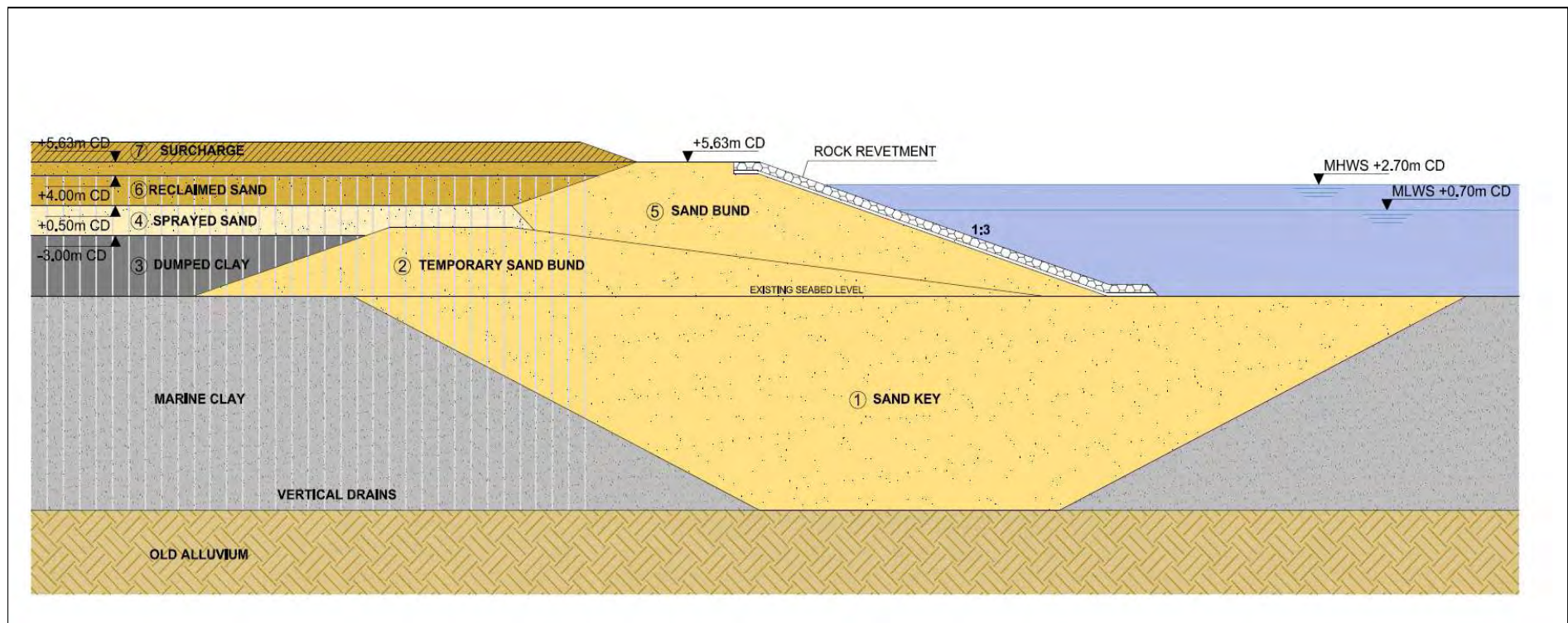


- **Upon the success of armour stone profile inspection, and once the expected sand bund settlement was obtained, gaps between armouring stones from elevation +1.5mCD shall be filled up by cement mortar.**
- **Cement mortar shall be mixed on site and suitable concrete pump shall be used for placement.**





Singapore: Reclamation of Pulau Ubin and Pulau Tekong Islands



Singapore, Pulau Ubin and Pulau Tekong Reclamation and Rock-Works (2000-2005)

Volume

- Dredging of sandkey trenches and filling with sand (dredging depth -20 mCD to -60 mCD): 20,400,000 m³
- Construction of sand bunds including vibroflotation: 23,700,000 m³
- Infilling of reclamation area with dredged clay: 15,000,000 m³
- Filling on top of the marine clay with sand: 150,000,000 m³
- Installation of geofabric: 1,000,000 m²
- Construction of sloping rock revetment: 1,000,000 m³
- Installation of Prefabricated Vertical Drains: 80,000,000 m
- Installation of a sheet pile wall serving as a silt curtain: 8.5km
- Installation and management of a staging ground receiving excavated good earth and soft clay from trucks for barging to Pulau Tekong: 6,300,000 m³ GE / 10,500,000 m³ SC
- Construction of a white sandy beach: 700,000 m³
- Dredging of access channels, including rock blasting: 3,000,000 m³
- Marine installation of gravel compaction piles: 74,000 m³
- Installation of silt curtains with floaters: 6 km



Palm Jebel Ali, Dubai Construction Phases

Dykes,
Breakwaters
and
Coastal
Defence



**Palm Jebel Ali Construction
Phases**

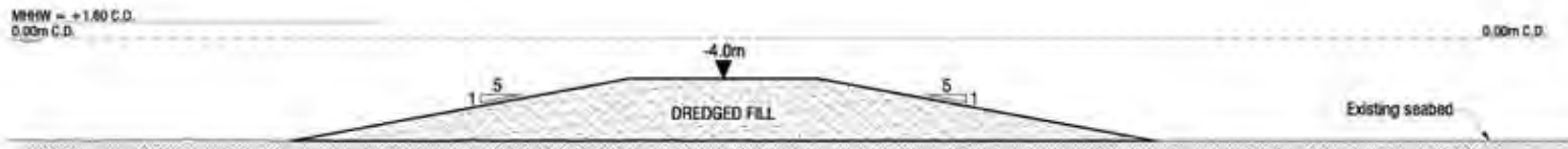
& Dredging 2010



**Landfill works with
THSD's 'Juan Sebastian
de Elcano'**



CRESCENT ISLAND : TYPICAL SECTION
PHASE 1



0 1 2 3 4 5

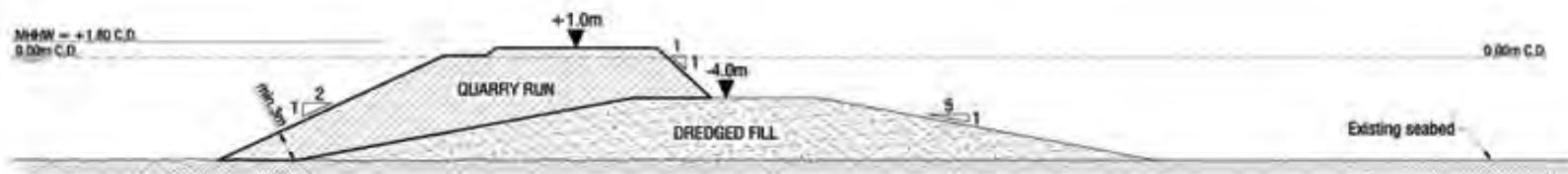
PALM ISLAND 2
CRESCENT ISLAND

TYPICAL SECTION

SCALE : 1 / 400
PLAN : 1 of 10



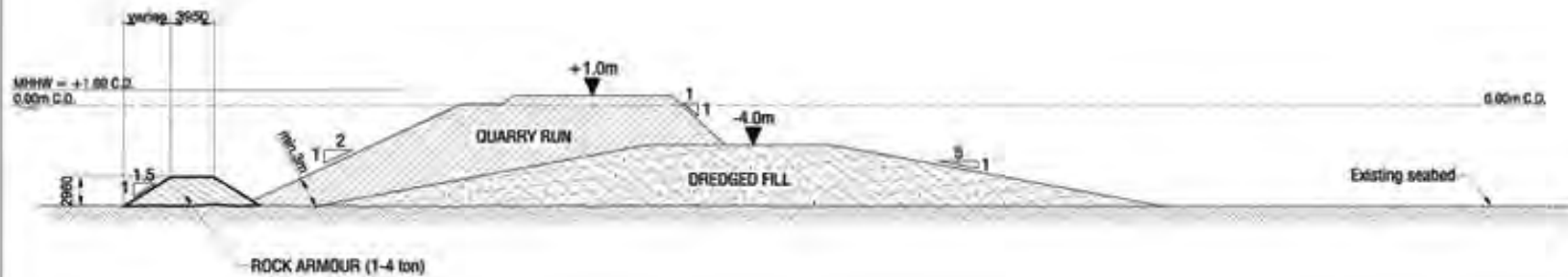
CRESCENT ISLAND : TYPICAL SECTION PHASE 2



PALM ISLAND 2 CRESCENT ISLAND	
TYPICAL SECTION	
	SCALE = 1/400
	PLAN = 3 of 10

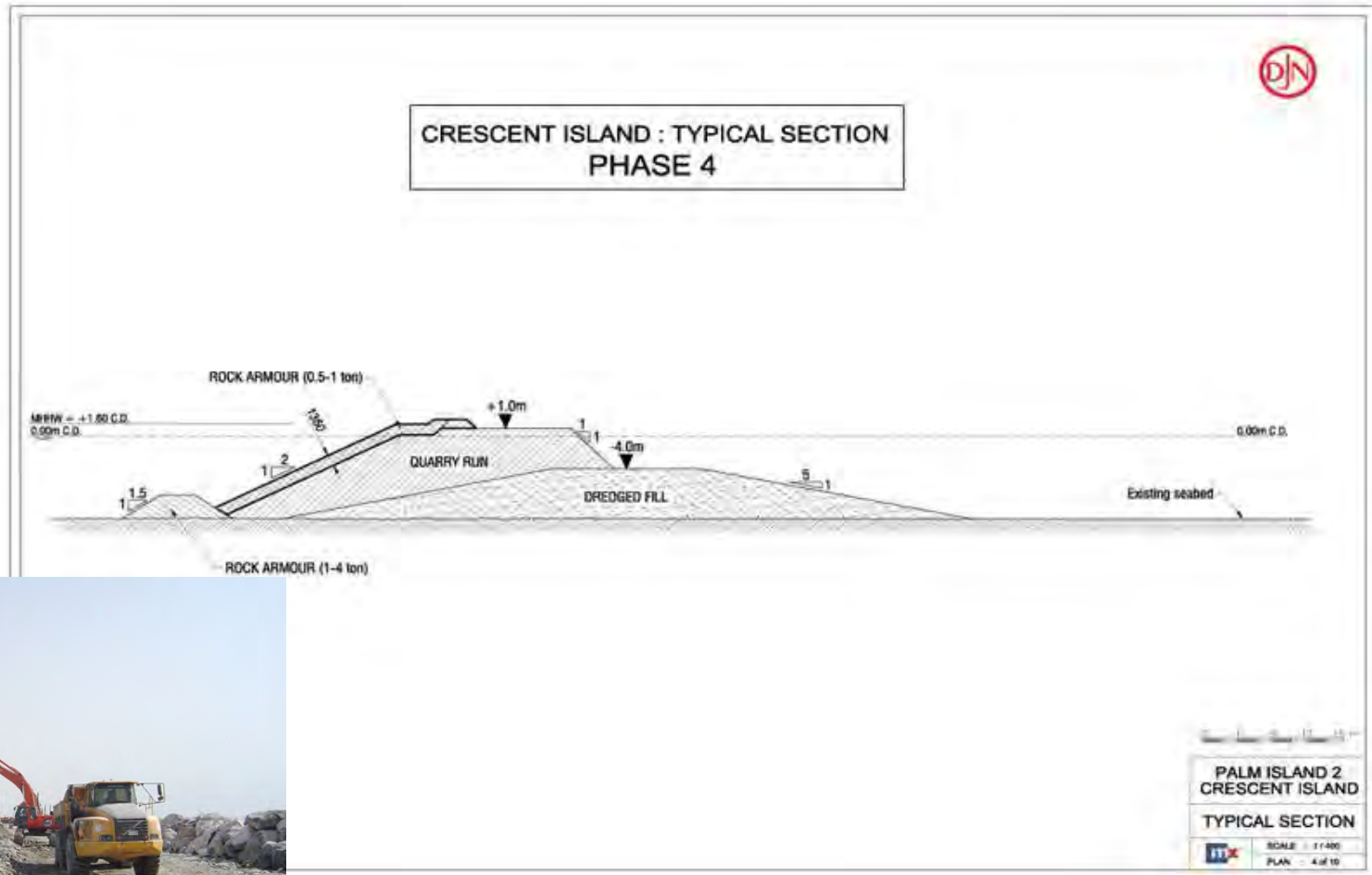


CRESCENT ISLAND : TYPICAL SECTION PHASE 3



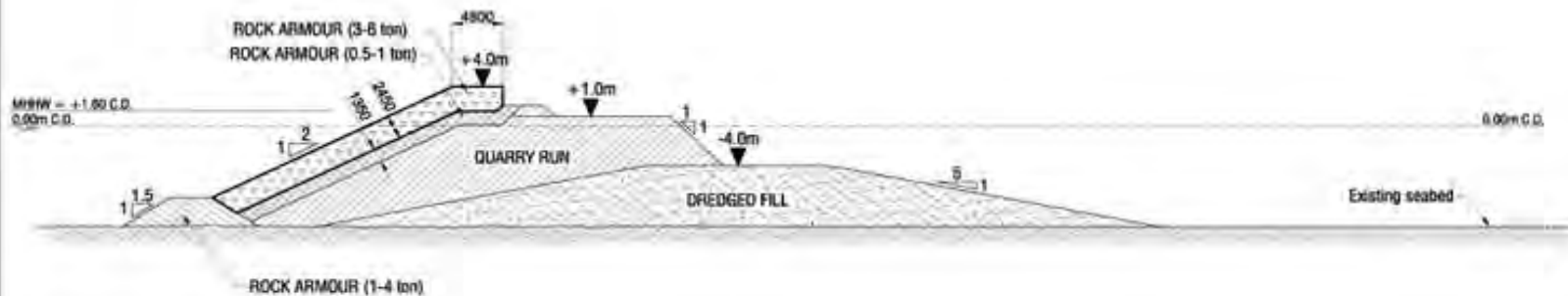
PALM ISLAND 2
CRESCENT ISLAND
TYPICAL SECTION
SCALE : 1:400
PLAN : 3 of 10

Dykes, Breakwaters and Coastal Defence





CRESCENT ISLAND : TYPICAL SECTION PHASE 5



Scale bar: 0 5 10 15

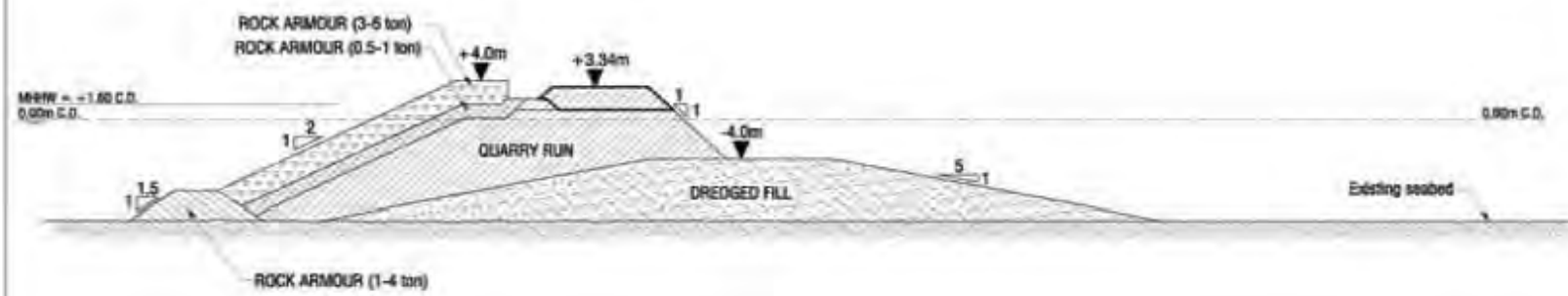
**PALM ISLAND 2
CRESCENT ISLAND**

TYPICAL SECTION

DTX SCALE : 1 : 400
PLAN : 5 of 10



CRESCENT ISLAND : TYPICAL SECTION
PHASE 6



Signature: _____
Date: _____

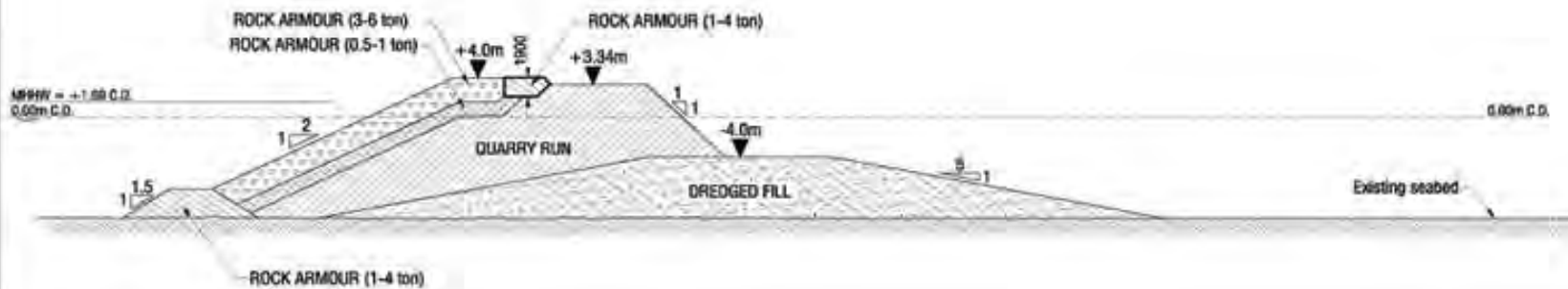
**PALM ISLAND 2
CRESCENT ISLAND**

TYPICAL SECTION

SCALE : 1:100
PLAN : 6 of 10



**CRESCENT ISLAND : TYPICAL SECTION
PHASE 7**



0 1 2 3 4 5

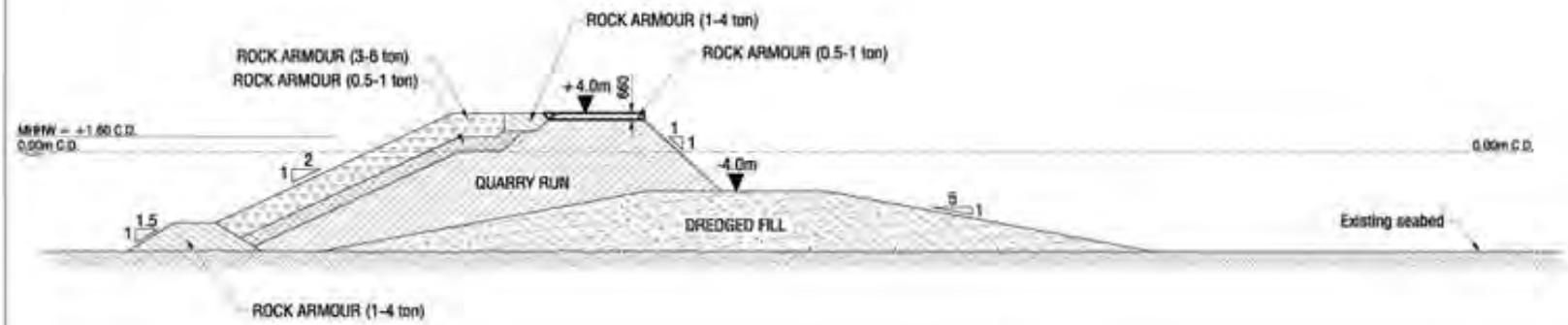
**PALM ISLAND 2
CRESCENT ISLAND**

TYPICAL SECTION

SCALE : 1/400
PLAN : 7 of 10



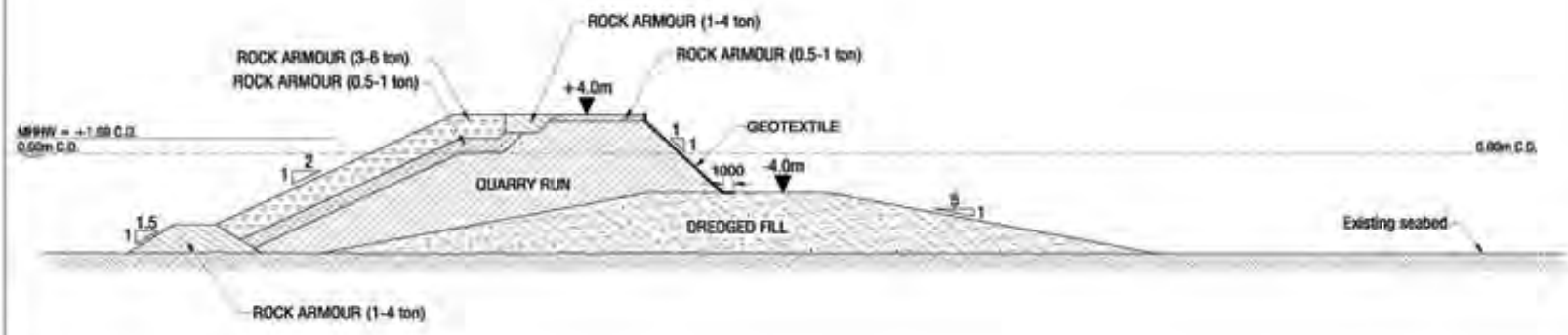
CRESCENT ISLAND : TYPICAL SECTION PHASE 8



PALM ISLAND 2
CRESCENT ISLAND
TYPICAL SECTION
SCALE : 1:1000
PLAN : 8 OF 10



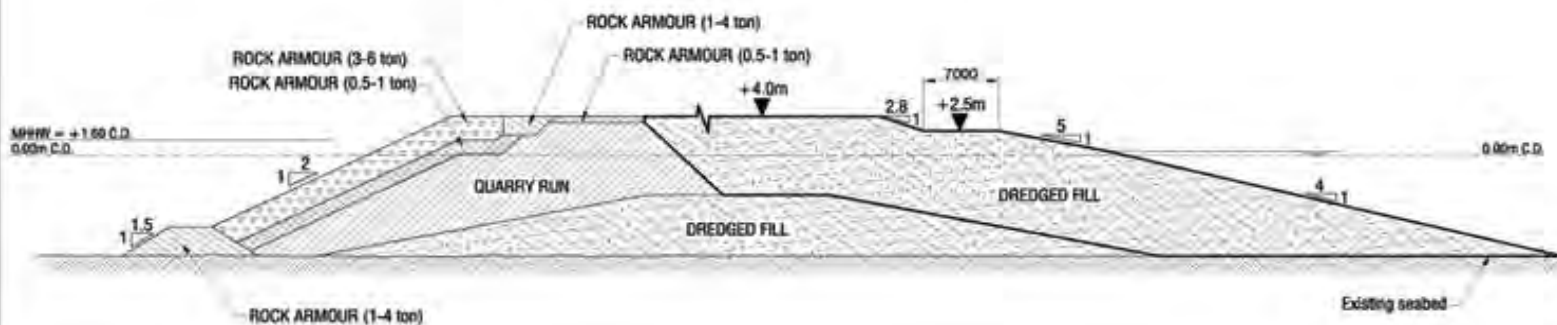
CRESCENT ISLAND : TYPICAL SECTION PHASE 9



PALM ISLAND 2
CRESCENT ISLAND
TYPICAL SECTION
SCALE : 1:400
PLAN : 9 of 10



CRESCENT ISLAND : TYPICAL SECTION PHASE 10



0 5 10 15 20

**PALM ISLAND 2
CRESCENT ISLAND**

TYPICAL SECTION

SCALE = 1:400
PLAN = 10 of 10

New Island Development (NID)

Scope

Reclamation and construction of underwater revetment berm

Soil

Sand and calcarenite

Volume

Dredging: 29 million m³

Reclamation: 29 million m³

Dredgingdepth

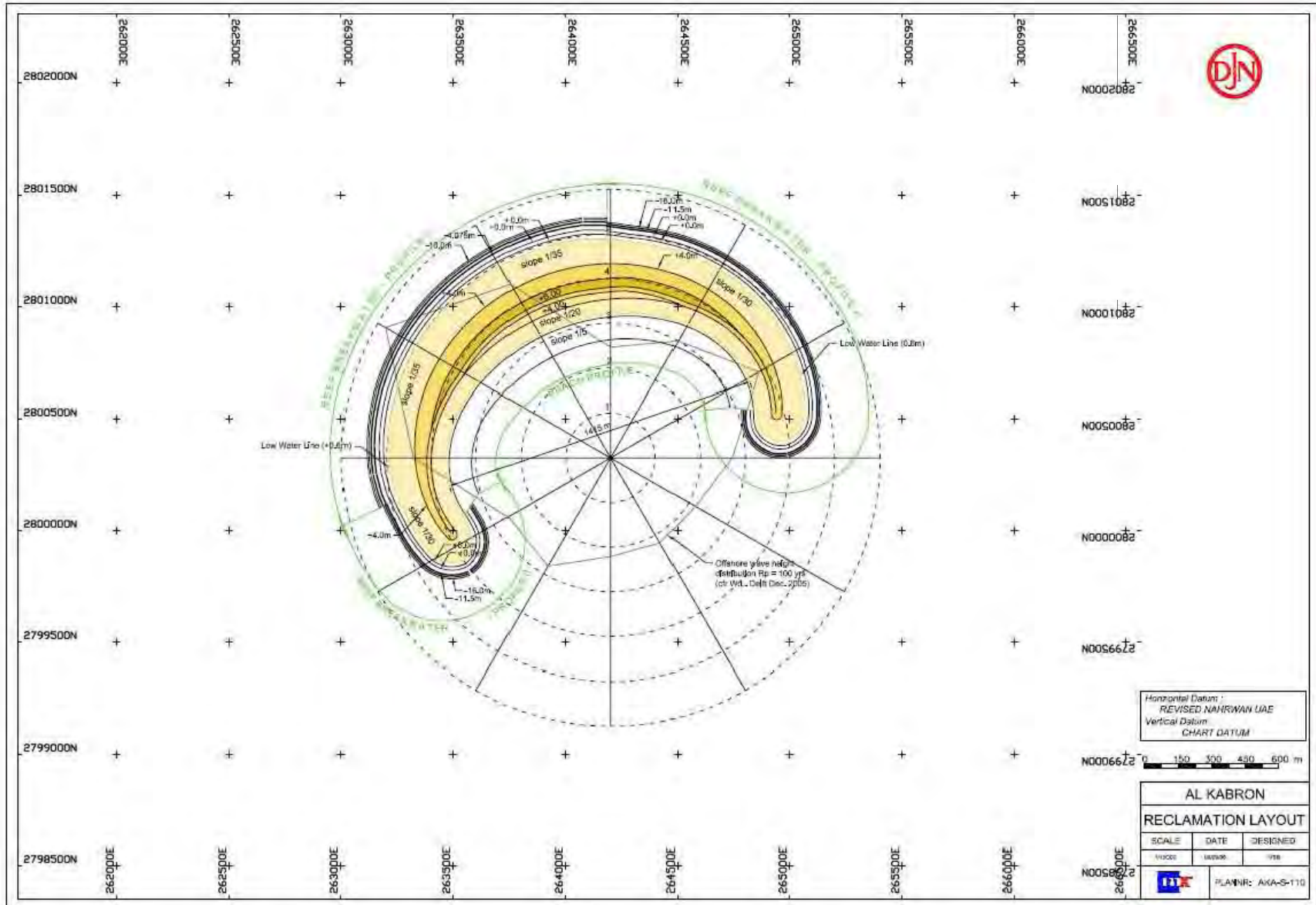
Borrow area depths between 25 and 30 metres

Otherworks

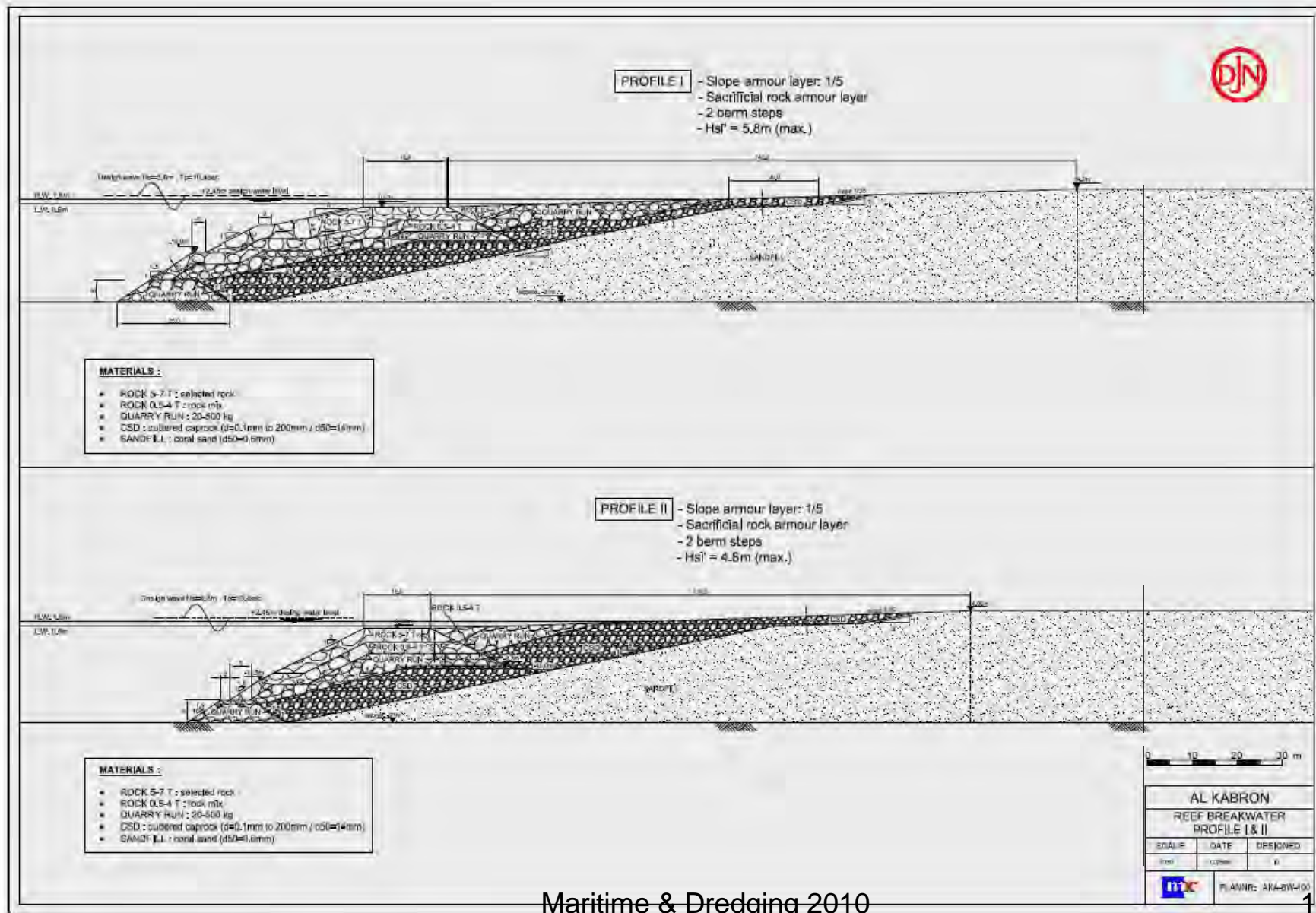
Rock dumping: 3 million m³



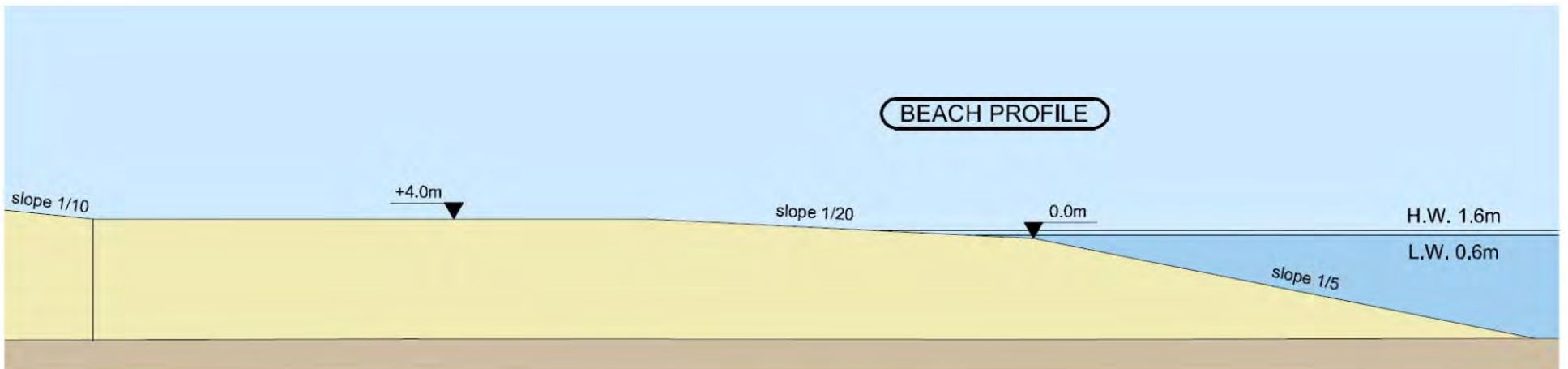
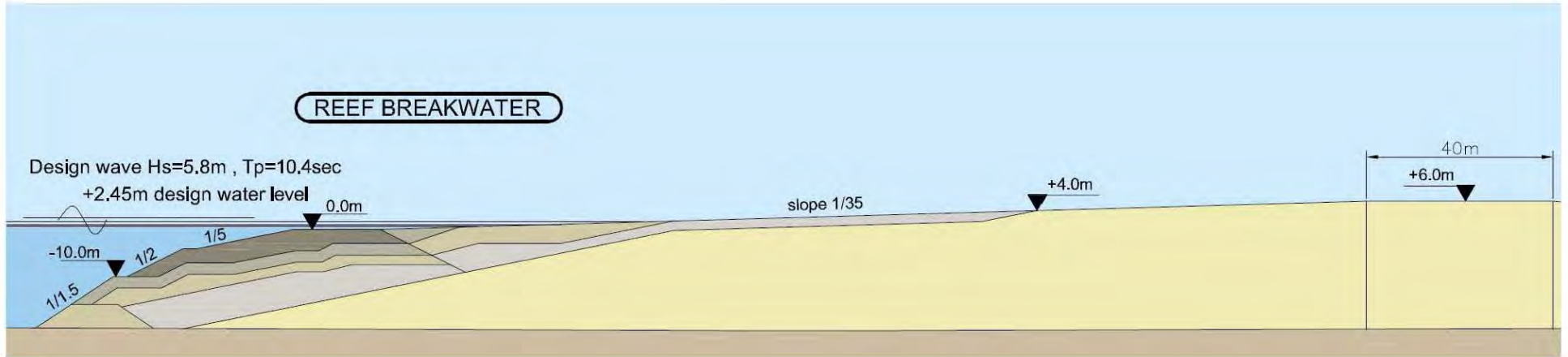
New Island Dedevelopment: Layout



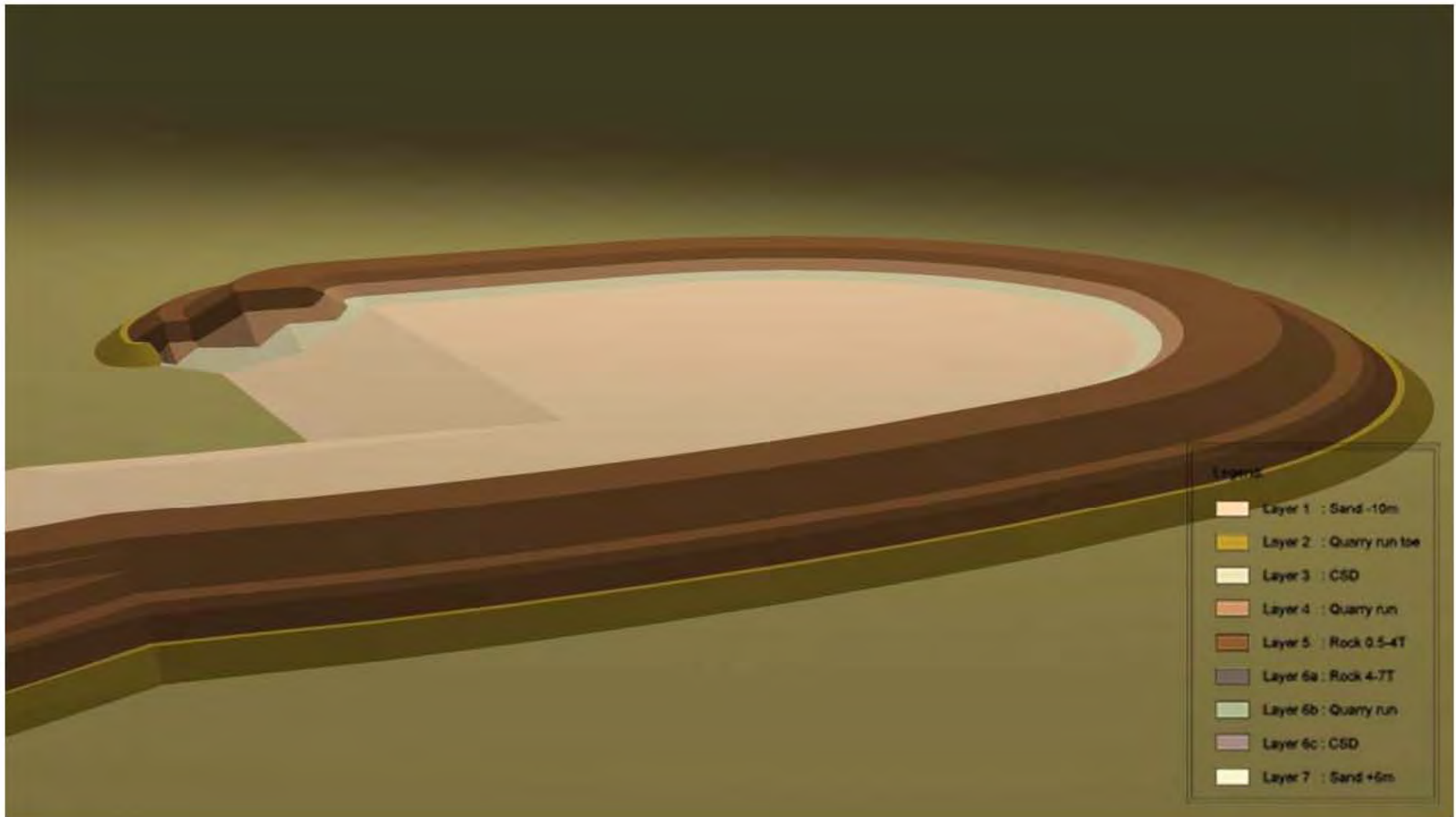
Engineering of Submerged “Reef” Breakwater



Submerged Shield Breakwater (New Island, Dubai)



NID: Visualisation of Roundhead Structures

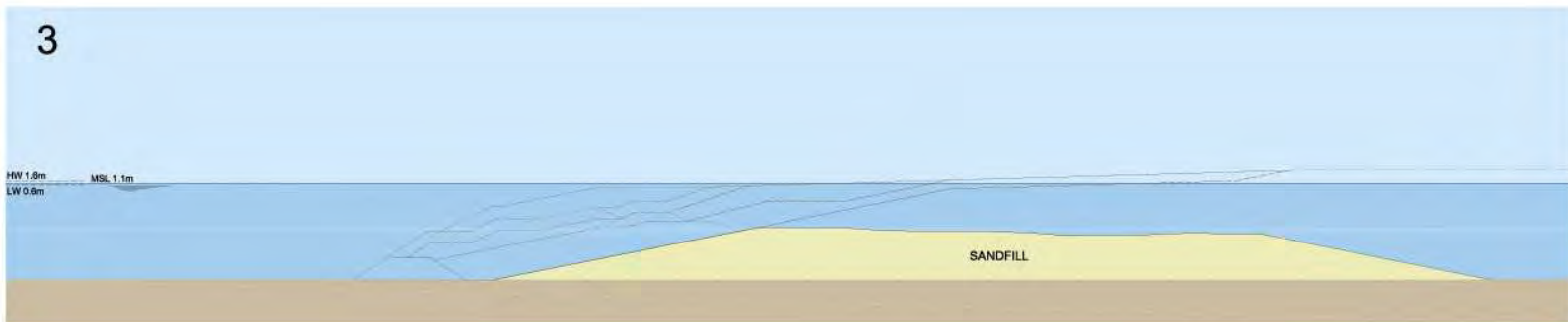
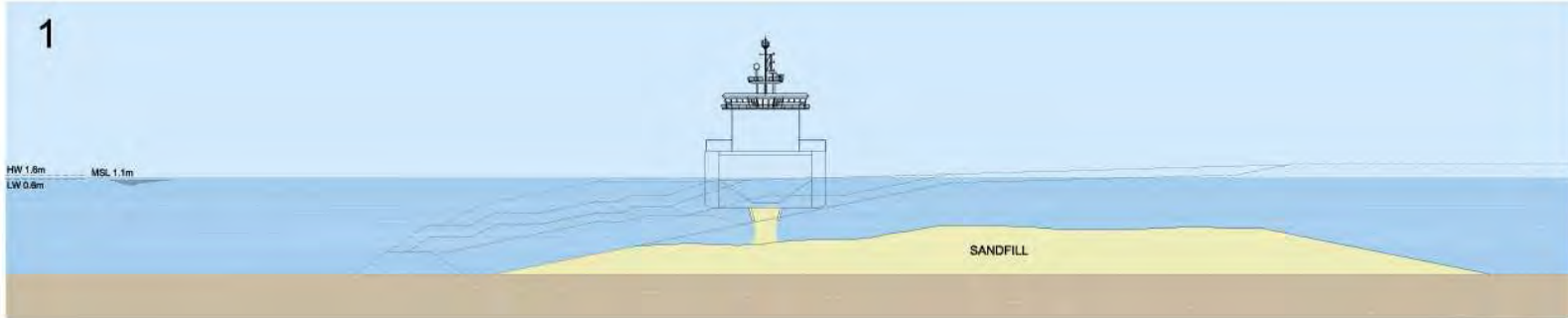


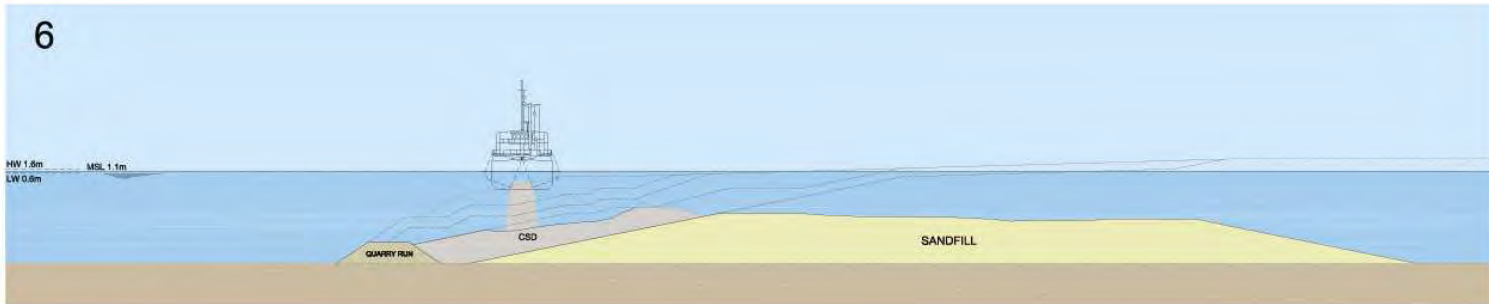
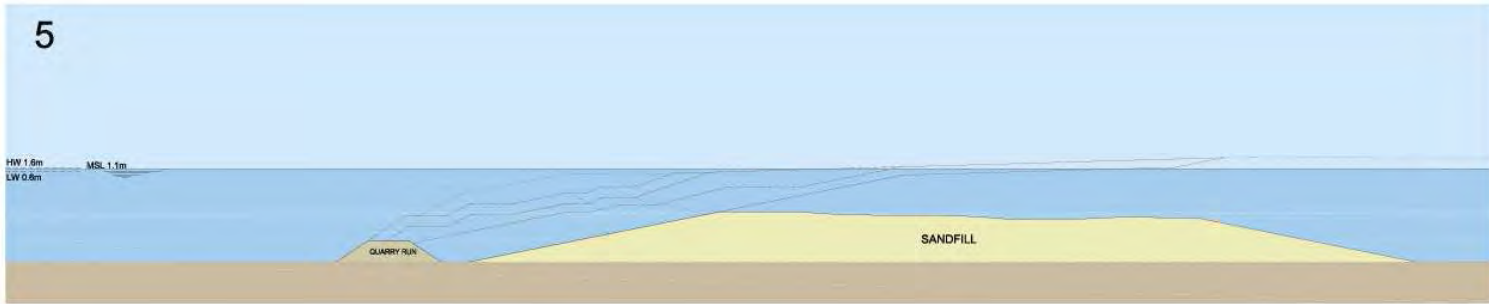
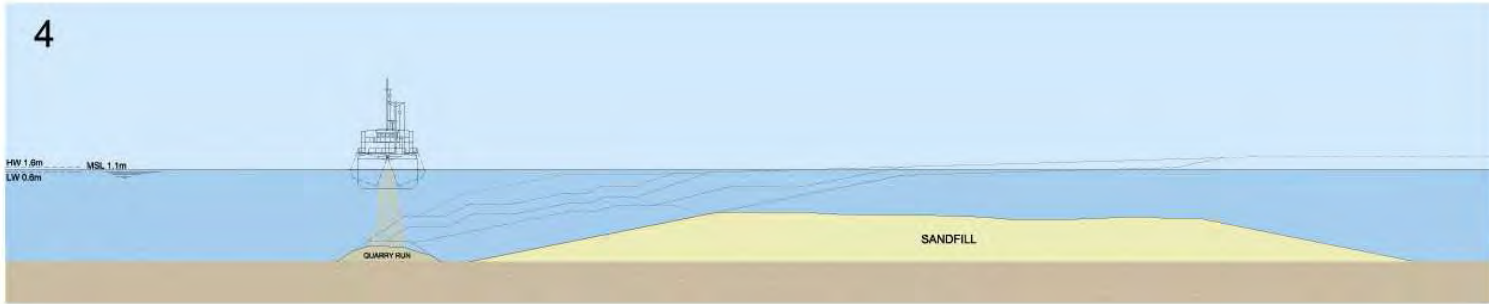
New Island Development (NID)

Equipment

- TSHD Juan Sebastian De Elcano and Gerardus Mercator
- CSD J.F.J. De Nul
- 2 split barges
- SSDV Pompei
- Positioning pontoon DN 121
- Rock transport barges DN 114, DN 115 and DN 116
- Split barge Verrazzano



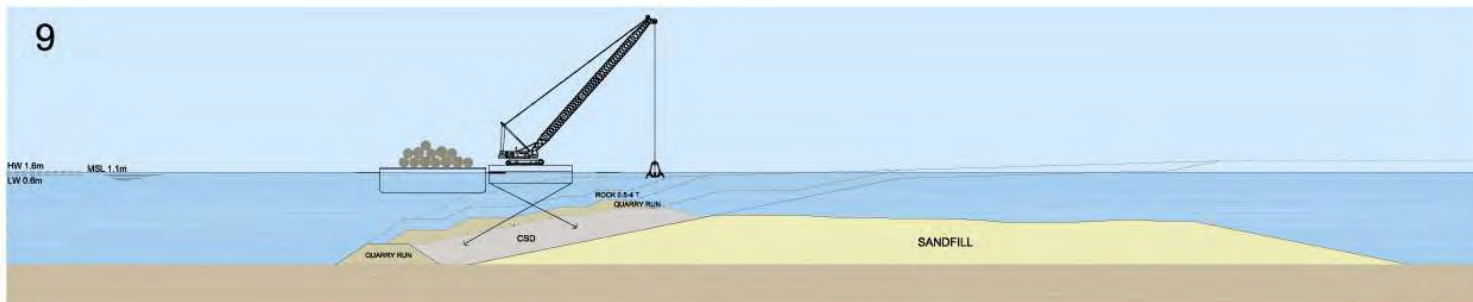
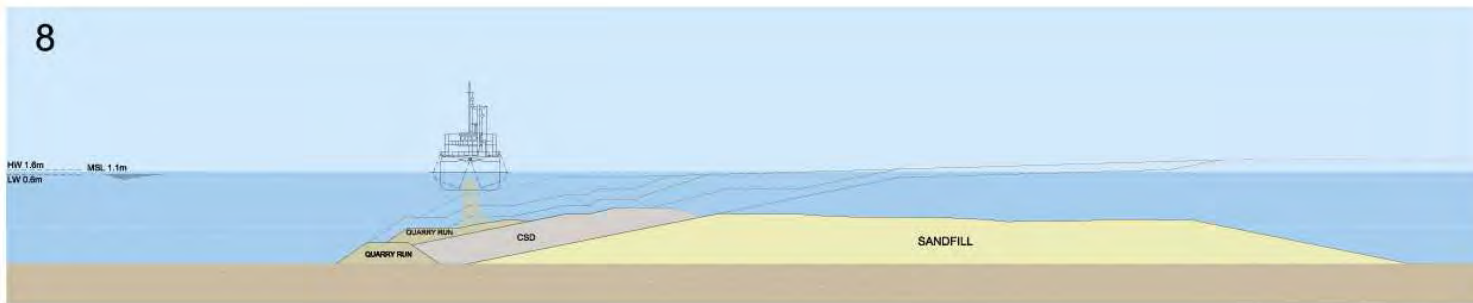
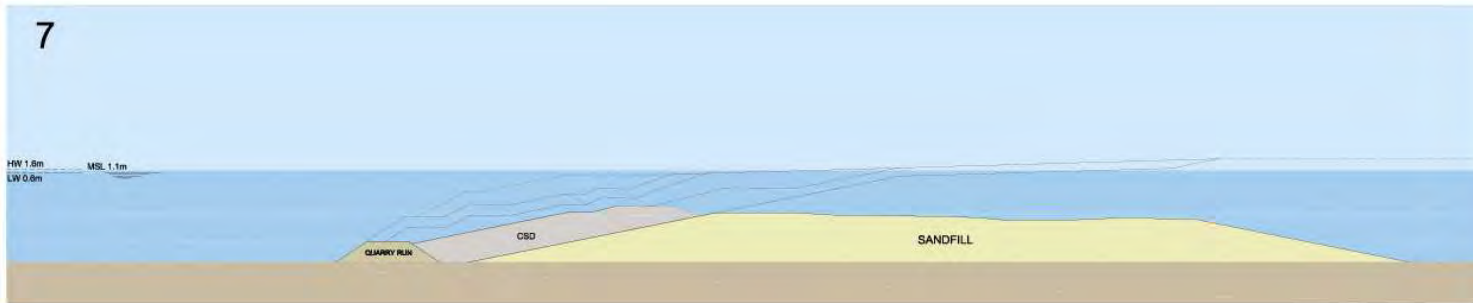




















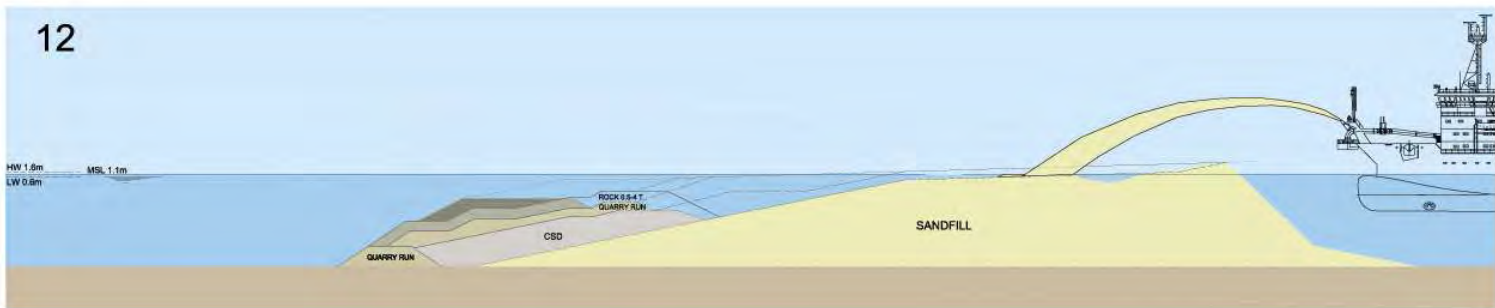
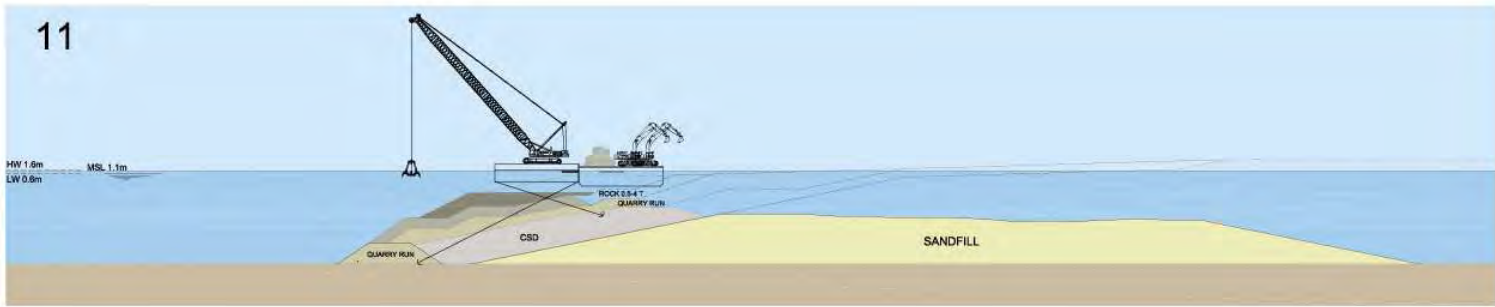
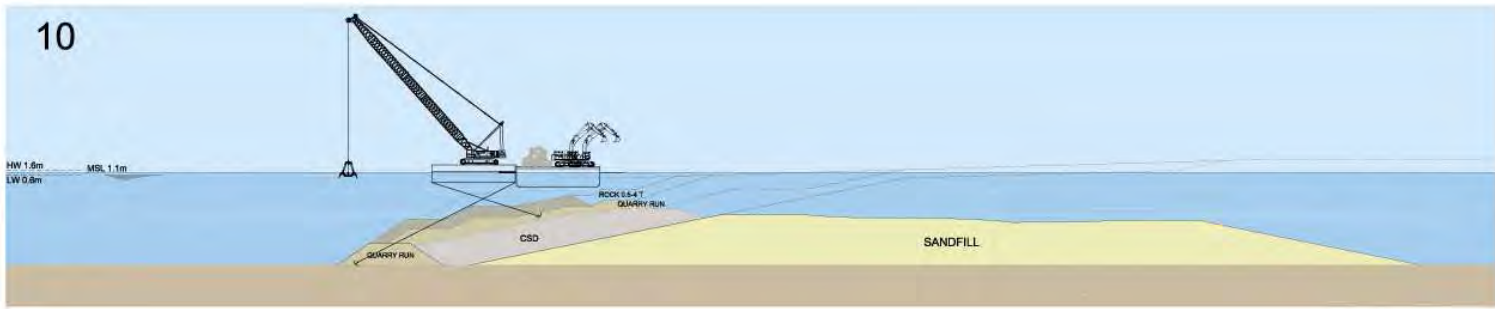






NID in September 2008 (under construction)





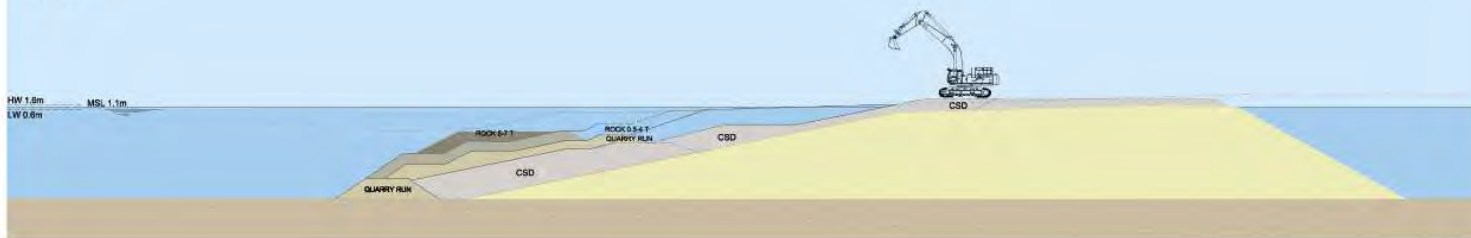




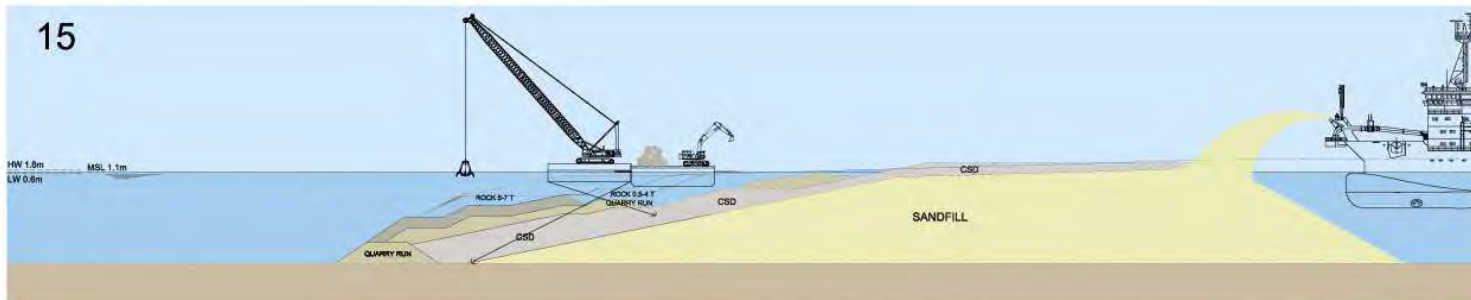
13

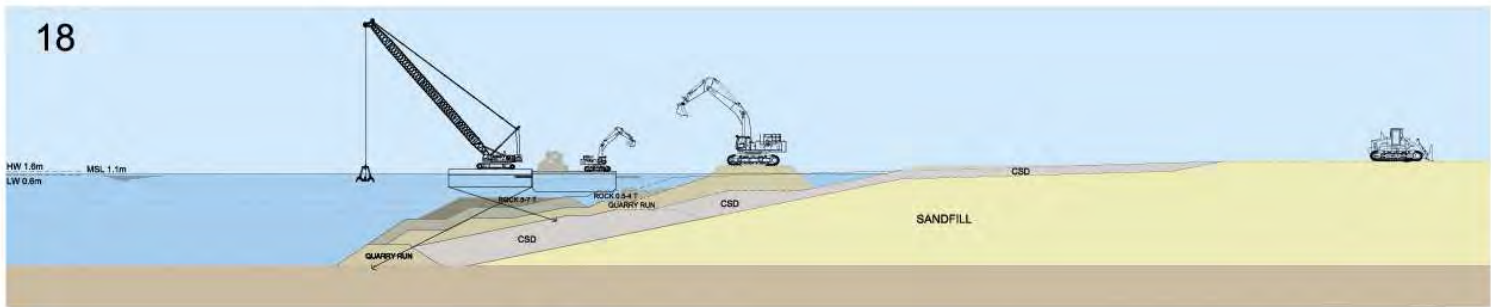
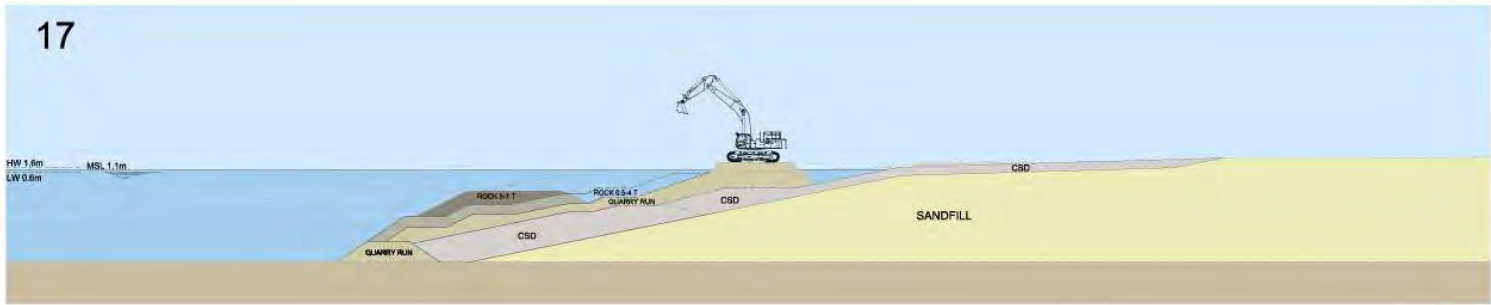
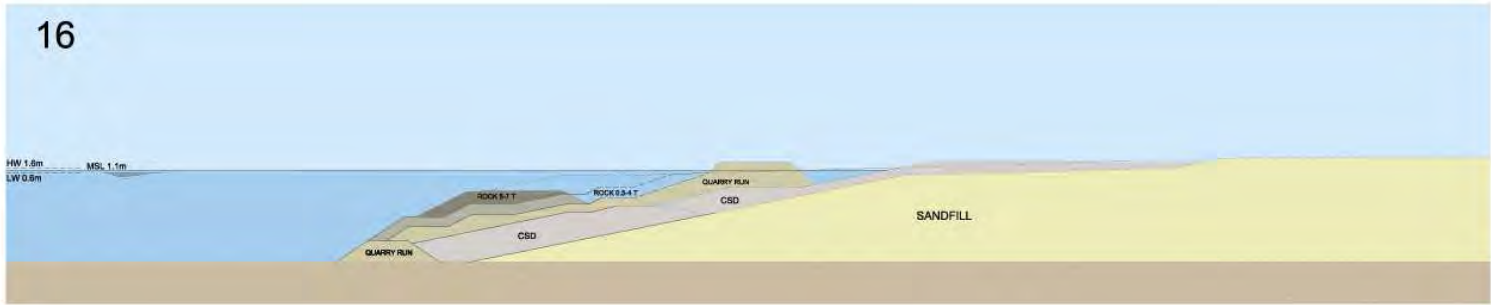


14

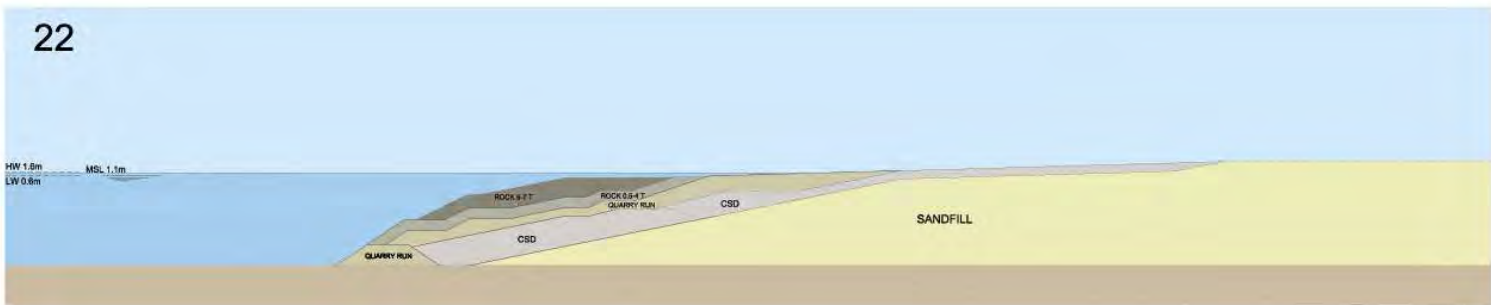
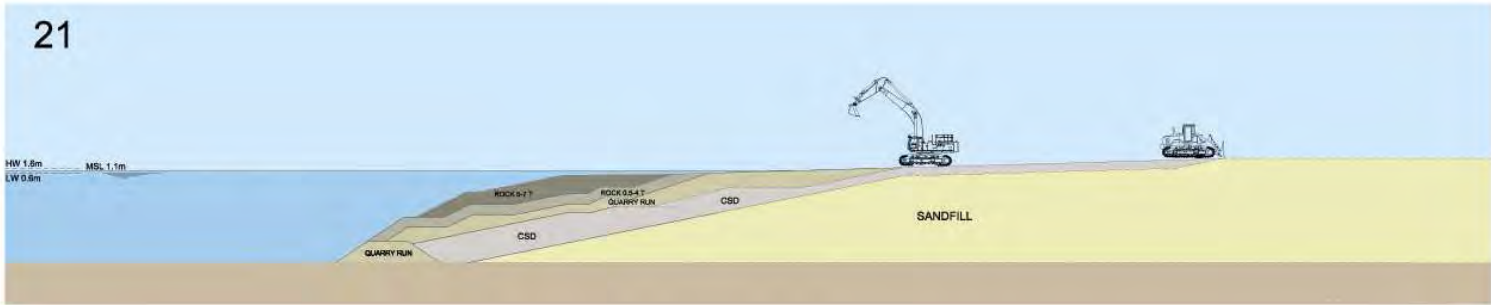


15









New Island Development: June 2009



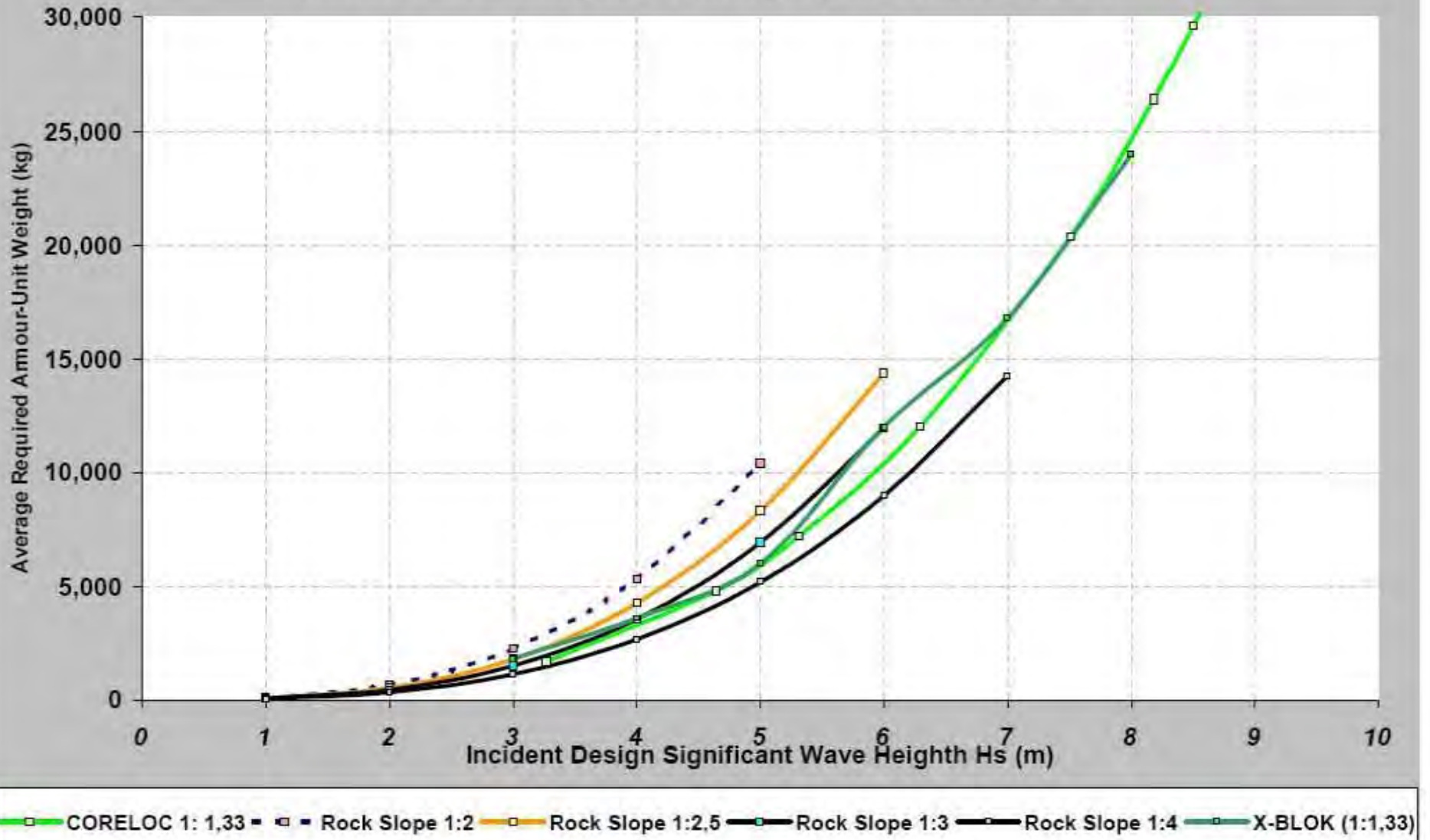
Errors in rubble-Mound Breakwaters NOT to make !



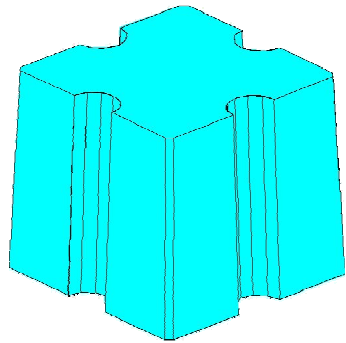




Comparison of Rock Armour Units (dens = 2.650 kg/m³) vs
Concrete Armour Units (dens = 2.400 kg/m³) cfr Hudson's formula

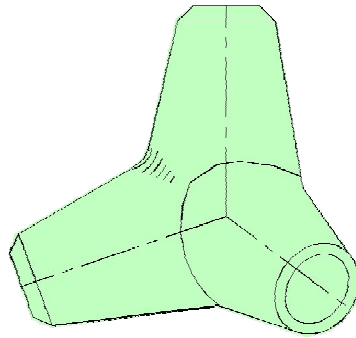


Armouring of Breakwaters with Concrete Armour Units, CAU's

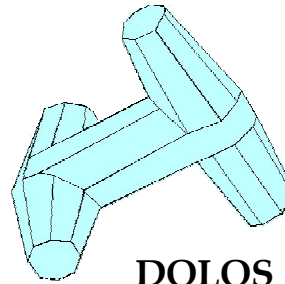
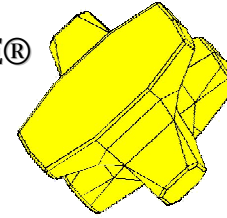


ANTIFER CUBE

TETRAPOD



ACCROPODE®

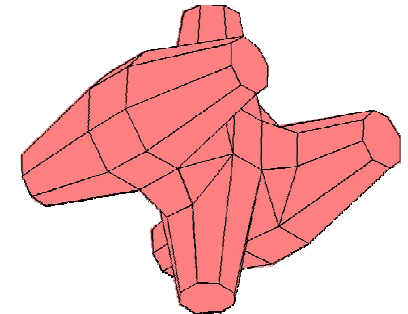


DOLOS

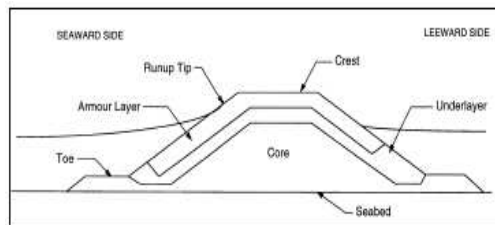


HARO

CORE-LOC™



Xbloc

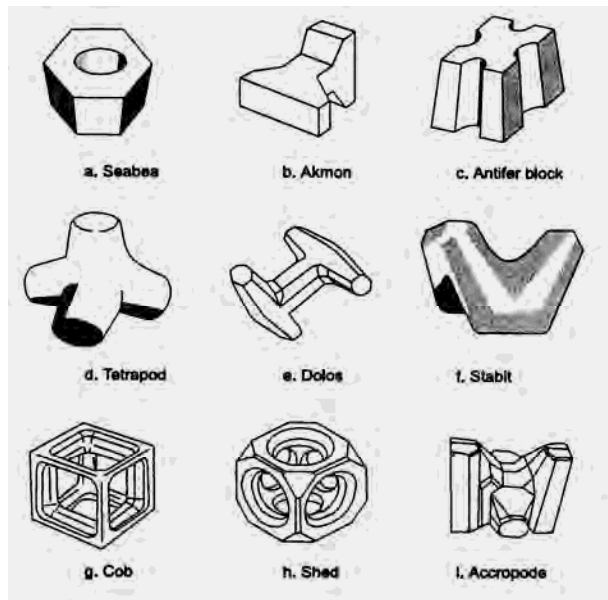


$$W = \frac{w_r H^3}{K_D (S_r - 1)^3 \cot \theta}$$

Type of Armour Block	TETRAPOD	ANTIFER CUBE	HARO	ACCROPODE®	CORE-LOC™
Number of Layers	2	2	2	1	1
Armour Slope H/V	3/2	3/2	3/2	4/3	4/3
Porosity %	50	45	51 - 53	52	60
Breaking Waves Kd	7*	9*	13,8	12	16
% Damage	5	5	0,5	0	0
Concrete Volume per m ² of Slope	0.35 Hs	0.38 Hs	0.27 Hs	0.2 Hs	0.18 Hs
Relative Quantity of Concrete	1.9	2.0	1.3	1.0	0.9

CAU's

Type	Layers	History	Void Percentage	Concrete percentage
Antifer Cube	2	Developed in 1972 Sogreah (Fr)	45%	55%
Tetrapod	2	Developed in 1950 Sogreah	50%	50%
Dolos	2	Developed in 1970 (SA)	60%	40%
Accropode I	1	Developed in 1980 Sogreah	50%	50%
Accropode II	1	Developed in 1994 Sogreah	55%	45 %
Core-Loc	1	Developed in 2000 USACE & commercialised by Sogreah	60%	40%
Xbloc	1	Developed in 2004 DMC (NI)	60%	40%



Placement-rythms of CAU's in Breakwaters

cyclus time for different CAU's:

Type	2,50 m ³ , 6 ton		5,00 m ³ , 12 ton		10,00 m ³ , 24 ton	
	[sec]	[min]	[sec]	[min]	[sec]	[min]
Kubus	150	2,50	200	3,33	250	4,17
Tetrapod	200	3,33	250	4,17	300	5,00
Accropod	250	4,17	300	5,00	375	6,25

Hourly productions at 3.000 working seconds per hour:

Type	2,50 m ³ , 6 ton	5,00 m ³ , 12 ton	10,00 m ³ , 24 ton
	[pcs/hr]	[pcs/hr]	[pcs/hr]
Kubus	20,00	15,00	12,00
Tetrapod	15,00	12,00	10,00
Accropod	12,00	10,00	8,00

Port of Rades: Armouring with Accropode I

ACCROPODE™ is a trademark of SOGREAH - France



ACCROPODE™ est une marque déposée par SOGREAH - France

RADES



ACCROPODE™

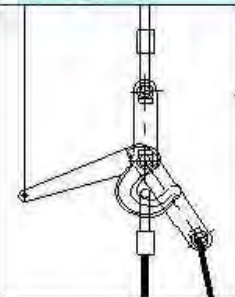
Shed Armouring Units (Limassol Marina)



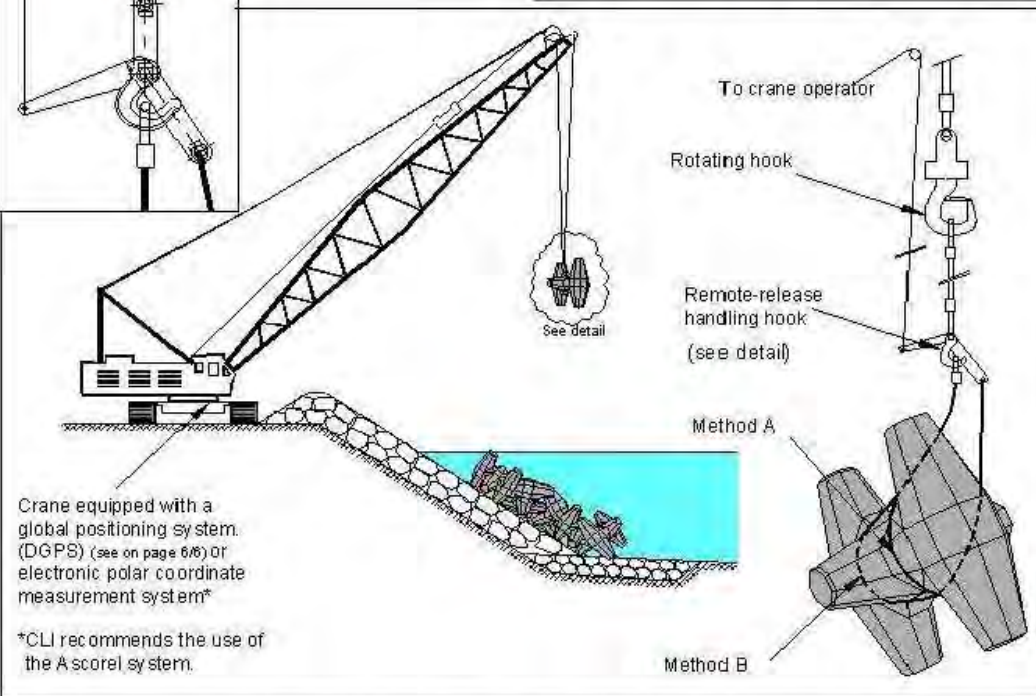
Port of Zeebrugge: Sand retention breakwaters armoured with HARO's



**Remote-release handling
Hook detail**



CORE-LOC™ placing



**Single-layer
CORE-LOC™ armouring**



Filter layer requirements: $W/15$ to $W/7$ (where W is the CORE-LOC™ unit weight)

Filter layer tolerances: $C/6$ (where C is the unit height)

CORE-LOC® est une marque déposée par l'US Army Corps of Engineers USA



CORE-LOC® is a trademark of the US Army Corps of Engineers USA



CORE-LOC®



ACCROPODE™ is a trademark of SOGREAH - France

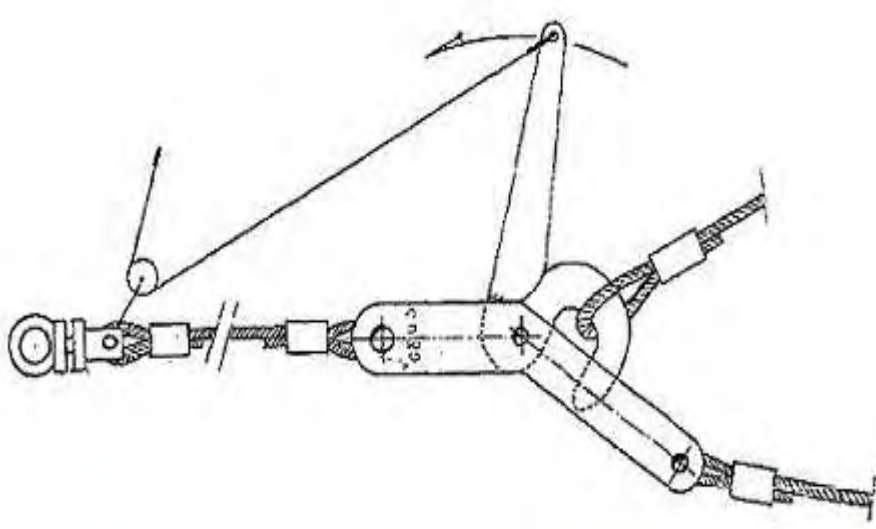
ACCROPODE™ est une marque déposée par SOGREAH - France



ACCROPODE™



ACCROPODE™ is a trademark of SOGREAH - France



ACCROPODE™ est une marque déposée par SOGREAH - France



ACCROPODE™

ACCROPODE™ est une marque déposée par SOGREAH - France



ACCROPODE™ is a trademark of SOGREAH - France

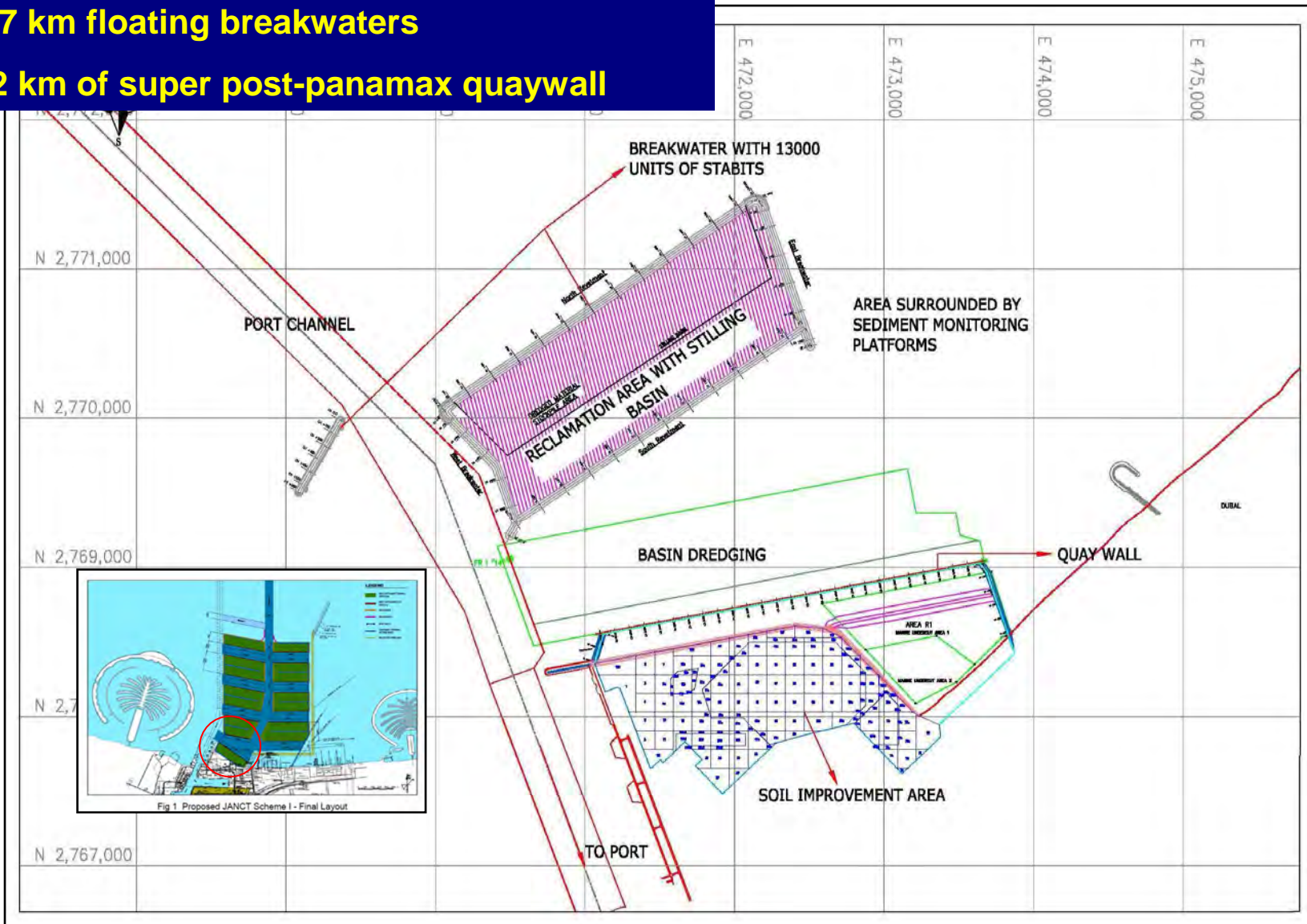


ACCROPODE™

Key Figures:

- 23 Mm³ of dredging
- 9 km of rubble-mound breakwaters
- 1,7 km floating breakwaters
- 2,2 km of super post-panamax quaywall

Jebel Ali New Container Terminal Phase 1



Jebel Ali New Container Terminal Extension



Construction of rock-bund and reclamation of container –terminal area

Jebel Ali New Container Terminal Extension



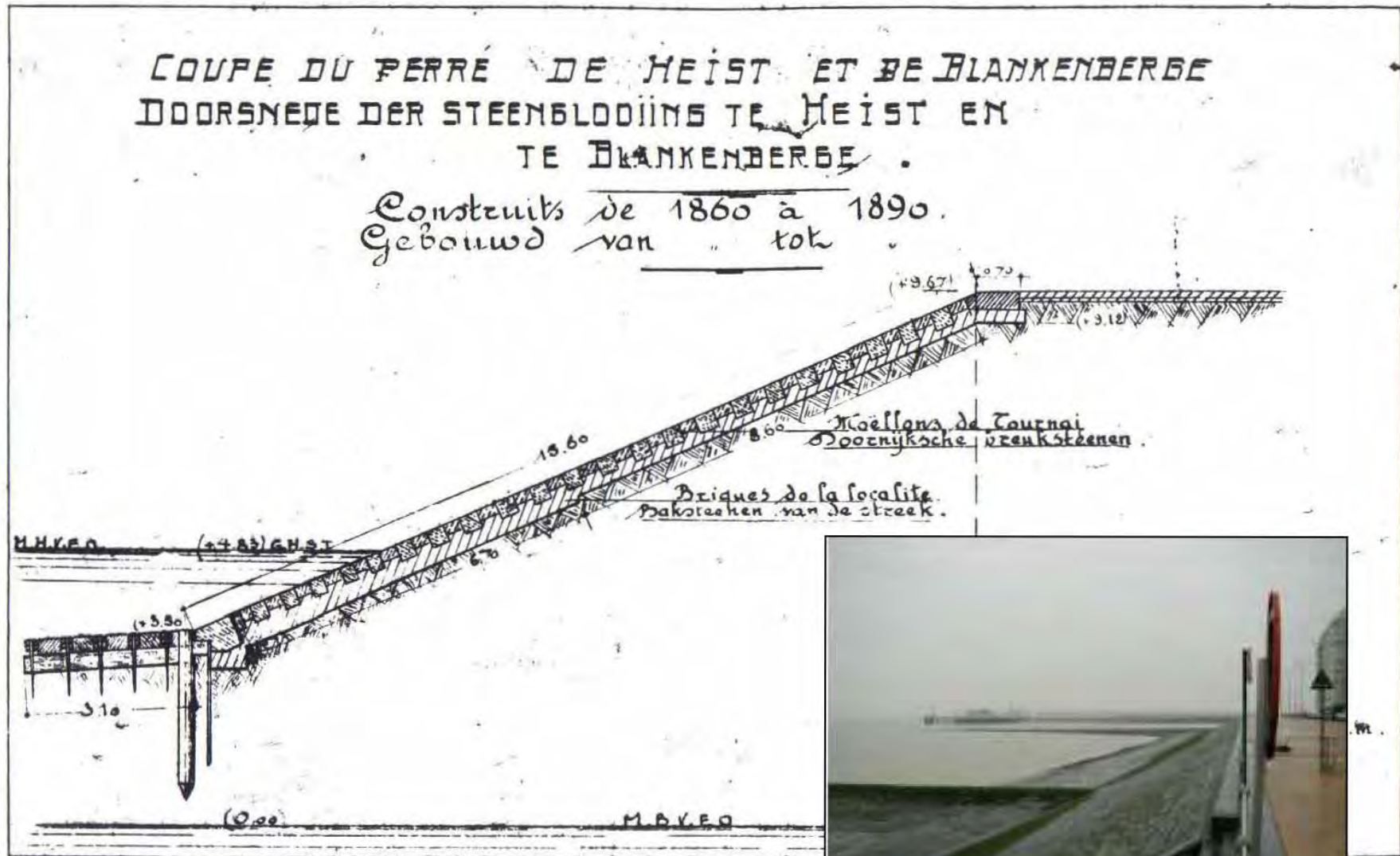
Container Port Jebel Ali, Dubai



Container Port Jebel Ali, Dubai
Armouring with 11 ton Stablit CAU's



Sea-defence works: sea-dikes



Sea-dike, Bredene (Belgium)



Coastal protection structures: groynes

JETÉE N°22 SUR LA PLAGE DE BLANKENBERGE
STRANDHOOFD N° 22 OP HET STRAND TE BLANKENBERGE
COUPE A-B. DOORSNEDE A-B.



Coastal groyne , Ostend (Belgium)



Groyne Fields, Cadzand



Concrete in Waterfront Engineering.

Challenges:

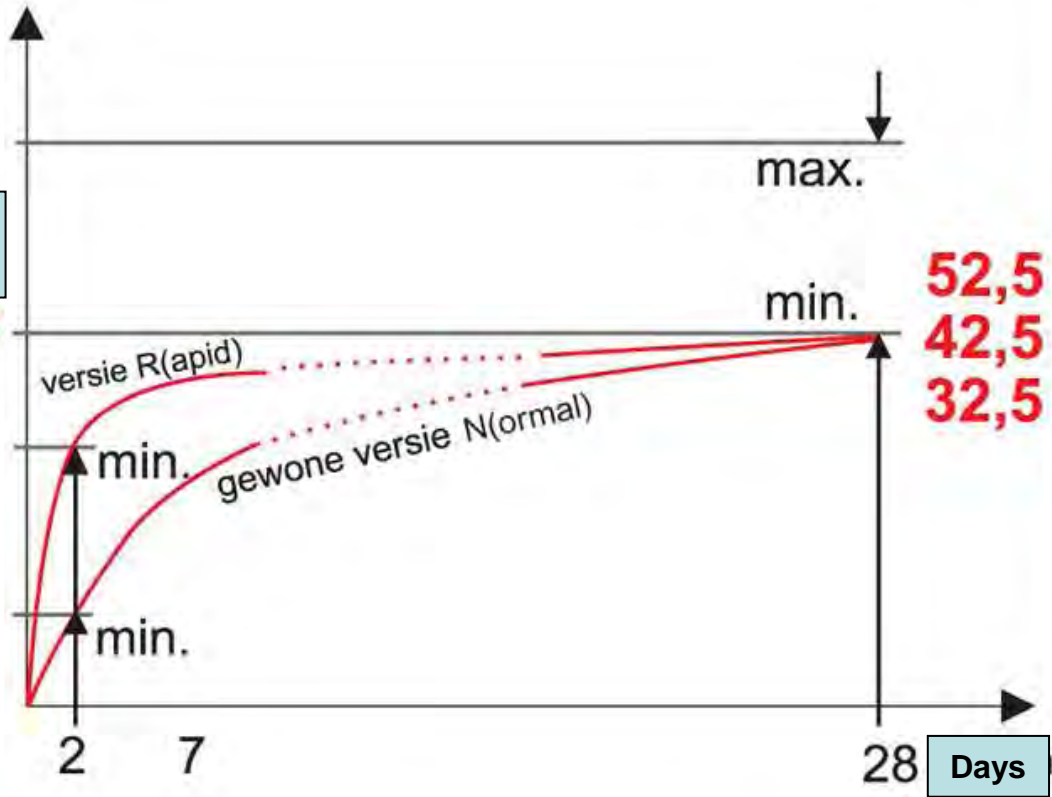
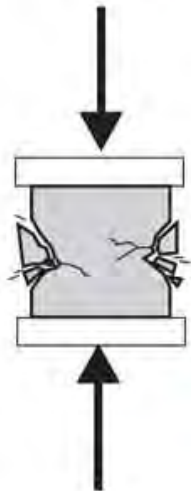
- **limited sustainability (> 100 years ?)**
- **sensitive to sulphate weathering (sea-water environment)**
- **reinforcement corrosion**
- **....**

Concrete for Waterfront structures: High Sulfate Resisting (HSR) Concrete

- Granulates : 0/4, 4/16, 16/32 or 4/32: grades in mm ranges @ 750 l/m³
- Sand: Rhine-sand @ 400 l/m³
- water : water/cement factor = 0,4
- Low-Alkali Cement (either or not self-compacting):
 - Lean Concrete
 - C15 (ca 100 kg Cement/m³): workfloor, ...
 - C20 : blinding support
 - Rich Concrete
 - C30 : precasting
 - C40 (ca 400 kg Cement/m³)
- Cement- containing additives:
 - micro-silicates: to improve durability
 - fly-ash : as a (cheap) substitute for cement
 - colloïds : to make concrete hydrophobic
- Additives to influence hardening:
 - Slow-down: when concrete-plant is remote
 - Accelerators: when formworks have to be removed swiftly
 - Mix e.g. Glenium (BASF): first slow-down, then accelerated
- Reinforcement:
 - fibre-glass (improves tensile strength)
 - steel with active cathodic protection
 - epoxy- coated steel
 - stainless steel

Compression Strength Tests on Concrete

Compression strength
UCS
(Newton/mm²)



Tests done on samples kept at 20°C under water

Concrete Caissons for Breakwaters or Quaywalls



Dry-docks used for caisson-construction



Colloïdal Concrete (info cfr Interbeton):

- open structure
- closed structure

Hydromix is een merknaam van Interbeton
Cfr www.heidelbergcement.com

Characteristics:

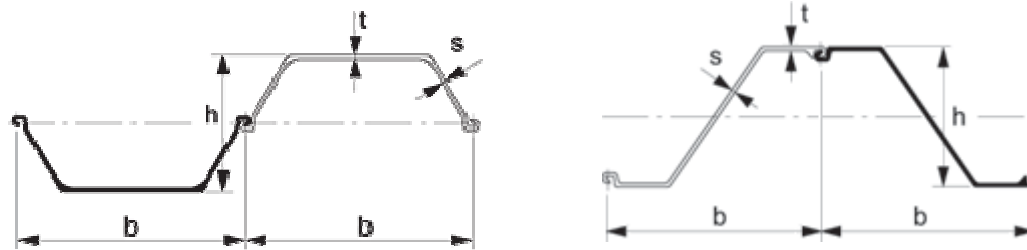
- UCS = 7 N/mm²
- $\rho = 1750 \text{ kg /m}^3$
- $k = 2 \cdot 10^{-4} \text{ to } 2 \cdot 10^{-7} \text{ m/sec}$



Underwater Concrete with closed structure (cfr Hydromix)



Sheetpile Walls : U- orf Z- profiles



Choice of profile depends upon:

- **Ultimate soil/water load (horizontal soil pressure): U-profile has a stronger bending moment, Z-profile is more economic**
- **Type of Soil :**
 - **Resistant Soils (e.g. $q_c > 2 \text{ MPa}$ or $\text{SPT} > 15$)with difficult driveability: U profile preferred (= stronger)**
 - **Soft soils with good driveability: Z-profile preferred because more cost-effective (relative to kg of steel)**

Accelerated Low-water Corrosion in Oxygen-rich water environment (top part & splash zone):

Protection by:

- **Overwidth on steel : corrosion = ca 0,10mm/year**
- **Coatings (epoxy) ...but risks of damage during driving**
- **Cathodic protection, either passive with sacrificial Zn-anodes (1kg/m² exposed), either active, with DC**

Application of sheet-piles in cofferdams



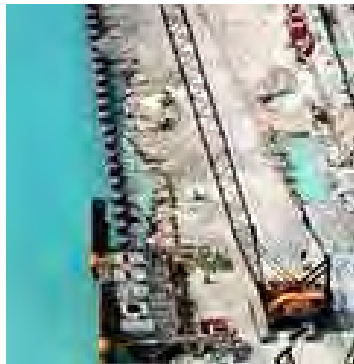
Double sheet-pile wall, Blankenberge (Belgium)

Maritime & Dredging 2010



Combi-Walls:

Combination of deeper tubes (stability) with shallow U-profiled sheetpiles (soil/water retention)



Bouw van de 2^{de} Sluis te Evergem: Buispalen en Combi-walls



New lock-chamber at Evergem-Lock on Canal Ghent-Terneuzen



Combiwall in Danish Quay-Wall , Albert I dock, Zeebrugge, Belgium

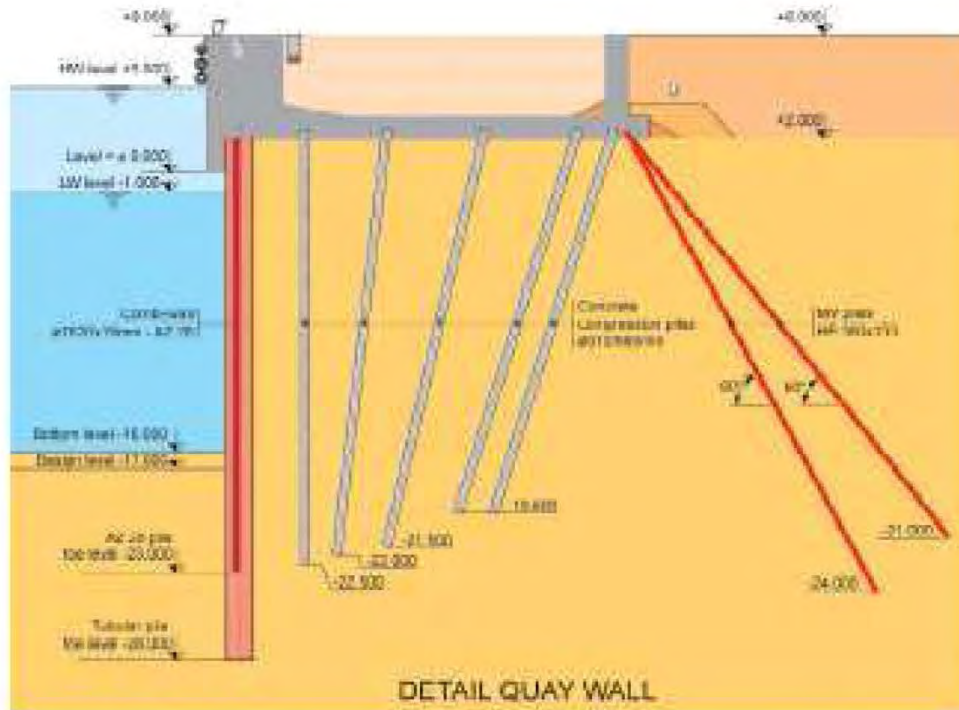


Fig 1: Type dwarsprofiel van kaaimuur 'Albert I dock'
 Section type du mur de quai 'Albert I dock'
 Typical cross-section of quay-wall 'Albert I dock'



Fig 2: Horizontale snede de or combi-waer d
 Coupe horizontale de la paroi combinée
 Horizontal section of combi-wall

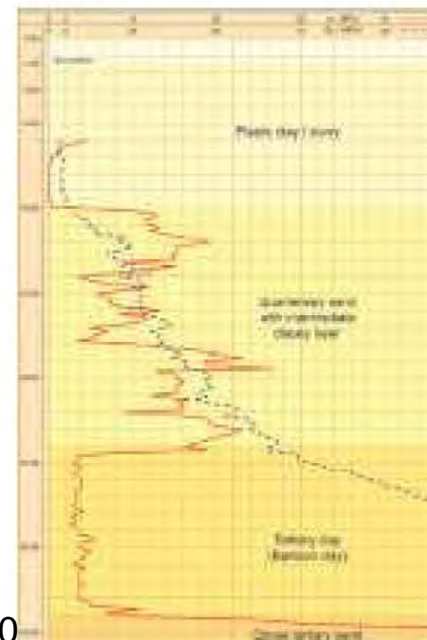
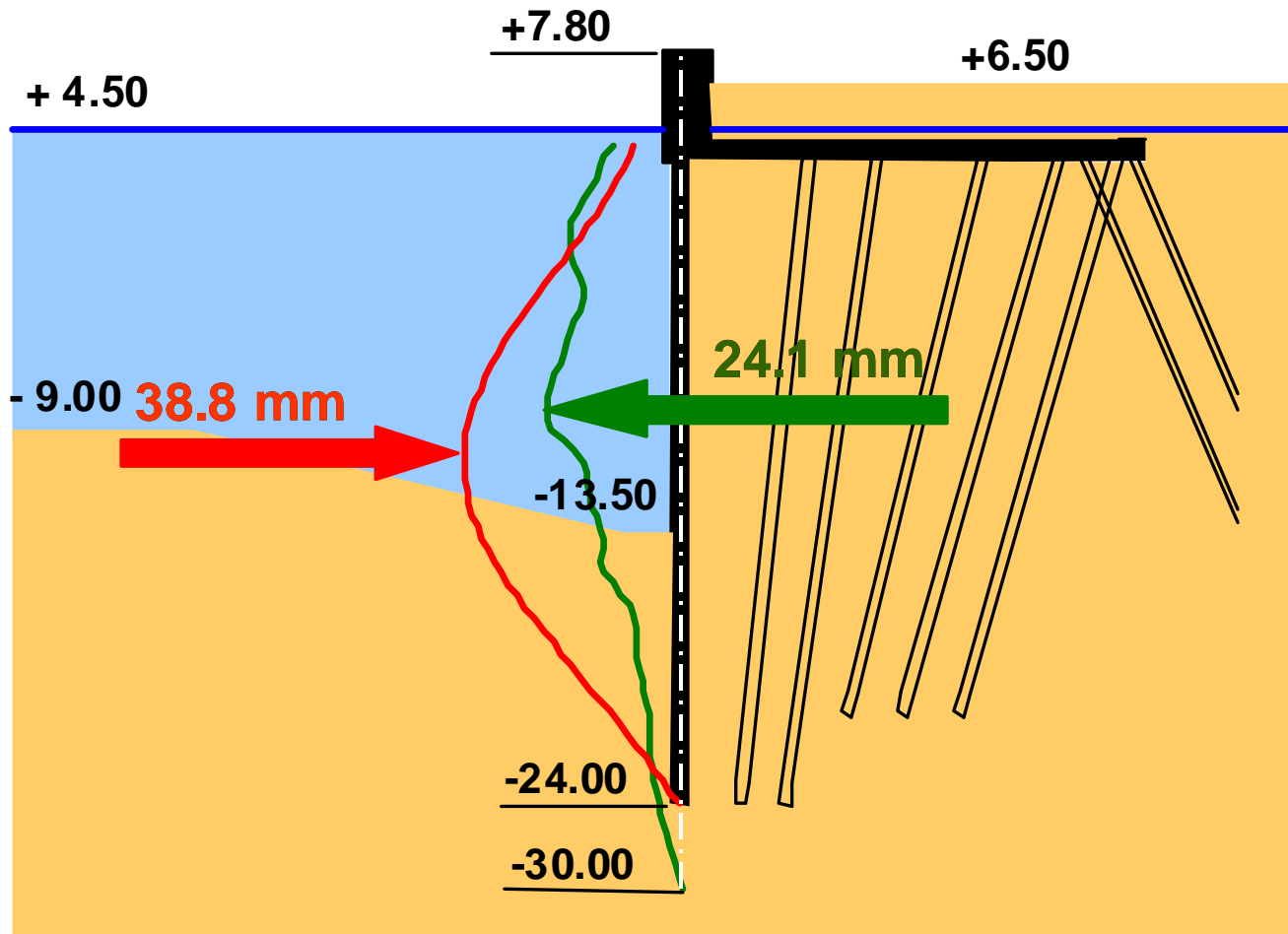


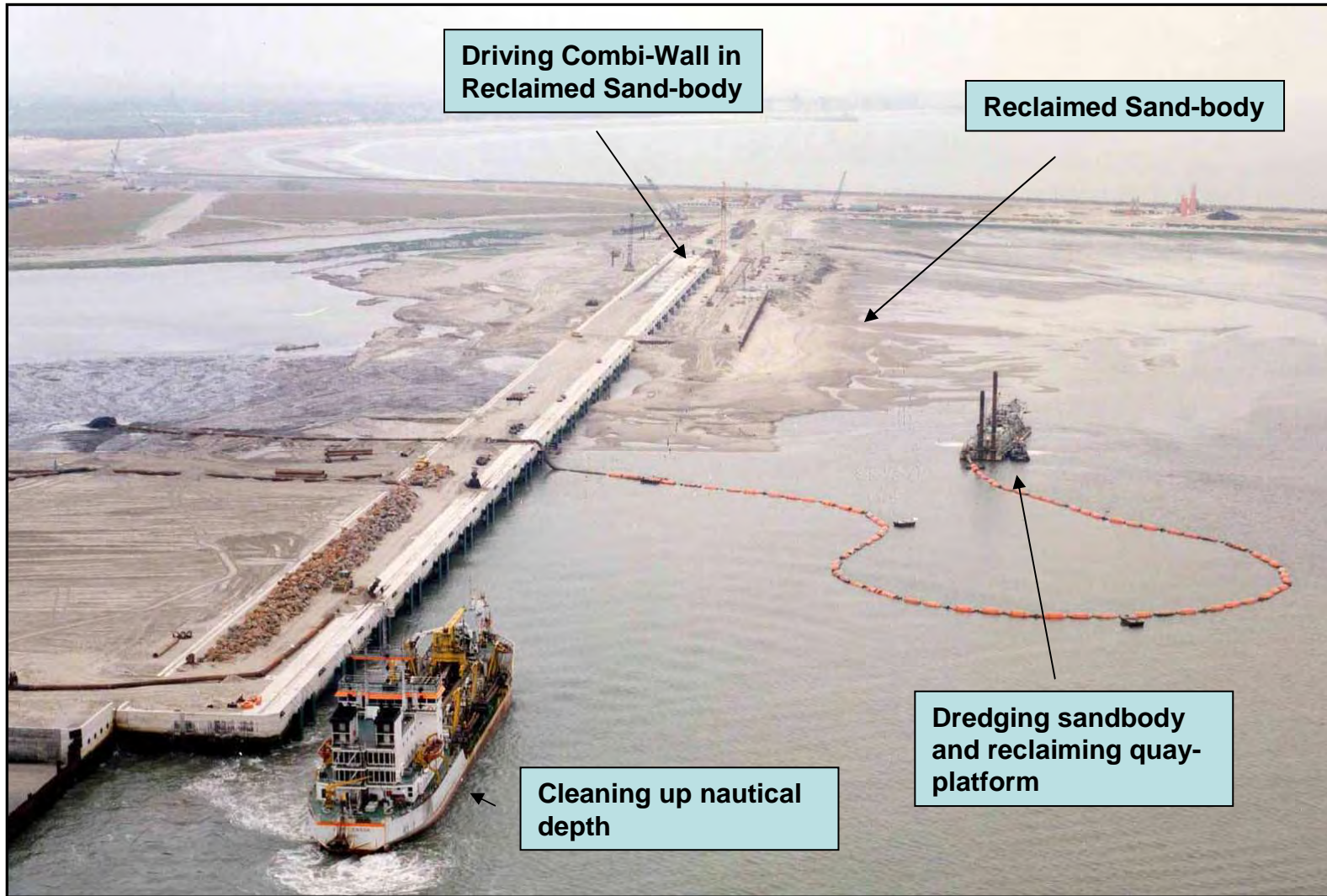
Fig 3: Sonderingen ter hoogte van dwarsprofiel

Monitoring horizontal movements in Combi-Walls

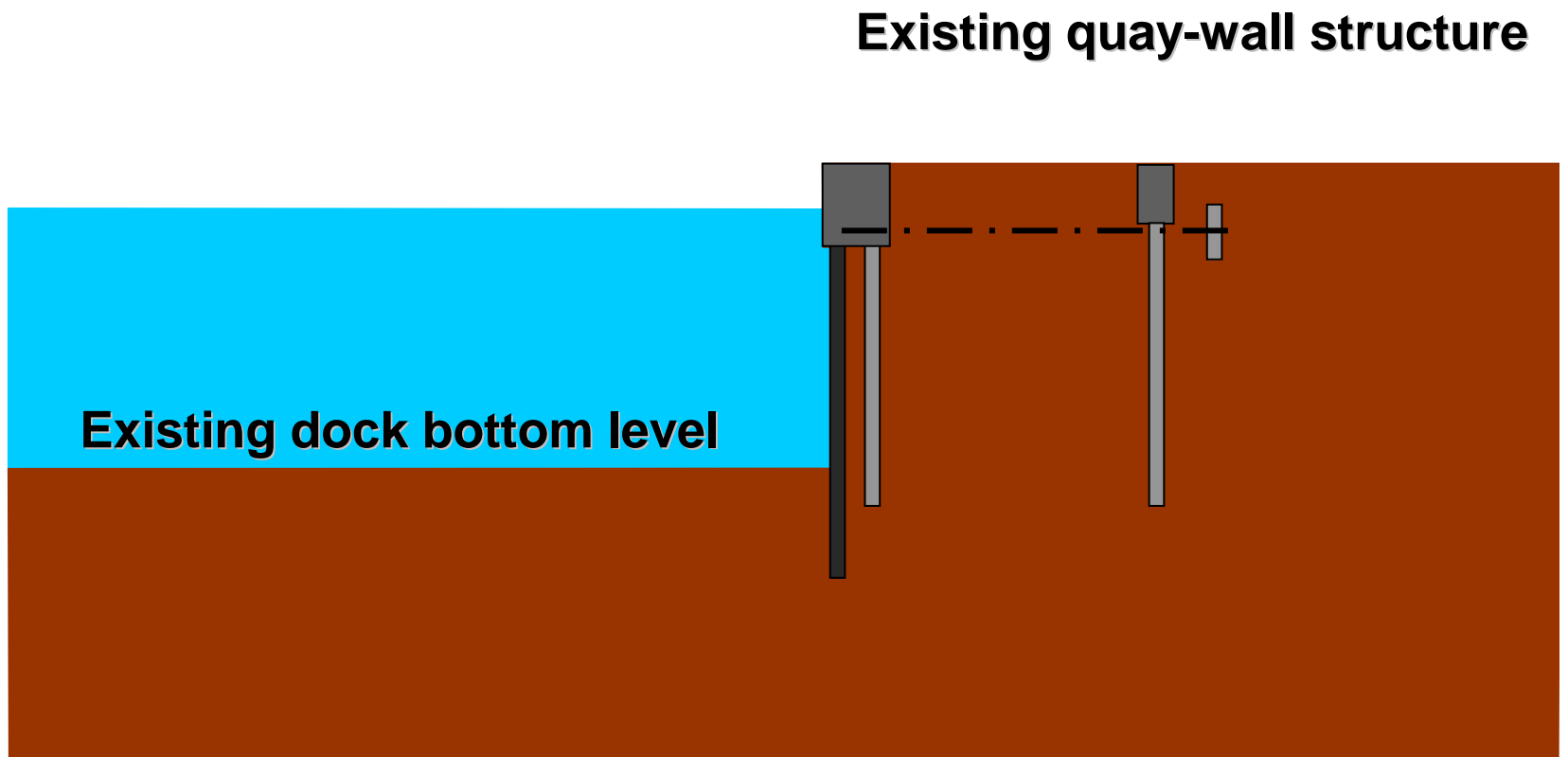
Monitoring : inclinometers (3/4)



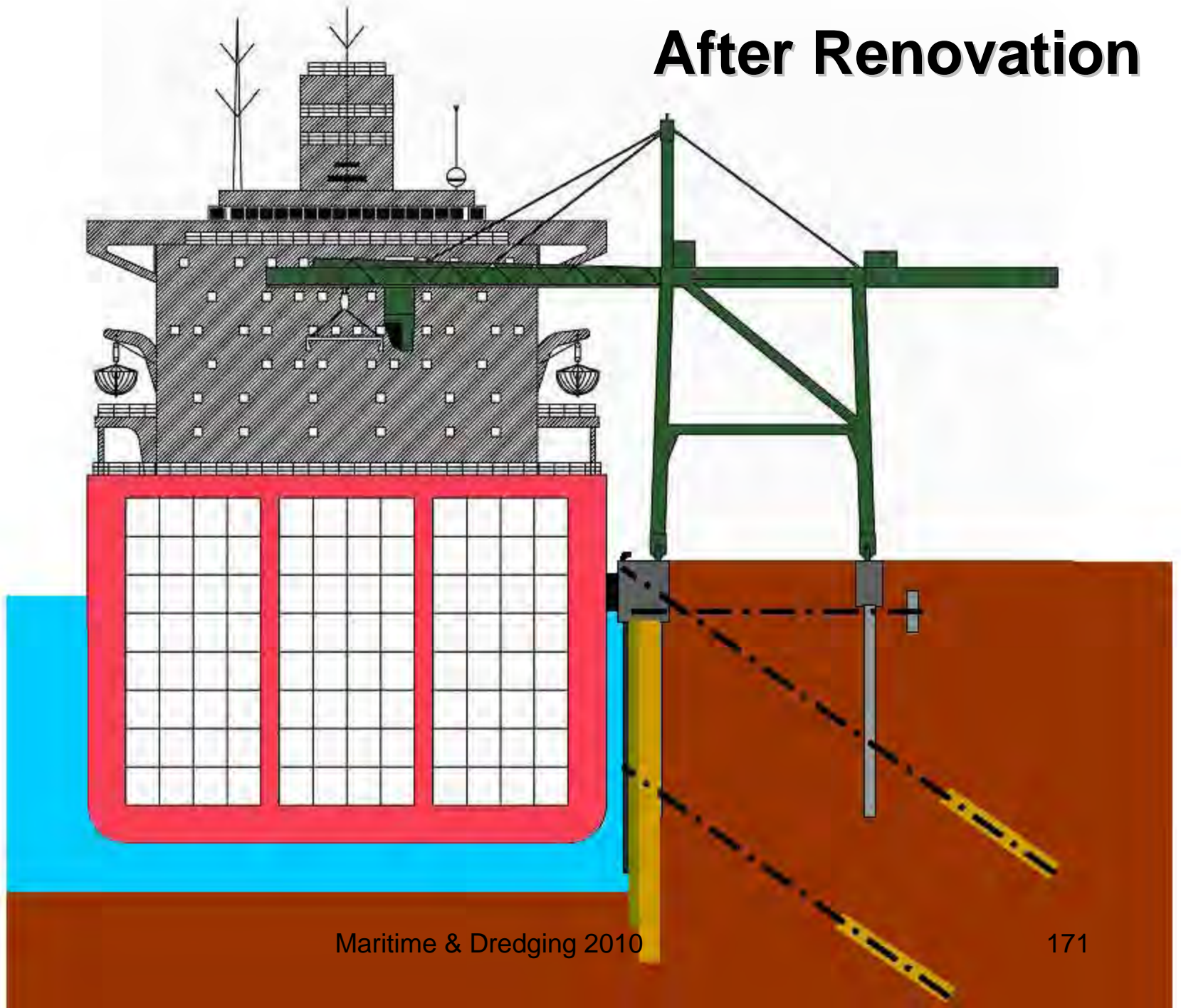
Construction of Albert II-Dok Quay-Wall (Zeebrugge)



Renovation of Quaywalss in the port of Ghent, Belgium



After Renovation



Sheetpiles in Waterfront Engineering: flexible, cheap, but... Accelerated Low Water Corrosion (ALWC)

What ?

In the tidal range and splash zone and to ca 1 to 2m under the LW-line, bacteria are agglutinated to the steel causing an acid-corrosion: the result is a strongly accelerated corrosion and oxydation of the steel.

Normally, a corrosion of 0,08mm to 0,17 mm/year/wet surface is to be considered

ALWC corrodes up to 0,3mm to 2mm/year/wet surface !

Solutions?

Cathodic Protection with sacrificial (Zn) anodes

Epoxy-coatings

Calcium Carbonate/ Mg - hydroxyde coating

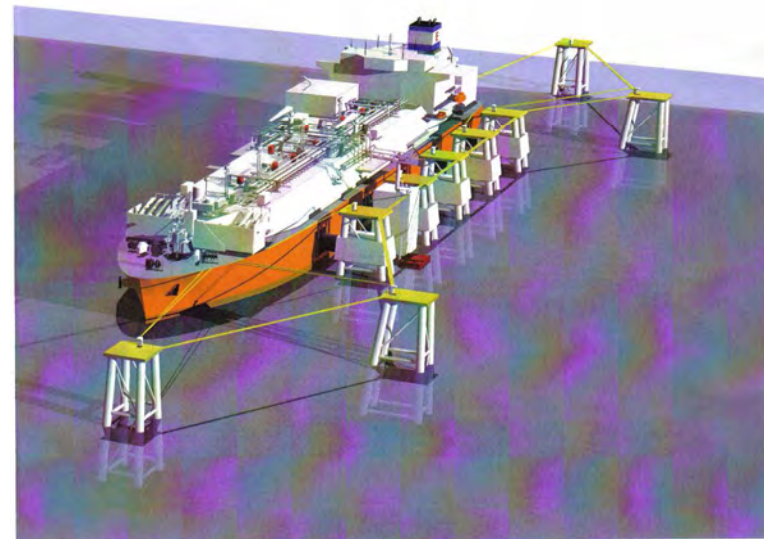
Concrete Tube-Piles or Steel Tube-Piles (fully or partially filled with (reinforced) concrete) for breasting Dolphins, Mooring Dolphins



Steel Tube-Piles: choice is determined by steel-quality, i.e. the Flow-limit of the steel.

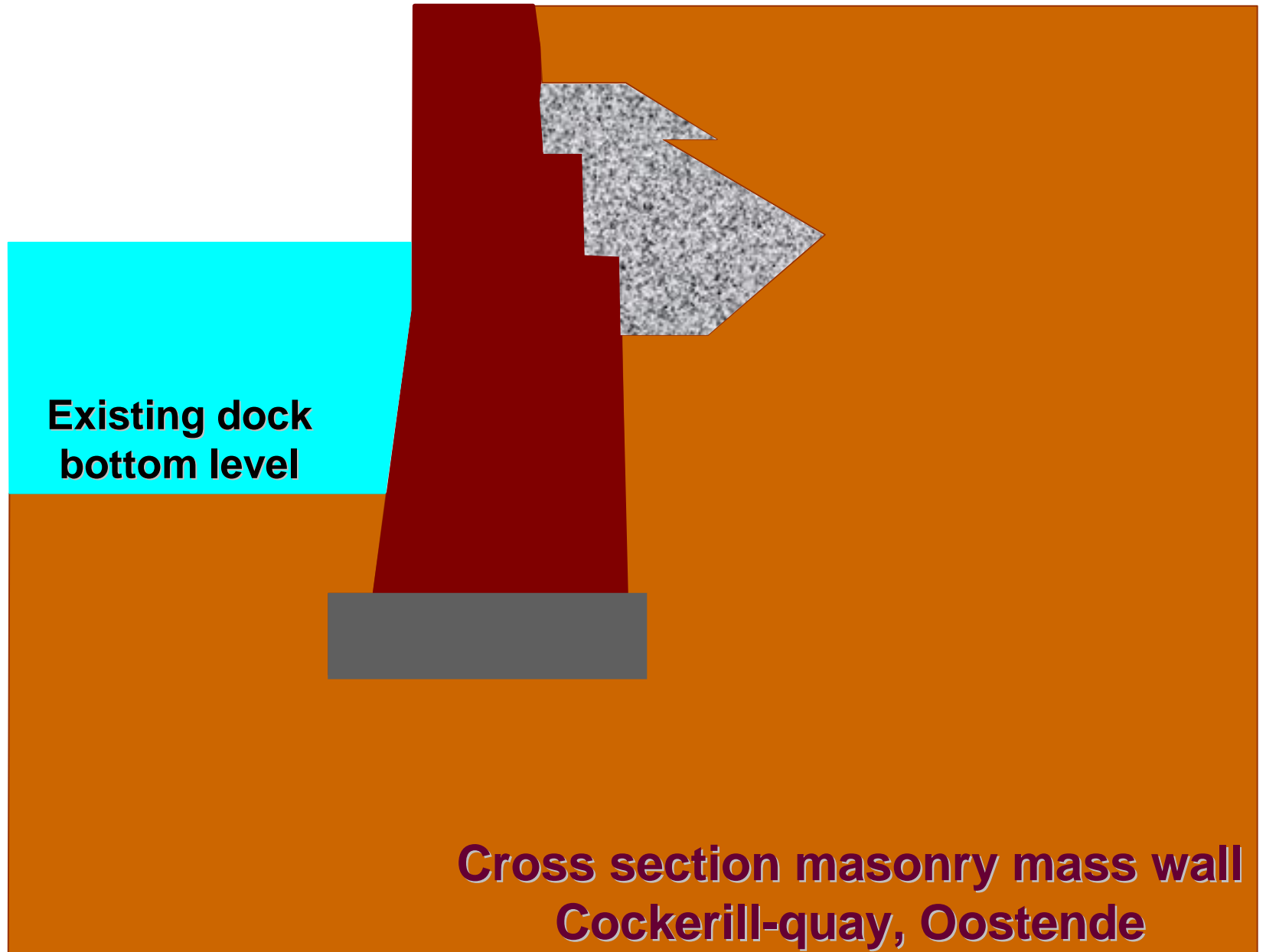
Generally, it appears to be more cost-effective to use lighter tube-piles with a high-quality steel (instead of larger tube-piles, with lower steel-quality).

Dimensions are engineered via bending moments, driving depth (geotechnics,...),...

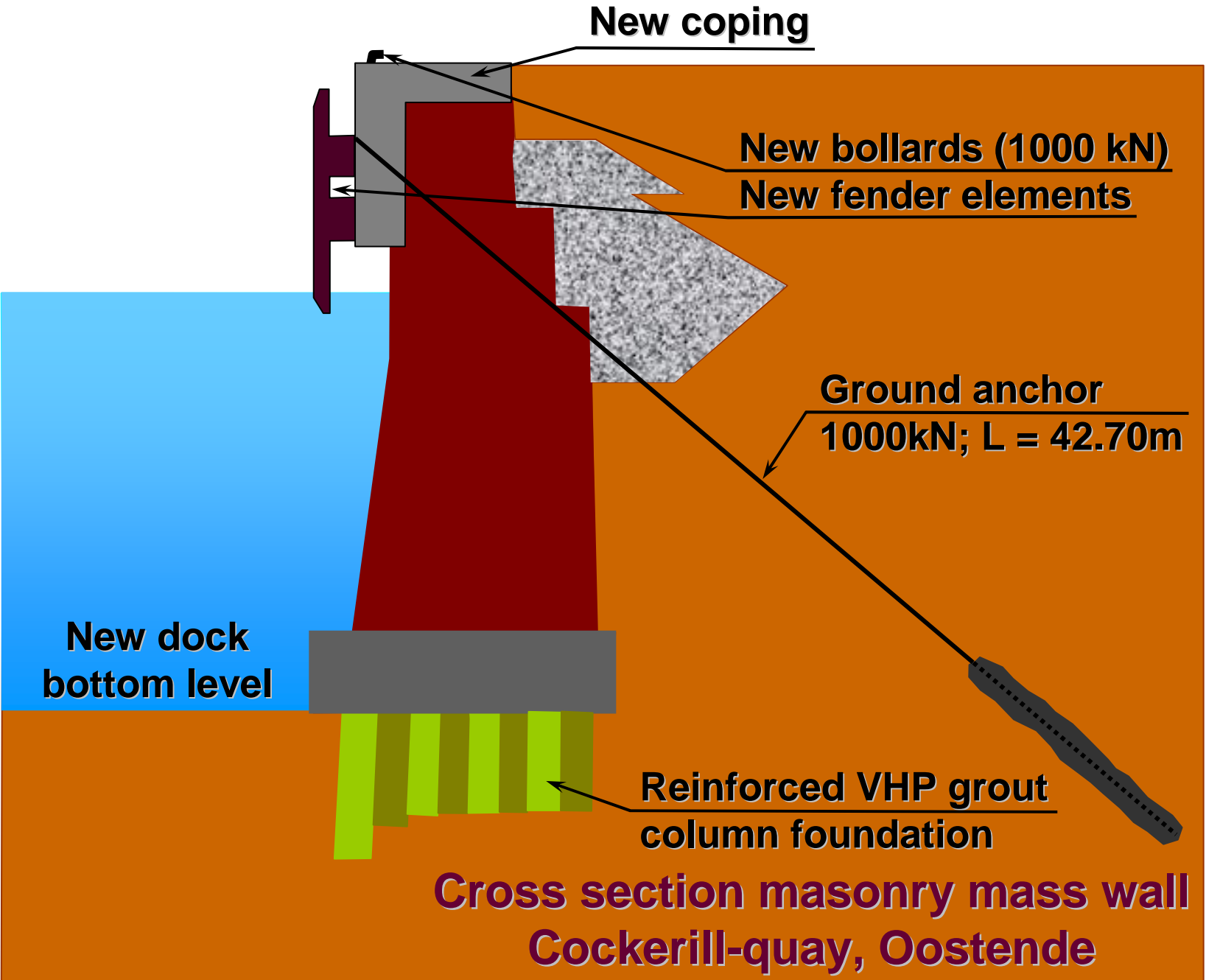


Massive gravity quay-walls

Existing quay-wall structure



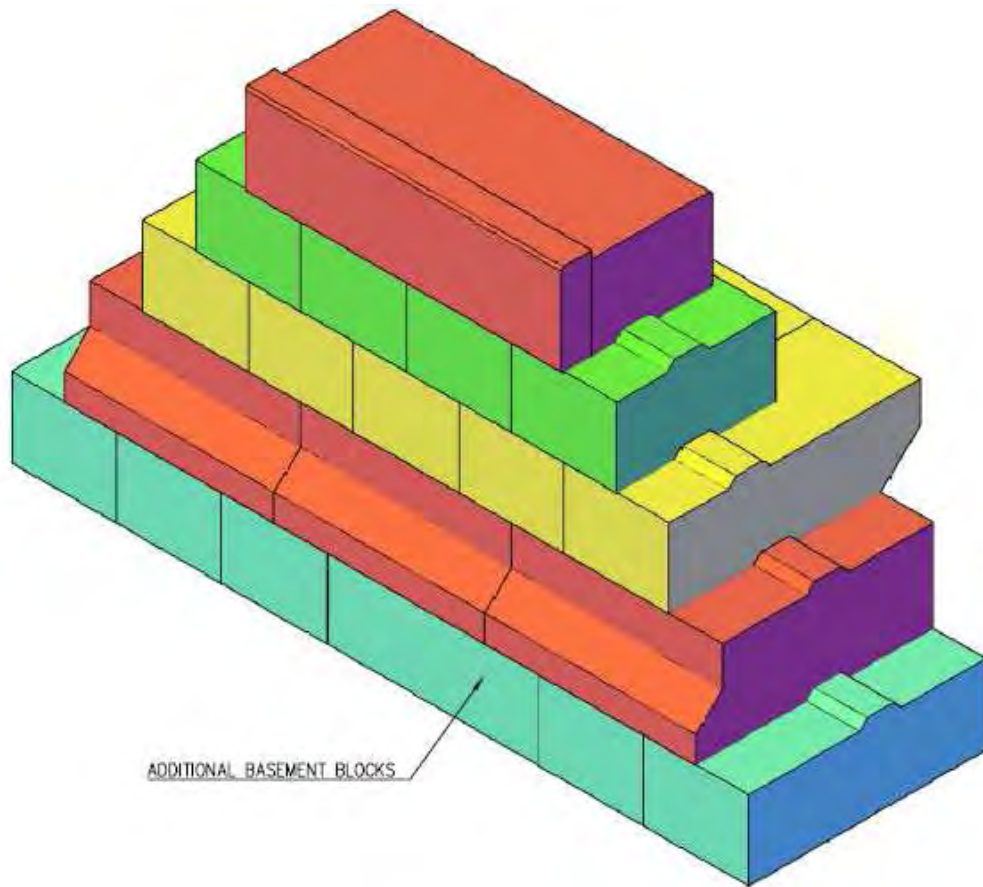
After renovation , Port of Klaipeda, Lit



IMPACT RECONSTRUCTION



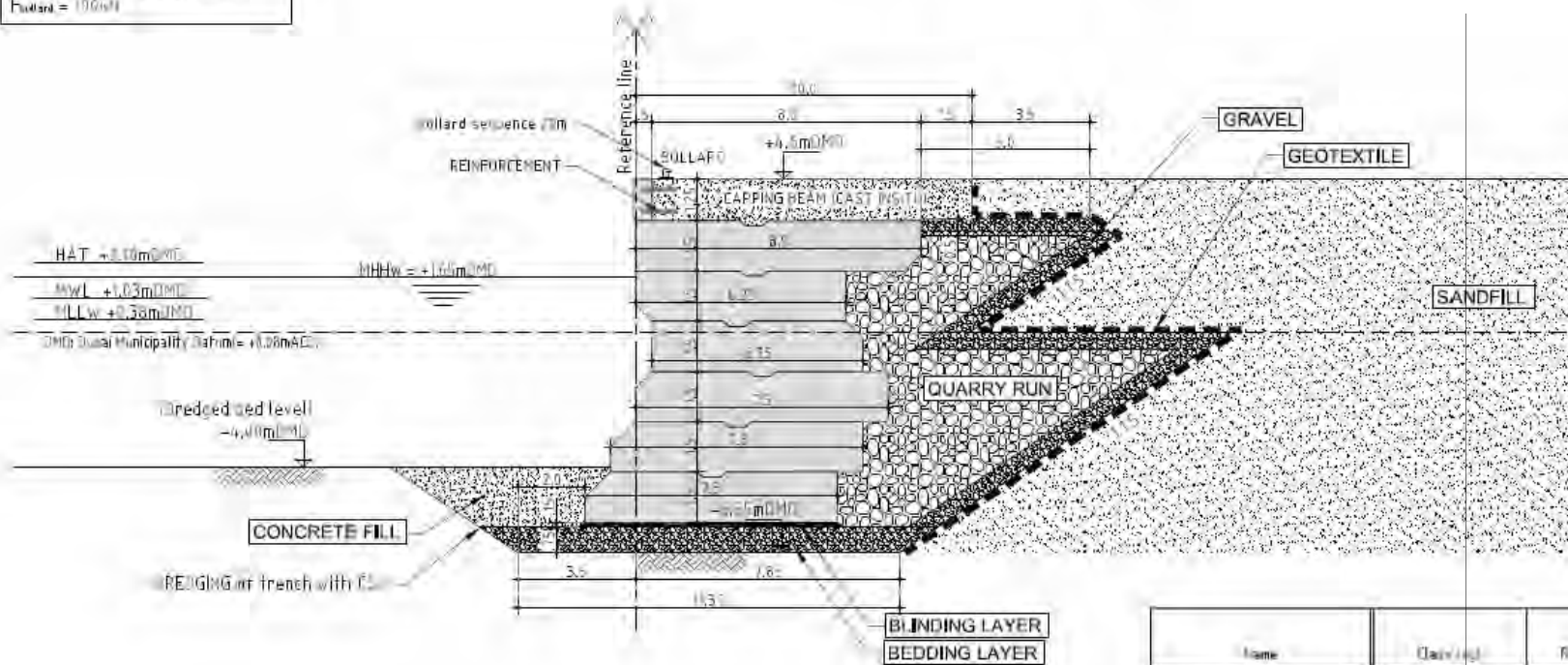
Gravity Quaywalls, constituted of Concrete Blocks, Cove Canal, UAE



Examples of Engineered Block-Walls

CROSS SECTION A-A

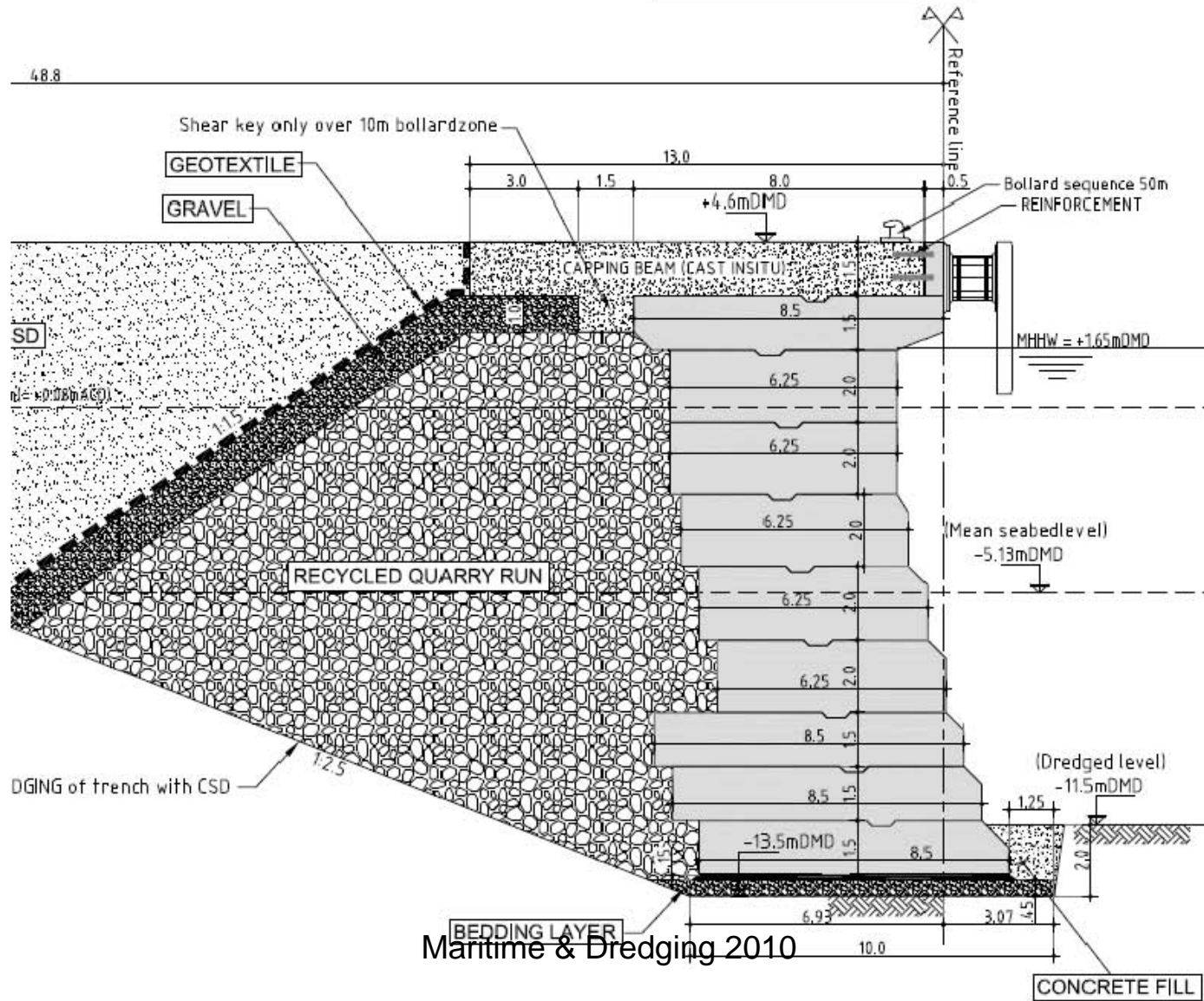
DESIGN PARAMETERS ODA/WALL
 Surcharge = 10kN/m² (trucks)
 Max. water difference = 0.2m
 Footing = 100kN



Name	Class (mm)	Rate (kg/m ³)
Bedding Layer (10 to 15mm)		1500
Quarry Run	0.75m	1000
Gravel (5 to 15mm)		700
Blinding Layer (30mm)		300
Cast in-situ		1000
Concrete Fill		1500
Precast Blocks		1500

Examples of Engineered Block-Walls , Cruise Terminal

DESIGN PARAMETERS QUAYWALL
 Surcharge = 10kN/m² (trucks)
 Max. Water Difference = 0.2m
 F_{ballard} = 1000kN
 S_{ballard} = 1.5
 S_{overturning} = 1.5





Palm Cove Canal, UAE:

More than 12 km of qua-wall constructed with 25 to 32 ton unreinforced concrete blocks





Course-1: 4-side mould.



Overview Precast Yard



Course-1: casting 2-side mould



Overview Precast Yard



Mould C2



Lifting Course-2 block.



Mould C3



Placing course-2 block.



Formwork Course-4B, Precast Front Panel. Casting position.



Course-4B "Precast Front Panel": Lifting block out of mould.



Formwork Course-4B, Precast Front Panel. Open position after removing block.



Course-4B "Precast Front Panel": Stockpile & GFRP-bars for connection with C4A.



Course-4B "Precast Front Panel": Placing blocks at Quay Wall.



Mould Course-4A



Course-4B "Precast Front Panel": Side view with mould Course-4A



Pontoon Corner



Return corner section-1



Insitu casted "Pontoon-Corner" after completion

Massive Gravity Wall cast in-situ: example of Verrebroeck-Dock, Port of Antwerp

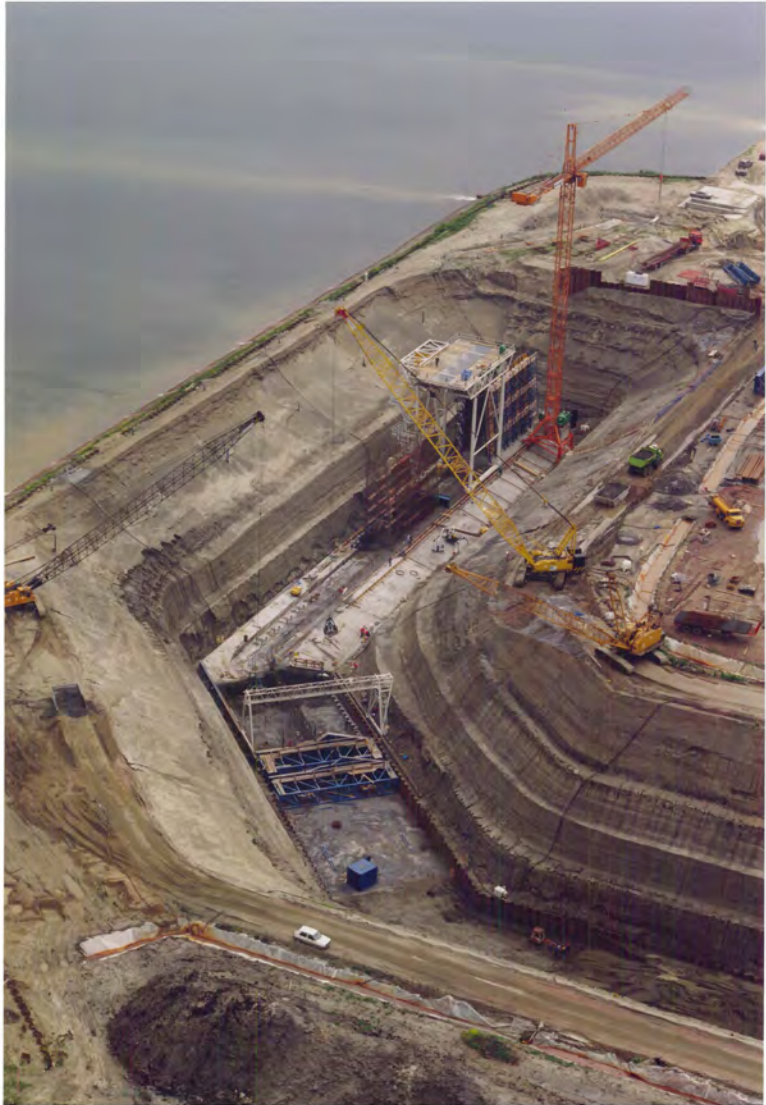


Fixed Formwork in corners



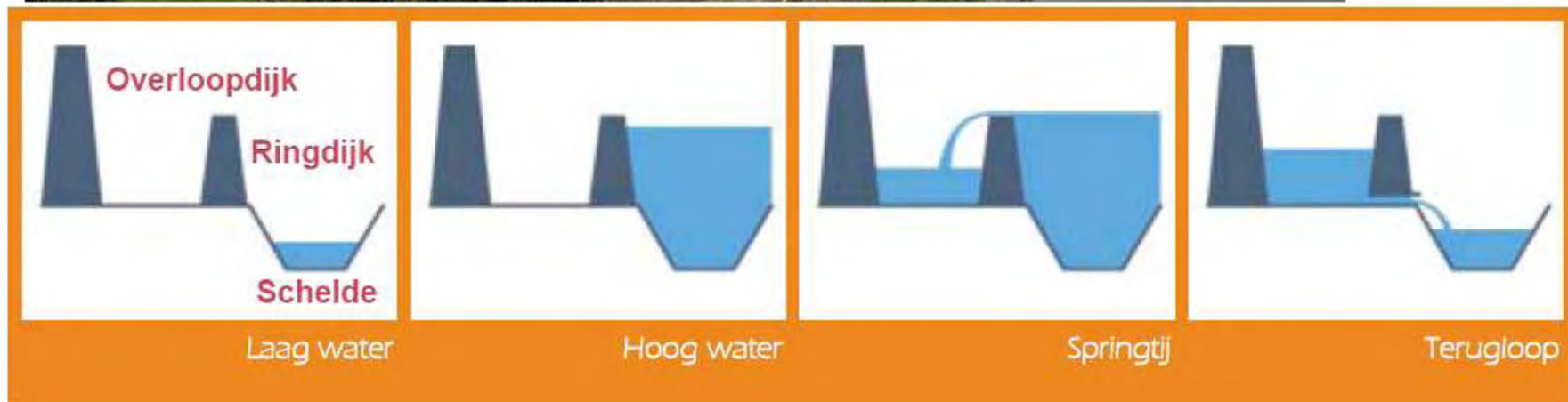
Sliding formwork

Verrebroeck-Dock: Port of Antwerp





Controlled Inundation Area at Kruiseke Bazel Rupelmonde (KBR), River Scheldt: construction of dewatering sluices





KBR at LW



KBR at HW



KBR at extreme HW

